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Process Safety and the Energy Transition

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2023 MKOPSE Conference

The Challenge of the Energy Transition is Immense

According to the International Energy Agency:

- Net zero to 2050 hinges on an **unprecedented** clean technology push to 2030
- Net zero to 2050 requires **large leaps** in clean energy innovation

Source: International Energy Agency Special Report “Net Zero by 2050”

What are some of the technologies involved?



Wind and Solar



Carbon Capture and Storage



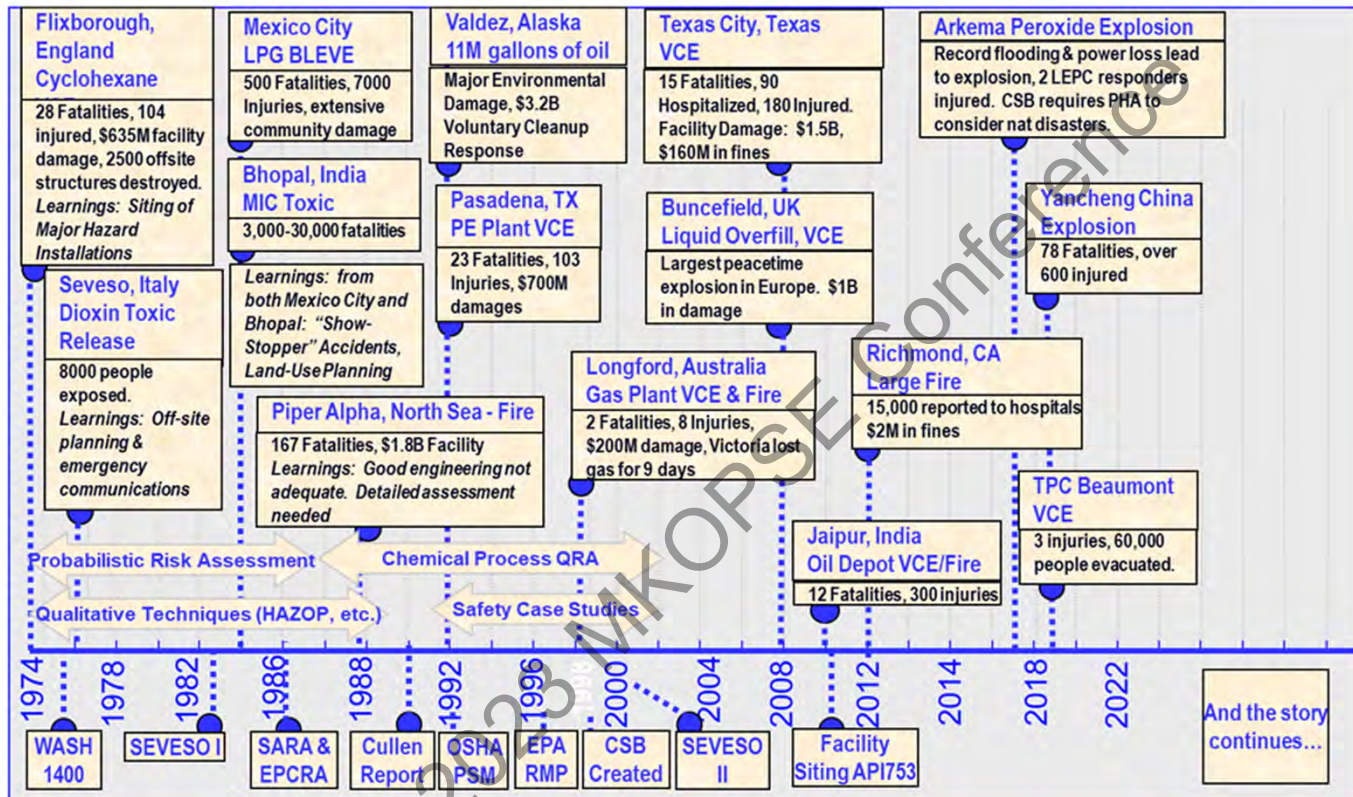
Low Emissions Fuels



Nuclear

And what are the hazards associated with them?

We Can Draw On Our Knowledge of the Past . . .



To Inform the Future of Process Safety

We Know What To Do



What We Must Do

- Consider the energy transition may bring new process safety challenges and hazards.
- Leverage current expertise to manage potential new hazards.
- As process safety professionals we must take a leading position to ensure the proper management of all hazards in the energy business – old and new.
- As new hazards emerge, we must lead the way to ensure our own organizations, regulators, standards bodies, policy makers and members of the communities in which we operate understand and effectively manage those hazards.

2023 MKOPSE Conference

Thank you

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2023 Mary Kay O'Connor Safety & Risk Conference

Safe and Sustainable Energy Transition

In Association with IChemE

October 11-13, 2023



Texas A&M Engineering Experiment Station

Mary Kay O'Connor
Process Safety Center

26th Process Safety International Symposium





Speaker profile



- Hema Divya Katna

- Hema Divya is currently pursuing her Masters in Process Safety at University of Aberdeen, Scotland, UK. She worked as a Process Safety Management Consultant at Kaypear from 2018. At Kaypear, she provides PSM consultancy services to Oil & Gas and Petrochemical industries. She has worked with both domestic and international clients providing specialized relief system validation that includes risk mitigation services and has strong knowledge of API 520, API 521, and ASME Section VIII Div.1. She is a scribe and assists the PHA facilitator in nodding of P&IDs, consolidation of risk register, prioritization of action items, and generation of technical reports. She is an Associate Member with Chartered Engineering Certificate from Institute of Engineers India(IEI). Hema Divya graduated with a Bachelors in Technology in Chemical Engineering from SVCE, Chennai [Anna University] in 2018 and a PG Diploma in Petrochemical Process Safety and Engineering from Bharat Sevak Samaj in 2020.



Threshold Quantity for Process Safety Metrics for Special / Coded Chemicals

- Essential element in improving the process safety program is to identify existing process safety performance to improve future performance
- To improve the performance, a company has to implement leading and lagging process safety metrics
- Lagging indicators measures what has already happened, such as accidents and injuries
- Lagging process metrics can be developed using the following guideline document CCPS Process Safety Metrics and API-754
- Major step involved in implementation is grouping the compounds based on its physical and chemical properties to define its threshold quantities

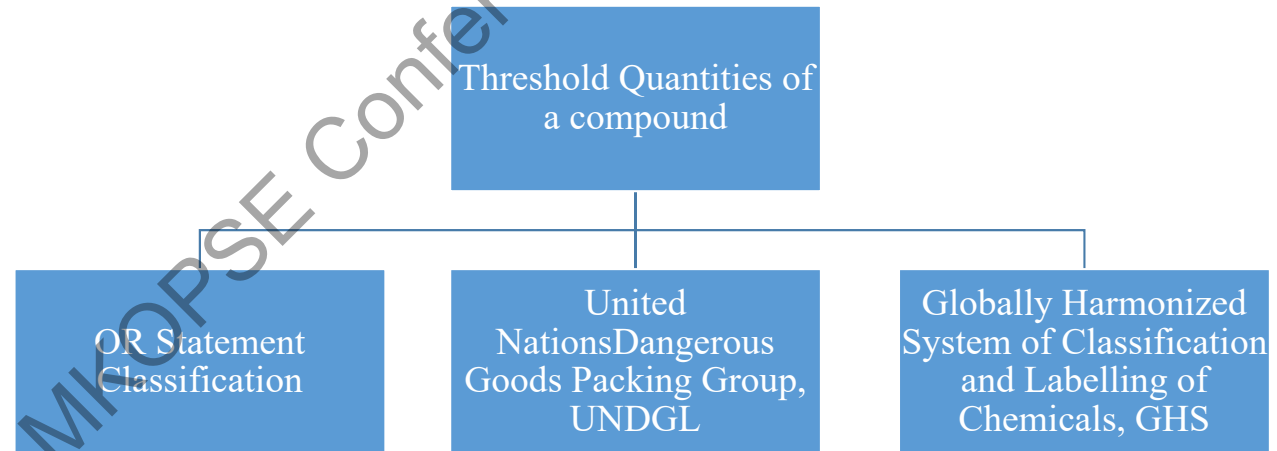


Problems Faced In Using Guideline

- Guidance provided is not exhaustive
- Especially leaves interpretation of determining threshold quantities for chemical compounds with ambiguity due to the material complexities in a multi-product plant
- Standards are US-centric and more guidance is needed for companies who want to implement it in a global scale
- Difficulty faced by these companies are grouping the materials and assigning the correct threshold quantities
- As these companies use coded chemicals and introduce at least 50 new compounds in 2-3 months of time frame

Understanding the Classification

- Use UNDG Classification - primary method
- Globally Harmonized System of Classification and Labelling of Chemicals - GHS Standard - primary method
- Simple characteristics such as toxicity, flammability or corrosivity of the compound - OR statement classification - secondary method





Precedence of Hazard Characteristics

- UNDG classification and secondary method of classification
- One compound can be classified in more than one class by the supplier based on transportation rules
- OR statement classification a compound can have two characteristics at the same time
- Example - styrene is reactive, toxic, and flammable
- Precedence table based on the Department Of Transportation (DOT) regulations - used to determine which property or class/packing group of the compound to be used to determine the threshold quantities

TABLE 3.10.A
Precedence of Hazards and Packing Groups for Classes 3, 4 and 8 and for Divisions 5.1 and 6.1 (3.10.1)

Class or Division	Packing Group	4.2		4.3		5.1		6.1		8		8		8		8			
		II	III	I	II	I	II	I	II	I	II	I	II	I	II	I	II		
3	I*			4.3, I	4.3, I	4.3, I	—	—	—	3, I	3, I	3, I	3, I	3, I	—	3, I	—	3, I	—
3	II*			4.3, I	4.3, II	4.3, II	—	—	—	3, I	3, I	3, II	3, II	8, I	—	3, II	—	3, II	—
3	III*			4.3, I	4.3, II	4.3, III	—	—	—	6.1, I	6.1, I	6.1, II	3, III**	8, I	—	8, II	—	3, III	—
4.1	II*	4.2, II	4.2, II	4.3, I	4.3, II	4.3, II	5.1, I	4.1, II	4.1, II	6.1, I	6.1, I	4.1, II	4.1, II	—	8, I	—	4.1, II	—	4.1, II
4.1	III*	4.2, II	4.2, III	4.3, I	4.3, II	4.3, III	5.1, I	4.1, II	4.1, III	6.1, I	6.1, I	6.1, II	4.1, III	—	8, I	—	8, II	—	4.1, III
4.2	II			4.3, I	4.3, II	4.3, II	5.1, I	4.2, II	4.2, II	6.1, I	6.1, I	4.2, II	4.2, II	8, I	8, I	4.2, II	4.2, II	4.2, II	4.2, II
4.2	III			4.3, I	4.3, II	4.3, III	5.1, I	5.1, II	4.2, III	6.1, I	6.1, I	6.1, II	4.2, III	8, I	8, I	8, II	8, II	4.2, III	4.2, III
4.3	I						5.1, I	4.3, I	4.3, I	6.1, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I
4.3	II						5.1, I	4.3, II	4.3, II	6.1, I	4.3, I	4.3, II	4.3, II	8, I	8, I	4.3, II	4.3, II	4.3, II	4.3, II
4.3	III						5.1, I	5.1, II	4.3, III	6.1, I	6.1, I	6.1, II	4.3, III	8, I	8, I	8, II	8, II	4.3, III	4.3, III
5.1	I									5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I
5.1	II									6.1, I	5.1, I	5.1, II	5.1, II	8, I	8, I	5.1, II	5.1, II	5.1, II	5.1, II
5.1	III									6.1, I	6.1, I	6.1, II	5.1, III	8, I	8, I	8, II	8, II	5.1, III	5.1, III
6.1 (d)	I													8, I	6.1, I	6.1, I	6.1, I	6.1, I	6.1, I
6.1 (o)	I													8, I	6.1, I	6.1, I	6.1, I	6.1, I	6.1, I
6.1 (l)	II													8, I	6.1, II	6.1, II	6.1, II	6.1, II	6.1, II
6.1 (d)	II													8, I	6.1, I	8, II	6.1, II	6.1, II	6.1, II
6.1 (o)	II													8, I	8, I	8, II	6.1, II	6.1, II	6.1, II
6.1	III													8, I	8, I	8, II	8, II	8, III	8, III



Based on Toxicity – Gases

- Threshold Quantities for Toxic Vapors

Zones	Inhalation Toxicity	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Hazard Zone A	LC ₅₀ less than or equal to 200 ppm	5 kg (11 lb)	0.5 kg (1.1 lb)	0.5 kg (1.1 lb)	0.25 kg (0.55 lb)
Hazard Zone B	LC ₅₀ greater than 200 ppm and less than or equal to 1000 ppm	25 kg (55 lb)	2.5 kg (5.5 lb)	2.5 kg (5.5 lb)	1.25 kg (2.75 lb)
Hazard Zone C	LC ₅₀ greater than 1000 ppm and less than or equal to 3000 ppm	100 kg (220 lb)	10 kg (22 lb)	10 kg (22 lb)	5 kg (11 lb)
Hazard Zone D	LC ₅₀ greater than 3000 ppm or less than or equal to 5000 ppm	200 kg (440 lb)	20 kg (44 lb)	20 kg (44 lb)	10 kg (22 lb)



Based on Toxicity – Liquids

- V is the saturated vapor concentration in air of the material in mL/m^3 at $20\text{ }^\circ\text{C}$ and standard atmospheric pressure.
- Volatility V_i is given by
- $$V_i = P_i \times \frac{10^6}{101.3} \text{ mL}/\text{m}^3$$
- Where, P_i is vapor pressure in kPa at $20\text{ }^\circ\text{C}$ and standard atmospheric pressure.

Zones	Vapor concentration and toxicity	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Hazard Zone A	$V \geq 500 \text{ LC}_{50}$ and $\text{LC}_{50} \leq 200 \text{ mL}/\text{m}^3$	5 kg (11 lb)	0.5 kg (1.1 lb)	0.5 kg (1.1 lb)	0.25 kg (0.55 lb)
Hazard Zone B	$V \geq 10 \text{ LC}_{50}$; $\text{LC}_{50} \leq 1000 \text{ mL}/\text{m}^3$; and the criteria for Packing Group I, Hazard Zone A are not met.	25 kg (55 lb)	2.5 kg (5.5 lb)	2.5 kg (5.5 lb)	1.25 kg (2.75 lb)
Packing Group II	$V \geq \text{LC}_{50}$; $\text{LC}_{50} \leq 3000 \text{ mL}/\text{m}^3$; and the criteria for Packing Group I, are not met.	1000 kg (2200 lb)	100 kg (220 lb)	100 kg (220 lb)	50 kg (110 lb)
Packing Group III	$V \geq 0.2 \text{ LC}_{50}$; $\text{LC}_{50} \leq 5000 \text{ mL}/\text{m}^3$; and the criteria for Packing Group I and II, are not met.	2000 kg (4400 lb)	200 kg (440 lb)	200 kg (440 lb)	100 kg (220 lb)



Based on Oral, Dermal and Inhalation of mists and dusts

- Threshold Quantities for Oral, Dermal and Inhalation mists and dusts

Oral Toxicity LD50 (mg/kg)	Dermal Toxicity LD50 (mg/kg)	Inhalation mists and dusts LC50 (mg/L)	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Less than equal to 5	Less than equal to 50	Less than equal 0.2	500 kg (1100 lb)	50 kg (110 lb)	50 kg (110 lb)	25 kg (55 lb)
Greater than 5 and less than equal to 50	Greater than 50 and less than equal to 200	Greater than 0.2 and less than equal to 2	1000 kg (2200 lb)	100 kg (220 lb)	100 kg (220 lb)	50 kg (110 lb)
Greater than 50 and less than equal to 300	Greater than 200 and less than equal to 1000	Greater than 2 and less than equal to 4	2000 kg (4400 lb)	200 kg (440 lb)	200 kg (440 lb)	100 kg (220 lb)



Based on Flammability

- Threshold Quantities for flammability

Description	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Flammable gases				
Liquids with normal boiling point less than 35 °C (95 °F) and flash point less than 23 °C (73 °F)	500 kg (1100 lb)	50 kg (110 lb)	50 kg (110 lb)	25 kg (55 lb)
Liquids with normal boiling point greater than 35 °C (95 °F) and flash point less than 23 °C (73 °F)	1000 kg (2200 lb)	100 kg (220 lb)	100 kg (220 lb)	50 kg (110 lb)
Liquids with flash point greater than equal to 23 °C (73 °F) and less than and equal to 60 °C (140 °F)	2000 kg (4400 lb)	200 kg (440 lb)	200 kg (440 lb)	100 kg (220 lb)
Liquids with flash point greater than 60 °C (140 °F) released at a temperature at or above flash point				
Liquids with flash point greater than 60 °C (140 °F) and less than equal to 93 °C (200 °F) released at a temperature below flash point	N/A	N/A	1000 kg (2200 lb)	500 kg (1100 lb)



Based on Crude Oil

- Threshold Quantities for Crude Oil

Description	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Crude oil less than equal to 15 API Gravity (unless actual flash point available)	1000 kg (2200 lb)	100 kg (220 lb)	100 kg (220 lb)	50 kg (110 lb)
Crude oil greater than 15 API Gravity (unless actual flash point available)	2000 kg (4400 lb)	200 kg (440 lb)	200 kg (440 lb)	100 kg (220 lb)

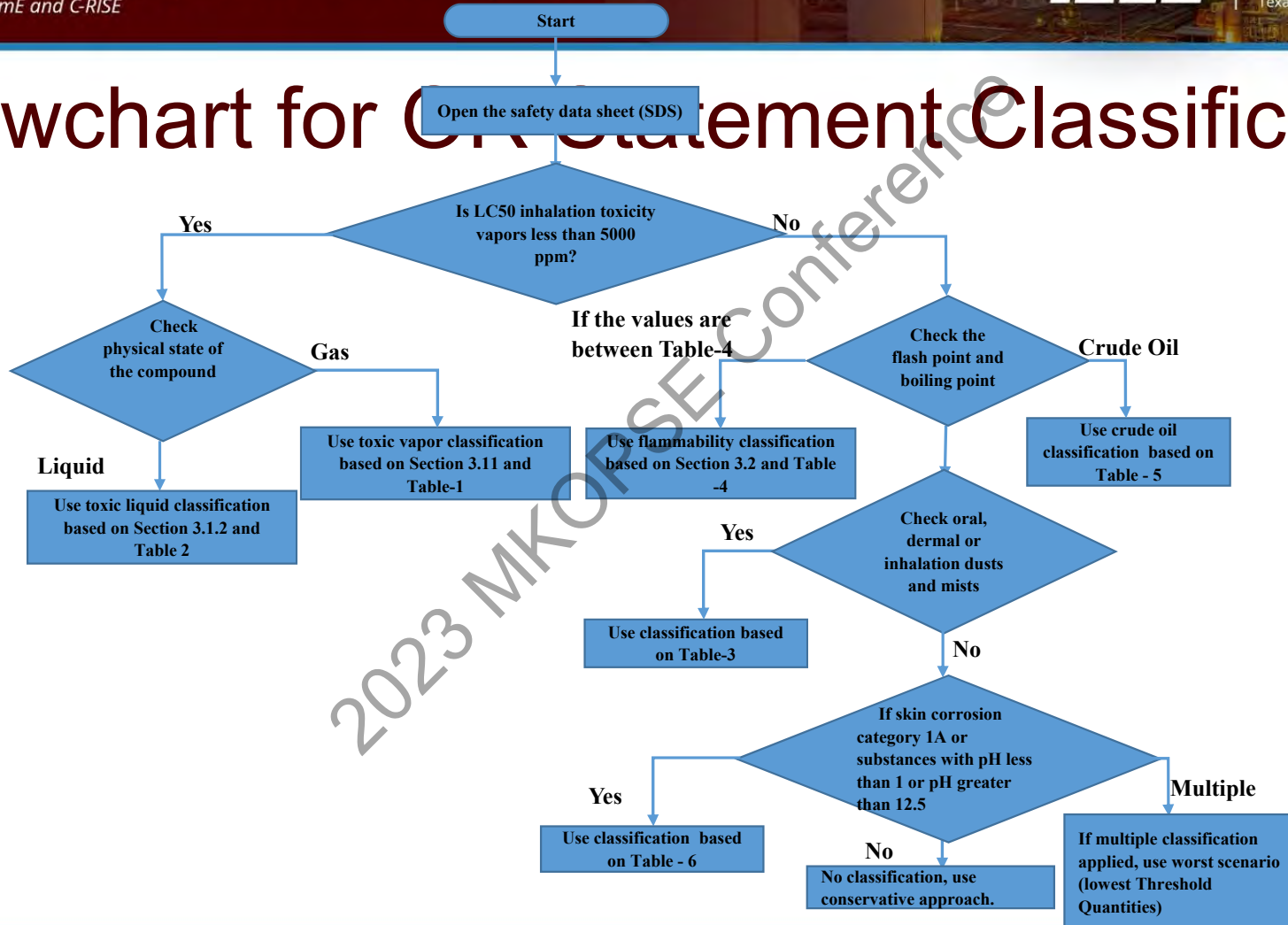
Based on Corrosivity

- Threshold Quantities for Corrosivity

Description	Threshold Quantities for Tier-1 (Outdoor)	Threshold Quantities for Tier-1 (Indoor)	Threshold Quantities for Tier-2 (Outdoor)	Threshold Quantities for Tier-2 (Indoor)
Strong acids/bases, (substances with GHS Skin Corrosion Category 1A (exposure less than equal to 3 minutes during an observation period less than equal than 1 hour) or substances with pH less than 1 or pH greater than 12.5	N/A	N/A	1000 kg (2200 lb)	500 kg (1100 lb)



Flowchart for GHS Statement Classification





Example for OR Statement Usage

Styrene

Source of MSDS: fishersci [9]

Step -1: Check the toxic LC50 Inhalation

LC50 = 11.7 mg/L

LC50 = 2746.66 ppm

We should use toxic liquid as the physical state is liquid

Pi = 7 mbar = 0.7 kPa

$$V_i = 0.7 \times \frac{10^6}{101.3} = 6910.17 \text{ mL/m}^3$$

$V_i > \text{LC50}$, $\text{LC50} < 3000$

So,

Tier I (Outdoor) = 1000 kg (2200 lb)

Tier I (Indoor) = 100 kg (220 lb)

Tier II (Outdoor) = 100 kg (220 lb)

Tier II (Indoor) = 50 kg (110 lb)

Methanol

Source: Pioneer Forensics [10]

Step -1: Check the toxic LC50 Inhalation

LC50 = 81778.67 ppm for 4 hrs

LC50 > 5000 ppm

Step-2: Check the boiling point and flash point

Boiling point = 64.7 °C

Flash point = 12 °C

Using flammability classification

Tier I (Outdoor) = 1000 kg (2200 lb)

Tier I (Indoor) = 100 kg (220 lb)

Tier II (Outdoor) = 100 kg (220 lb)

Tier II (Indoor) = 50 kg (110 lb)

Sodium Hydroxide

Source of MSDS: DCM Shriram [11]

Step -1: Check the toxic LC50 Inhalation

LC50 = Not available

Step-2: Check the boiling point and flash point

Boiling point = Not available

Flash point = Not available

Step-3: Check the oral, dermal and inhalation dusts and mists

Oral, dermal and inhalation dusts and mists = Not available

Step-4: Check pH and skin corrosivity category

pH = 13 to 14

Using corrosivity classification

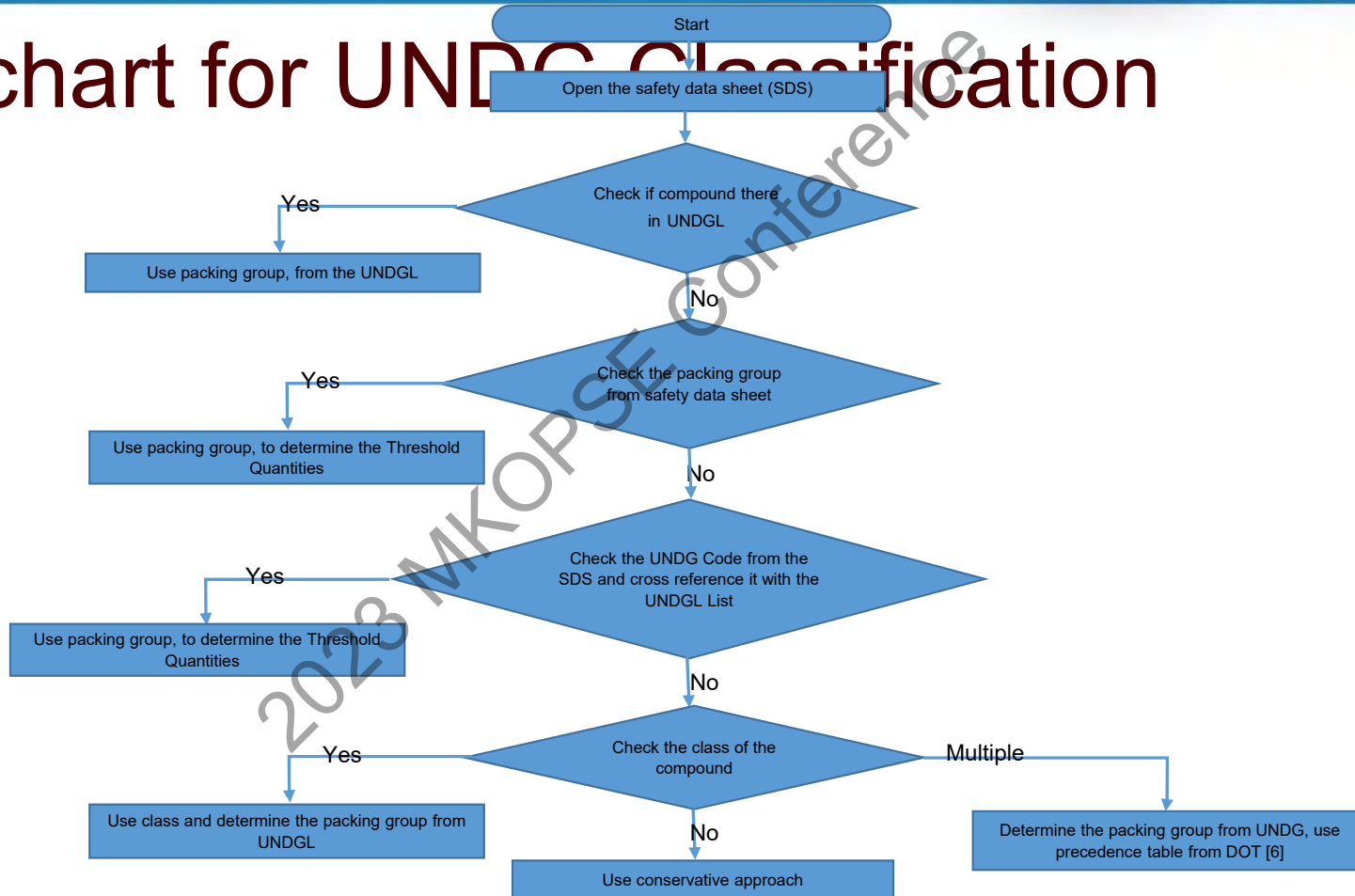
Tier I (Outdoor) = NA

Tier I (Indoor) = NA

Tier II (Outdoor) = 1000 kg (2200 lb)

Tier II (Indoor) = 500 kg (1100 lb)

Flowchart for UNDG Classification





Example for UNDG Classification

Methanol

2055	STYRENE MONOMER, STABILIZED	3	III	5L	E1	P001	T2	TP1
2056	TETRAHYDROFURAN	3	II	1L	E2	P001	T4	TP1

Source: Pioneer Forensics [10]

Step -1: Check if the compound there in UNDG

It is classified in Class 3, Packing Group III

So
Tie

TABLE 3.10.A
 Precedence of Hazards and Packing Groups for Classes 3, 4 and 8 and for Divisions 5.1 and 6.1 (3.10.1)

Class or Division	Packing Group	4.2		4.3		5.1		6.1		8		8		8		8	
		II	III	I	II	I	II	I	II	I	II	I	II	I	II	I	II
3	I*			4.3, I	4.3, I	4.3, I	—	—	—	3, I	3, I	3, I	3, I	3, I	—	—	—
3	II*			4.3, I	4.3, II	4.3, II	—	—	—	3, I	3, I	3, II	3, II	8, I	—	—	3, II
3	III*			4.3, I	4.3, II	4.3, III	—	—	—	6.1, I	6.1, I	6.1, II	3, III*	8, I	—	—	3, III
4.1	II*	4.2, II	4.2, II	4.3, I	4.3, II	4.3, II	5.1, I	4.1, II	4.1, II	6.1, I	6.1, I	4.1, II	4.1, II	8, I	—	4.1, II	4.1, II
4.1	III*	4.2, II	4.2, III	4.3, I	4.3, II	4.3, III	5.1, I	4.1, II	4.1, III	6.1, I	6.1, I	6.1, II	4.1, III	8, I	—	8, II	4.1, III
4.2	II			4.3, I	4.3, II	4.3, II	5.1, I	4.2, II	4.2, II	6.1, I	6.1, I	4.2, II	4.2, II	8, I	4.2, II	4.2, II	4.2, II
4.2	III			4.3, I	4.3, II	4.3, III	5.1, I	5.1, II	4.2, III	6.1, I	6.1, I	6.1, II	4.2, III	8, I	8, I	8, II	8, II
4.3	I						5.1, I	4.3, I	4.3, I	6.1, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I	4.3, I
4.3	II						5.1, I	4.3, II	4.3, II	6.1, I	4.3, II	4.3, II	4.3, II	8, I	8, I	4.3, II	4.3, II
4.3	III						5.1, I	5.1, II	4.3, III	6.1, I	5.1, I	5.1, I	4.3, III	8, I	8, I	8, II	8, II
5.1	I						5.1, I	5.1, I	5.1, I	6.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I	5.1, I
5.1	II						5.1, I	5.1, I	5.1, I	6.1, I	5.1, I	5.1, I	5.1, I	8, I	8, I	5.1, II	5.1, II
5.1	III						5.1, I	5.1, I	5.1, I	6.1, I	5.1, I	5.1, I	5.1, I	8, I	8, I	5.1, II	5.1, II
6.1 (d)	I													8, I	6.1, I	6.1, I	6.1, I
6.1 (o)	I													8, I	6.1, I	6.1, I	6.1, I
6.1 (j)	II													8, I	6.1, I	6.1, II	6.1, II
6.1 (d)	II													8, I	6.1, I	8, II	6.1, II
6.1 (o)	II													8, I	8, I	8, II	6.1, II
6.1	III													8, I	8, I	8, II	8, III

Let us assume, the packing group is not there in the SDS as well

Step-3: Check the class the compound

Source of MSDS: Sigma Aldrich [12]

Class of methanol 3, packing group II and 6.1 packing group II

Based on Precedence Table [6], Class 3 Packing Group II is preferred

So,

Tier I (Outdoor) = 1000 kg (2200 lb)

Tier I (Indoor) = 100 kg (220 lb)

Tier II (Outdoor) = 100 kg (220 lb)

Tier II (Indoor) = 50 kg (110 lb)



Example for UNDG Classification

Sodium Hydroxide

1823	SODIUM HYDROXIDE, SOLID	8		II
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Step -1: Check if the compound there in UNDG

In this case, refer to the physical properties if solid or vapor and then decide the packing group. Here let us assume its solid

It is classified has packing group II

So,

Tier I (Outdoor) = 1000 kg (2200 lb)

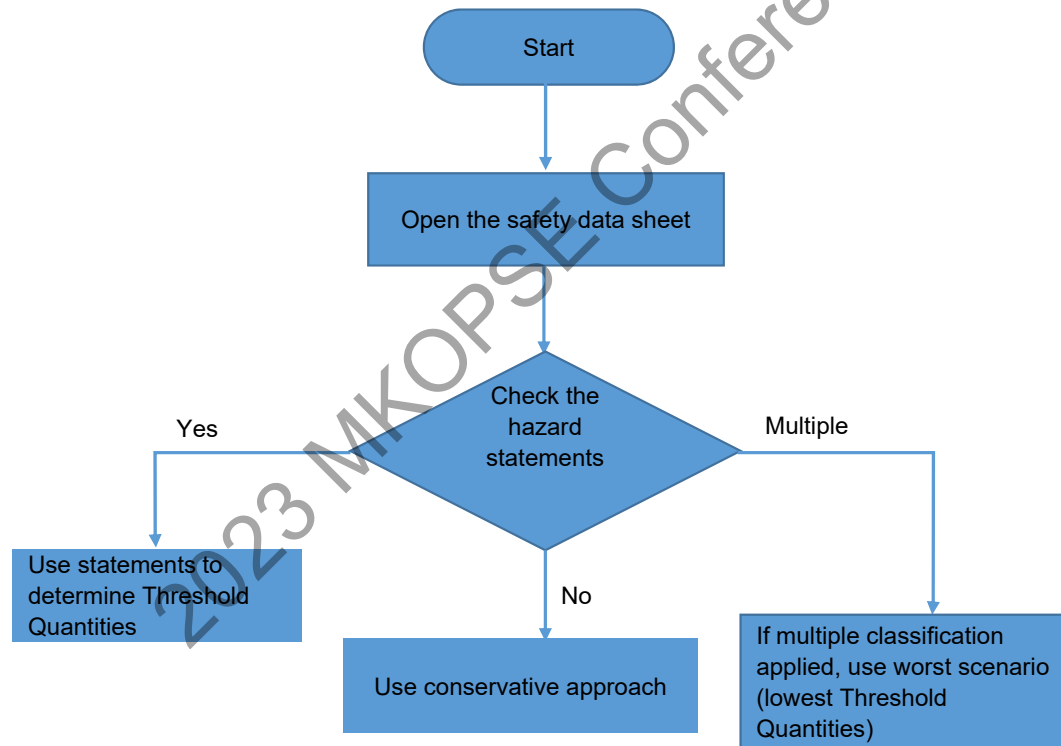
Tier I (Indoor) = 100 kg (220 lb)

Tier II (Outdoor) = 100 kg (220 lb)

Tier II (Indoor) = 50 kg (110 lb)

	3.1.2	2.0	2.0	2.0.1.3	3.3	3.4	3.5
1824	SODIUM HYDROXIDE SOLUTION	8		III	223	5 L	E1

Flowchart for GHS Classification





Example for GHS

Styrene

Source of MSDS: eChem Portal [13]

The hazard statements are

H226 – Flammable Liquid Category 3

H315 – Skin Irritation Category 2

H319 - Eye Irritation Category 2

H332 - Acute Toxicity Category 4

Based on the hazard statements H332 - Acute Toxicity Category 4, is having the lowest threshold quantities

So,

Tier I (Outdoor) = 200 kg (440 lb)

Tier I (Indoor) = 20 kg (44 lb)

Tier II (Outdoor) = 20 kg (44 lb)

Tier II (Indoor) = 10 kg (22 lb)

Methanol

Source of MSDS: eChem Portal [14]

The hazard statements are

H225 – Flammable Liquid Category 2

H301 – Acute Toxicity Category 3

H311 - Acute Toxicity Category 3

H331 - Acute Toxicity Category 3

Based on the hazard statements H331 - Acute Toxicity Category 3, is having the lowest threshold quantities

So,

Tier I (Outdoor) = 100 kg (220 lb)

Tier I (Indoor) = 10 kg (22 lb)

Tier II (Outdoor) = 10 kg (22 lb)

Tier II (Indoor) = 5 kg (11 lb)

Sodium Hydroxide

Source of MSDS: eChem Portal [15]

The hazard statements are

H314 – Skin Corrosion Category 1A

H319 – Eye Irritation Category 2

H315 – Skin Irritation Category 2

Based on the hazard statements H314 - Skin Corrosion Category 1A, is having the lowest threshold quantities

So,

Tier I (Outdoor) = NA

Tier I (Indoor) = NA

Tier II (Outdoor) = 1000 kg (2200 lb)

Tier II (Indoor) = 500 kg (1100 lb)



Conclusion

Compounds	OR Statement	United Nations Dangerous Goods Packing Group, UN/DGL	GHS Method
Styrene	Tier I (Outdoor) = 1000 kg (2200 lb)	Tier I (Outdoor) = 2000 kg (4400 lb)	Tier I (Outdoor) = 200 kg (440 lb)
	Tier I (Indoor) = 100 kg (220 lb)	Tier I (Indoor) = 200 kg (440 lb)	Tier I (Indoor) = 20 kg (44 lb)
	Tier II (Outdoor) = 100 kg (220 lb)	Tier II (Outdoor) = 200 kg (440 lb)	Tier II (Outdoor) = 20 kg (44 lb)
	Tier II (Indoor) = 50 kg (110 lb)	Tier II (Indoor) = 100 kg (220 lb)	Tier II (Indoor) = 10 kg (22 lb)
		Assumption 1 – Based on the MSDS	
		Tier I (Outdoor) = 2000 kg (4400 lb)	
		Tier I (Indoor) = 200 kg (440 lb)	
		Tier II (Outdoor) = 200 kg (440 lb)	
Methanol	Tier I (Outdoor) = 1000 kg (2200 lb)	Tier I (Outdoor) = 1000 kg (2200 lb)	Tier I (Outdoor) = 100 kg (220 lb)
	Tier I (Indoor) = 100 kg (220 lb)	Tier I (Indoor) = 100 kg (220 lb)	Tier I (Indoor) = 10 kg (22 lb)
	Tier II (Outdoor) = 100 kg (220 lb)	Tier II (Outdoor) = 100 kg (220 lb)	Tier II (Outdoor) = 10 kg (22 lb)
	Tier II (Indoor) = 50 kg (110 lb)	Tier II (Indoor) = 50 kg (110 lb)	Tier II (Indoor) = 5 kg (11 lb)
		Assumption 1 – Based on the MSDS	
		Tier I (Outdoor) = 1000 kg (2200 lb)	
		Tier I (Indoor) = 100 kg (220 lb)	
		Tier II (Outdoor) = 100 kg (220 lb)	
		Tier II (Indoor) = 50 kg (110 lb)	
		Assumption 2 - Based on the class	
	Tier I (Outdoor) = 1000 kg (2200 lb)		
	Tier I (Indoor) = 100 kg (220 lb)		
	Tier II (Outdoor) = 100 kg (220 lb)		
	Tier II (Indoor) = 50 kg (110 lb)		
Sodium Hydroxide	Tier I (Outdoor) = NA	Tier I (Outdoor) = 1000 kg (2200 lb)	Tier I (Outdoor) = NA
	Tier I (Indoor) = NA	Tier I (Indoor) = 100 kg (220 lb)	Tier I (Indoor) = NA
	Tier II (Outdoor) = 1000 kg (2200 lb)	Tier II (Outdoor) = 100 kg (220 lb)	Tier II (Outdoor) = 1000 kg (2200 lb)
	Tier II (Indoor) = 500 kg (1100 lb)	Tier II (Indoor) = 50 kg (110 lb)	Tier II (Indoor) = 500 kg (1100 lb)



Conclusion

- Based on the three approaches, a company has to use a consistent approach for all the compounds.
- Choosing the Safety Data Sheet (SDS) is the key factor, company should use an appropriate safety data sheet during the process of classification.
- Company has to decide a conservative approach for the classification.
- Above table shows that different Threshold Quantities can be obtained when using the various approaches.
- The GHS classification is most conservative due to the lower threshold values.
- Companies dealing with many coded/special chemicals with global operations must determine the best classification method and consistent so that they can obtain proper process safety metrics across various sites.



Thank You

Hema Divya – khdivya@gmail.com

Rahul Raman – rahul@kaypear.com

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The work of the Gulf Research Program in offshore safety

MKO Process Safety & Risk Conference

11 October 2023

Hallie Graham

*Jim Pettigrew, CAPT, USN (Ret),
Board Director*

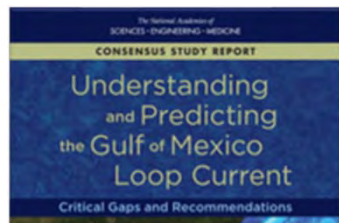


THE NATIONAL ACADEMIES OF SCIENCES, ENGINEERING, AND MEDICINE

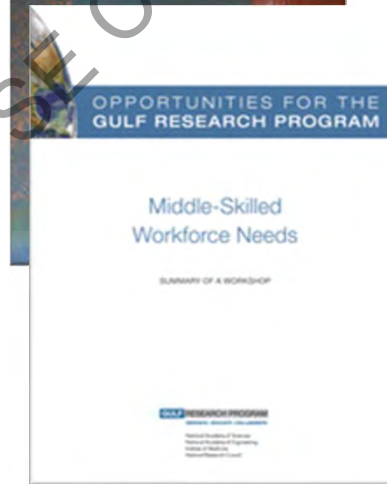
- Advisors to the Nation on sciences, engineering, and medicine.
- NAS created in 1863 under Lincoln Administration.
- Non-profit, non-governmental organization
- The National Academies is the umbrella term for NAS, NAE, and NAM.
- Strengths of our work:
 - Independence
 - Scientific objectivity
 - Balance



CONSENSUS STUDIES & WORKSHOPS

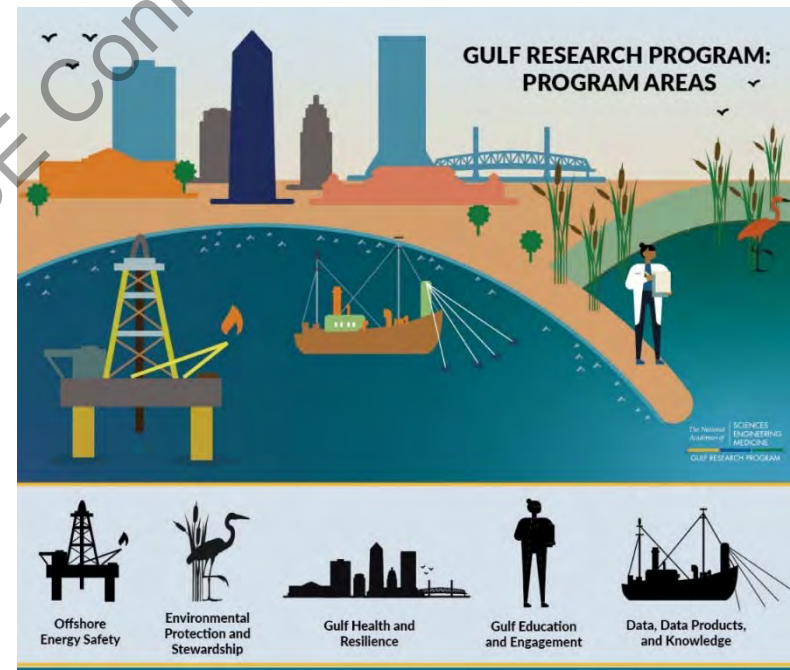


The National Academies of SCIENCES - ENGINEERING - MEDICINE

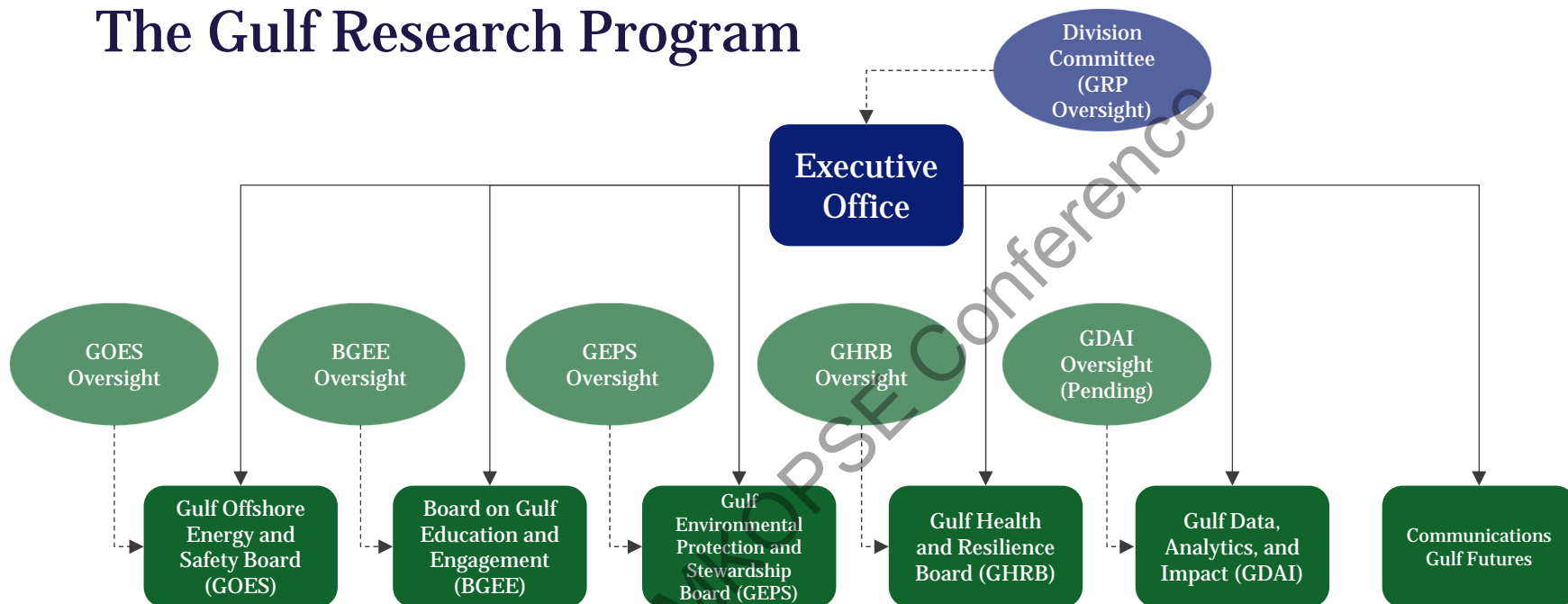


THE GULF RESEARCH PROGRAM (GRP)

- A 30-year program (2013 - 2043) managed by the National Academies.
- Funds research grants, fellowships, studies, and other activities.
- Operate in five areas:
 - Offshore energy safety
 - Environmental protection and stewardship
 - Human health and resilience
 - Education and engagement
 - Data, analysis, and information



The Gulf Research Program



Offshore Energy Safety Board

Contribute to the reduction of systemic risk across offshore energy activities



...issues concerning the safety of offshore oil drilling and hydrocarbon {*Energy*} production and transportation in the Gulf of Mexico and on the United States' outer continental shelf.

NATIONAL Sciences
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GULF RESEARCH PROGRAM

GOES BOARD

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The overarching goal for the GRP's Offshore Energy Safety (GOES) program area is to contribute to the management of systemic risk and improve operational safety for offshore energy activities. Additionally, lead GRP efforts related to the Energy Transition

Learning...



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GULF RESEARCH PROGRAM

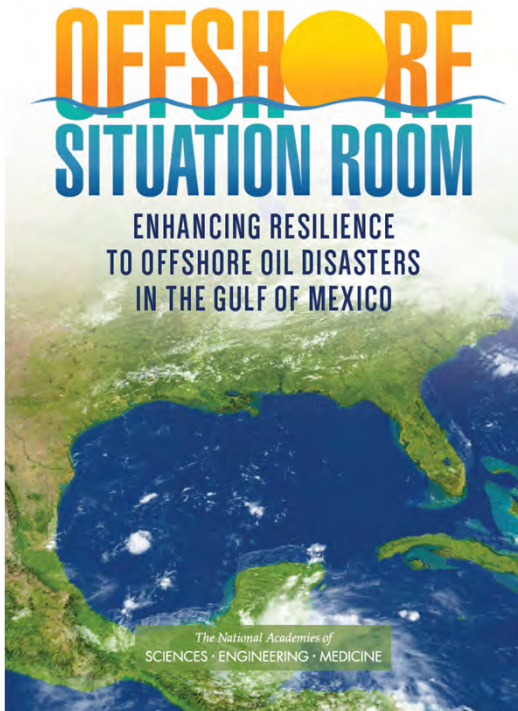
Learning through Serious Games...

NATIONAL ACADEMIES Sciences
Engineering
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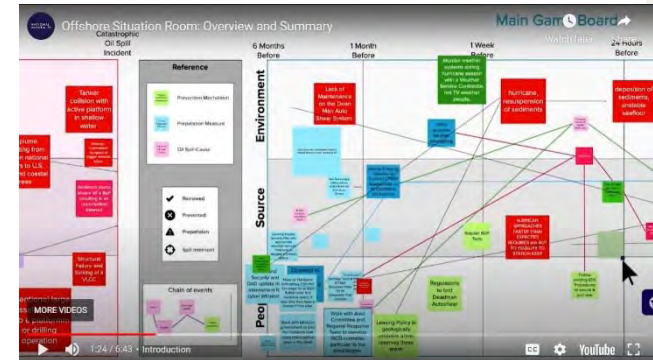
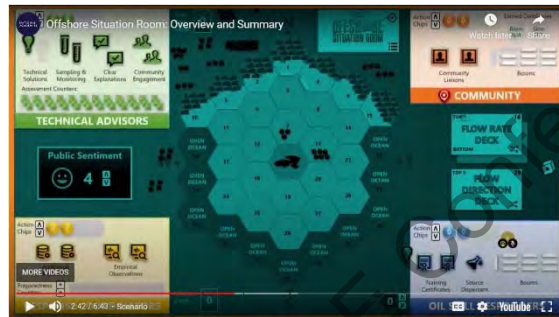
GULF RESEARCH PROGRAM

Oil Spill response and restoration...

PROCEEDINGS OF A WORKSHOP



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Navigating the Energy Transition in the Gulf of Mexico, a Workshop

- How do we achieve 2050 goals?
- Bring together diverse stakeholders
- Look for GRP opportunities



Fellowships



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Early-Career Research Fellows:

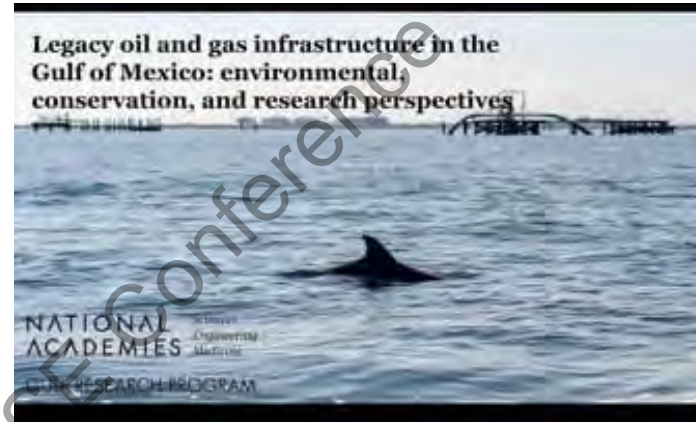
- Receive two years of funding to pursue innovative research paths
- Connect with a network of researchers across disciplines
- Build research skills and confidence with the support of a mentor

Science Policy Fellows:

- Gain a year of hands-on experience alongside decision-makers in the Gulf of Mexico region
- Connect with a network of colleagues at their host office
- Build skills with professional development opportunities and the guidance of a mentor

Legacy Infrastructure, Decommissioning...

- Legacy Infrastructure
 - End of service life of platforms and structures
 - Abandoned pipelines
 - Transition to enabling new energy sources
- Decommissioning
 - Meeting of Experts, 14-15 September, Houston, TX

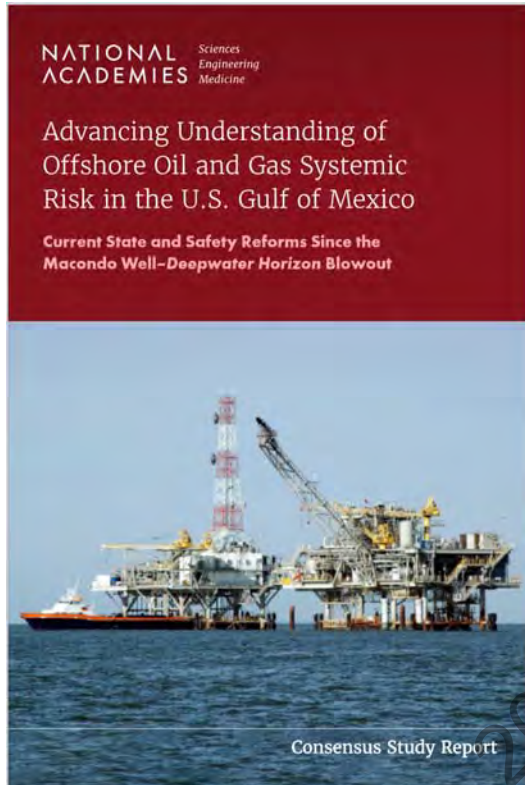


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GULF RESEARCH PROGRAM

Safer Offshore Energy Systems (SOES) Grants

- Previous SOES Grants (~\$20M)
 - Advancing Safety Culture in the Offshore Oil and Gas Industry
 - Preventing the Next Spill: Understanding Systemic Risk in the Offshore Oil and Gas Environment
 - Scenario Planning to Advance Safety Culture and Minimize Risk in Offshore Oil and Gas Operations
 - Exploring Approaches for Effective Education and Training of Workers in the Offshore Oil and Gas Industry and Health Professions
- Current SOES Grants (~\$5M)
 - Evolution of Offshore Energy Safety Management Systems
- Future SOES efforts
 - Reduction of risk during offshore oil and gas decommissioning activities
 - Increasing awareness of leading indicators and barrier health through artificial intelligence and machine learning

Consensus Study



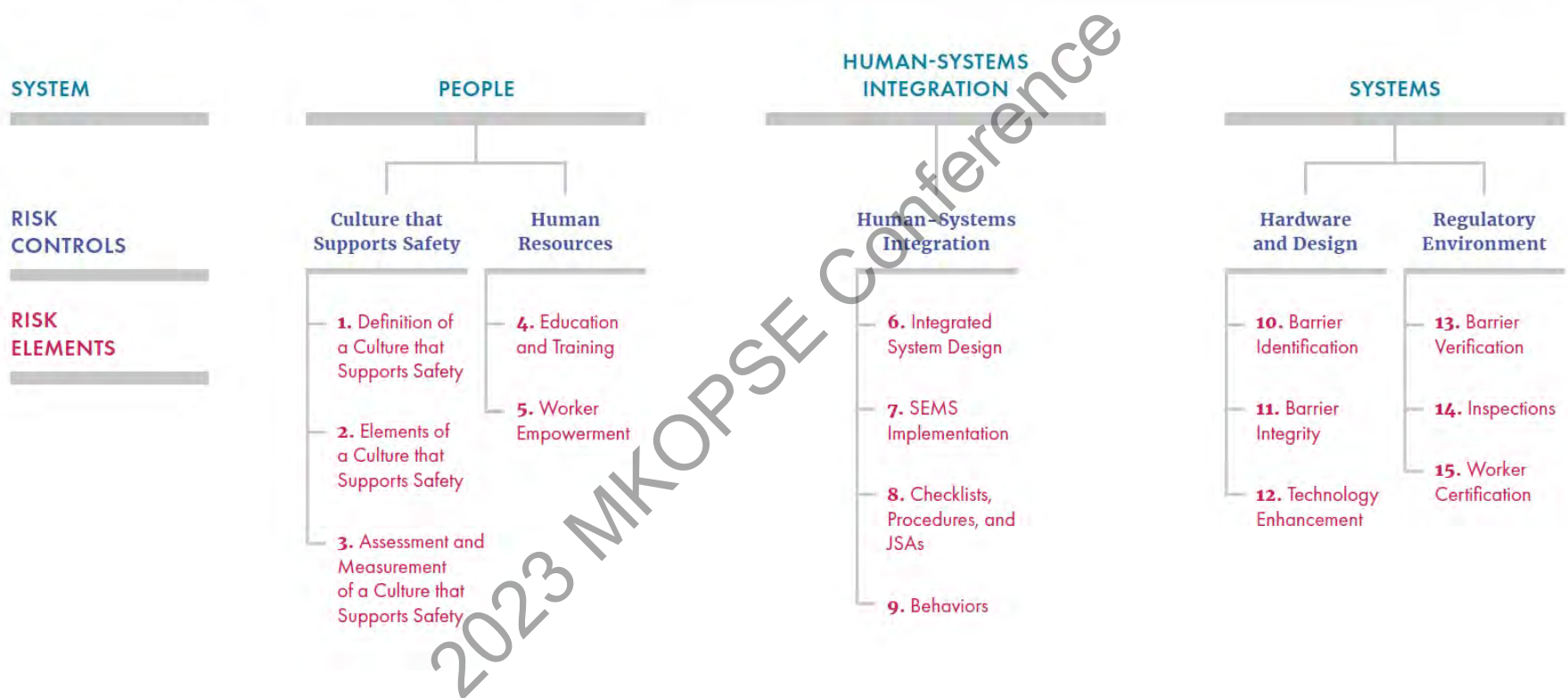
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The Gulf Research Program and Offshore Energy Safety • Jim Pettigrew

- Define the current profile of systemic risks of offshore oil and gas operations in the Gulf of Mexico.
- Assess the impact of technological, regulatory, environmental, organizational, and process changes.
- Consider the impact of the regulatory structure.
- Assess the impact and potential of GRP.

RISK PROFILE FOR OFFSHORE OIL AND GAS



Moving forward into the future of the Gulf of Mexico



Questions?

Jim Pettigrew
jpettigrew@nas.edu

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Safe and Sustainable Energy Transition



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78th Annual Instrumentation and Automation Symposium





Securing Industrial Control Systems

Implementing Zero Trust Architecture in OT Environments



That's the way we've always done it...

- *“The most damaging phrase in the language is ‘We’ve always done it this way’.”*
 - Rear Admiral Grace Murray Hopper – Developer for COBOL coding language
- How many times do we say this phrase to justify work processes and other actions? Is it safe just because “nothing bad happened before?”
- Alternative is Continuous Improvement
 - Turn the question around: **“Why do we do it this way?”**



Speaker profile

wood.

- Brad Mozisek
 - OPA COE Program Manager/Automation and Control Lead
 - Brad has over 15 years of experience in the Refining, Oil and Gas, Chemical, Offshore and Onshore industries. Brad currently manages Wood's Center of Excellence for OPA. This includes utilizing experience across multiple DCS systems to develop technical solutions including application libraries, sample architectures and technology stacks.

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Implicit Trust to Zero Trust

2023 MKO'CONNOR Conference

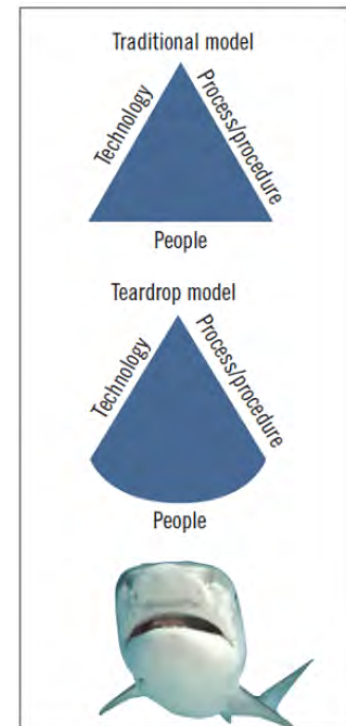
Most common model in OT Today - Quick overview

- **Trusted Connections - Implicit Trust**
 - Perimeter based/Castle and Moat
- Rapidly changing threat base
 - Foundations for trusted Connections are not as stable as the past



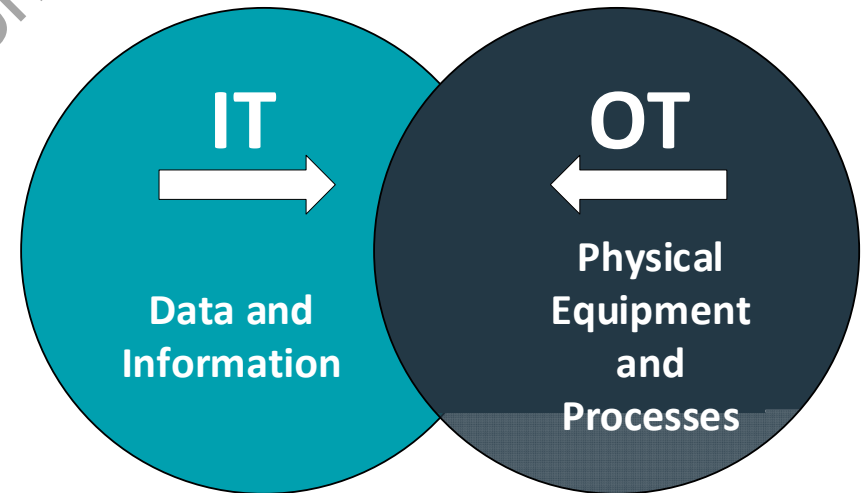
From Implicit trust to Zero Trust

- Zero Trust - Assuming no user or device trust by default
 - As technology advances, People may be the weakest link in security
- “Never Trust, Always Verify”
- Continual re-validation of credentials based on profiles, actions and other information.
 - Least privileged access at any given time.
- Figure: Brad Bonnette - Wood



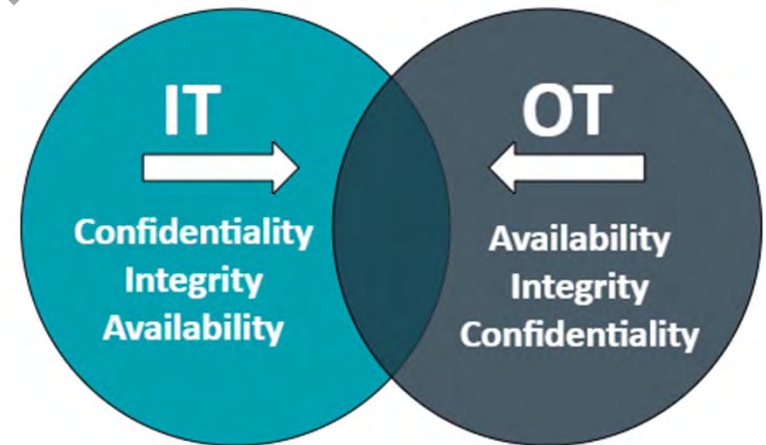
Bringing in IT and other Solutions to OT

- Not entirely new concepts - Online banking and other industries utilizes premises of ZTA today.
- Higher degree of implementation in more IT centric Areas



Bringing in IT and other Solutions to OT

- CIA vs AIC models – Conflicting Interests to always keep in mind
 - Unlike purely digital domains, cyber-attacks in OT environments can have immediate physical consequences.
 - Compromised industrial systems can lead to equipment damage, production disruptions, and even safety hazards.





Long Journey – Not overnight trip

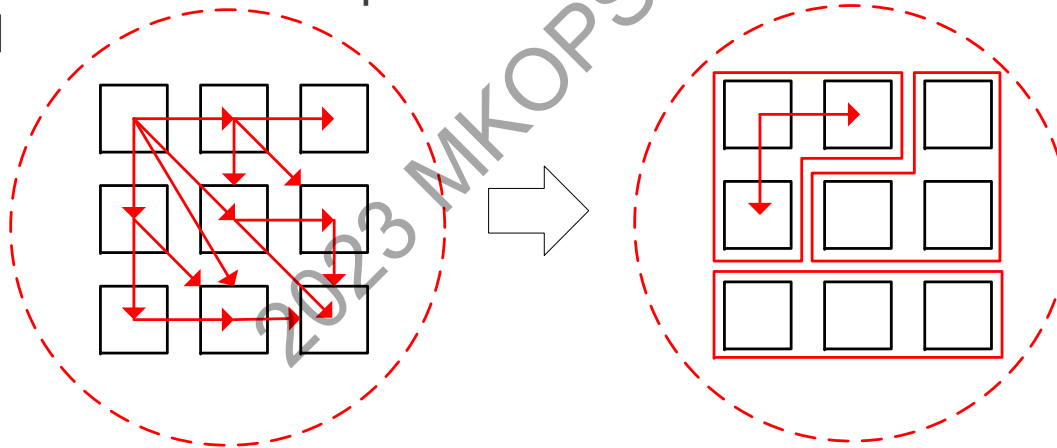
- CISA – Zero Trust Maturity Model – Version 2.0 – April 2023
- Similar to the safety journey - S84/61511
- Iterative

Figure: CISA Zero Trust Maturity Model Version 2.0, April 2023

	Identity	Devices	Networks	Applications and Workloads	Data
Optimal	<ul style="list-style-type: none"> • Continuous validation and risk analysis • Enterprise-wide identity integration • Tailored, as-needed automated access 	<ul style="list-style-type: none"> • Continuous physical and virtual asset analysis including automated supply chain risk management and integrated threat protections • Resource access depends on real-time device risk analytics 	<ul style="list-style-type: none"> • Distributed micro-perimeters with just-in-time and just-enough access controls and proportionate resilience • Configurations evolve to meet application profile needs • Integrates best practices for cryptographic agility 	<ul style="list-style-type: none"> • Applications available over public networks with continuously authorized access • Protections against sophisticated attacks in all workflows • Immutable workloads with security testing integrated throughout lifecycle 	<ul style="list-style-type: none"> • Continuous data inventorying • Automated data categorization and labeling enterprise-wide • Optimized data availability • DLP exfil blocking with security testing integrated throughout lifecycle • Encrypts data in use
Advanced	<ul style="list-style-type: none"> • Phishing-resistant MFA • Consolidation and secure integration of identity stores • Automated identity risk assessments • Need/session-based access 	<ul style="list-style-type: none"> • Most physical and virtual assets are tracked • Enforced compliance implemented with integrated threat protections • Initial resource access depends on device posture 	<ul style="list-style-type: none"> • Expanded isolation and resilience mechanisms • Configurations adapt based on automated risk-aware application profile assessments • Encrypts applicable network traffic and manages issuance and rotation of keys 	<ul style="list-style-type: none"> • Most mission critical applications available over public networks to authorized users • Protections integrated in all application workflows with context-based access controls • Coordinated teams for development, security, and operations 	<ul style="list-style-type: none"> • Automated data inventory with tracking • Consistent, tiered, targeted categorization and labeling • Redundant, highly available data stores • Static DLP • Automated context-based access • Encrypts data at rest
Initial	<ul style="list-style-type: none"> • MFA with passwords • Self-managed and hosted identity stores • Manual identity risk assessments • Access expires with automated review 	<ul style="list-style-type: none"> • All physical assets tracked • Limited device-based access control and compliance enforcement • Some protections delivered via automation 	<ul style="list-style-type: none"> • Initial isolation of critical workloads • Network capabilities manage availability demands for more applications • Dynamic configurations for some portions of the network • Encrypt more traffic and formalize key management policies 	<ul style="list-style-type: none"> • Some mission critical workflows have integrated protections and are accessible over public networks to authorized users • Formal code deployment mechanisms through CI/CD pipelines • Static and dynamic security testing prior to deployment 	<ul style="list-style-type: none"> • Limited automation to inventory data and control access • Begin to implement a strategy for data categorization • Some highly available data stores • Encrypts data in transit • Initial centralized key management policies
Traditional	<ul style="list-style-type: none"> • Passwords or MFA • On-premises identity stores • Limited identity risk assessments • Permanent access with periodic review 	<ul style="list-style-type: none"> • Manually tracking device inventory • Limited compliance visibility • No device criteria for resource access • Manual deployment of threat protections to some devices 	<ul style="list-style-type: none"> • Large perimeter/macro-segmentation • Limited resilience and manually managed rulesets and configurations • Minimal traffic encryption with ad hoc key management 	<ul style="list-style-type: none"> • Mission critical applications accessible via private networks • Protections have minimal workflow integration • Ad hoc development, testing, and production environments 	<ul style="list-style-type: none"> • Manually inventory and categorize data • On-prem data stores • Static access controls • Minimal encryption of data at rest and in transit with ad hoc key management

Granular security – least privilege

- Building point from IEC 62443 -
- Building on zones and conduits down to micro-segmentation
 - Self Contained attack protection – Block attacks before they spread



Best laid plans...


- Today's state of the art is tomorrow open attack vector
- ZTA will not prevent all threats, but continuous improvement can limit any potential damage to systems.
- Monitor and analyze network activity: Set up continuous monitoring of network traffic and user/device behavior, using tools like Security Information and Event Management (SIEM) systems or network traffic analysis software.
- Automate response and remediation: Develop automated response mechanisms to **quickly identify** and **remediate** security threats or policy violations



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Moving Forward Technology Adoption/Adaptation

2023 MKORSE Conference



How do we move forward?

- Incremental Journey with many milestones, not a single large jump.
 - Every step decreased risk – Refer back to CISA Zero Trust Security Model transitions.
- End users/Stakeholders need to continue to engage partnerships – Many existing players in the game today. Workshops along the journey.
 - Assessing Current state of Security
 - Auditing/analyzing OT risk vectors
 - Vendors and integrators need to continue innovate
 - Problem analysis to develop solutions
 - Not solution creation to find problems.
 - CHAZOPs



How do we move forward? – Technology Adoption

- Technology partners within system for secure access, Multi-factor Authentication (MFA, First steppingstone toward ZTA) and Intrusion detection
 - Many partners exist in this space today – Experts in bridging security gaps into the OT spaces
- Secure by Design technology adoption through standards-based technology and protocols
 - Open Process Automation Standards (O-PAS)
 - OPC-UA (adopting full encryption/security paths)
 - IEC 61499 – Event Based programming



O-PAS – Secure by Design

- Open (Not open source!) Standards allow for continuous improvement through new technologies – “Standard of Standards”
 - Hardware solutions
 - Software solutions
 - Communication protocols
- Ability to incorporate latest technology to improve security.
- Allows integration with legacy systems while maintaining isolation for security.



Expanding segmentation within OT – Application and HMI

- Technology adoption – adaptation
- Expanding security focus from just systems basis
 - Further focus on application and HMI security for **Least Privileges** approach. Does not exist in most cases today.
 - Does HMI need full time write access to parameters?



Expanding segmentation within OT – Application and HMI

- Ex. Just in time authentication based on operator actions for changing PV or setpoint.
 - Was the request legitimate? Did the request come from a (currently) trust source – Trust needs to be constantly validated, including contextual needs.
 - Did the operator log in to an operator station, Is this a unit the operator is assigned to (We can already do this level)?
 - Secondary authentication with new technologies – robustness is a requirement to ensure reliability.
- **Must maintain operability** while balancing security needs

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Greg Hardin, CFSE

- 50 years as a process engineer, instrument and controls engineer, functional safety practitioner
- Half of career with multi-national chemical firm, half with various engineering firms and one safety system manufacturer
- Senior Principal Specialist with aeSolutions in Houston



greg.hardin@aesolutions.com



The Unrealized Potential of an Effective Safety Requirements Specification (SRS)

- It's a requirement of the ANSI/ISA-61511 and IEC-61511 standards
- The standards set out the required contents in some detail
- So, what's the problem?
- *It's completed after the fact*
- *It's not updated to reflect the final design*
- *It's filed away and forgotten*



IEC 61511-1

Edition 2.1 2017-08

FINAL VERSION

Functional safety – Safety instrumented systems for the process industry sector –
Part 1: Framework, definitions, system, hardware and application programming requirements



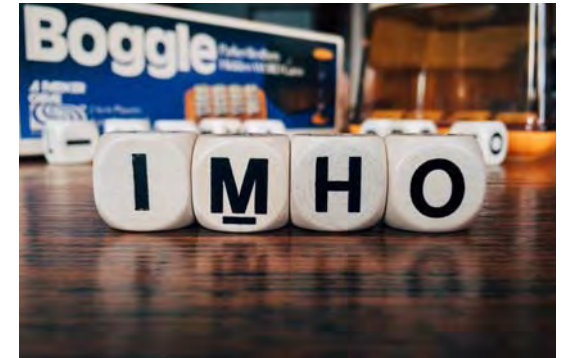
Why should you care?

If a project is following the 61511 standard then resources have been invested in creating the SRS. You want to obtain the maximum return on the investment.

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Acronyms

- SRS, Safety Requirements Specification
- SIS, Safety Instrumented System
- SIF, Safety Instrumented Function
- IPL, Independent Protection Layer
- MRT, Mean Repair Time
- MTTR, Mean Time To Restore
- 61511, ANSI/ISA 61511-1-2018 (AKA: IEC 61511)



What's in an SRS?

- The 2018 edition of the 61511 standard lists 29 items that make up an SRS
- The standard does not require that all 29 items be present for every Safety Instrumented Function (SIF), but if any are omitted it is good practice to include an explanation of why
- The standard does not require that the SRS be a single document
- There is also an application program SRS (APSRS)





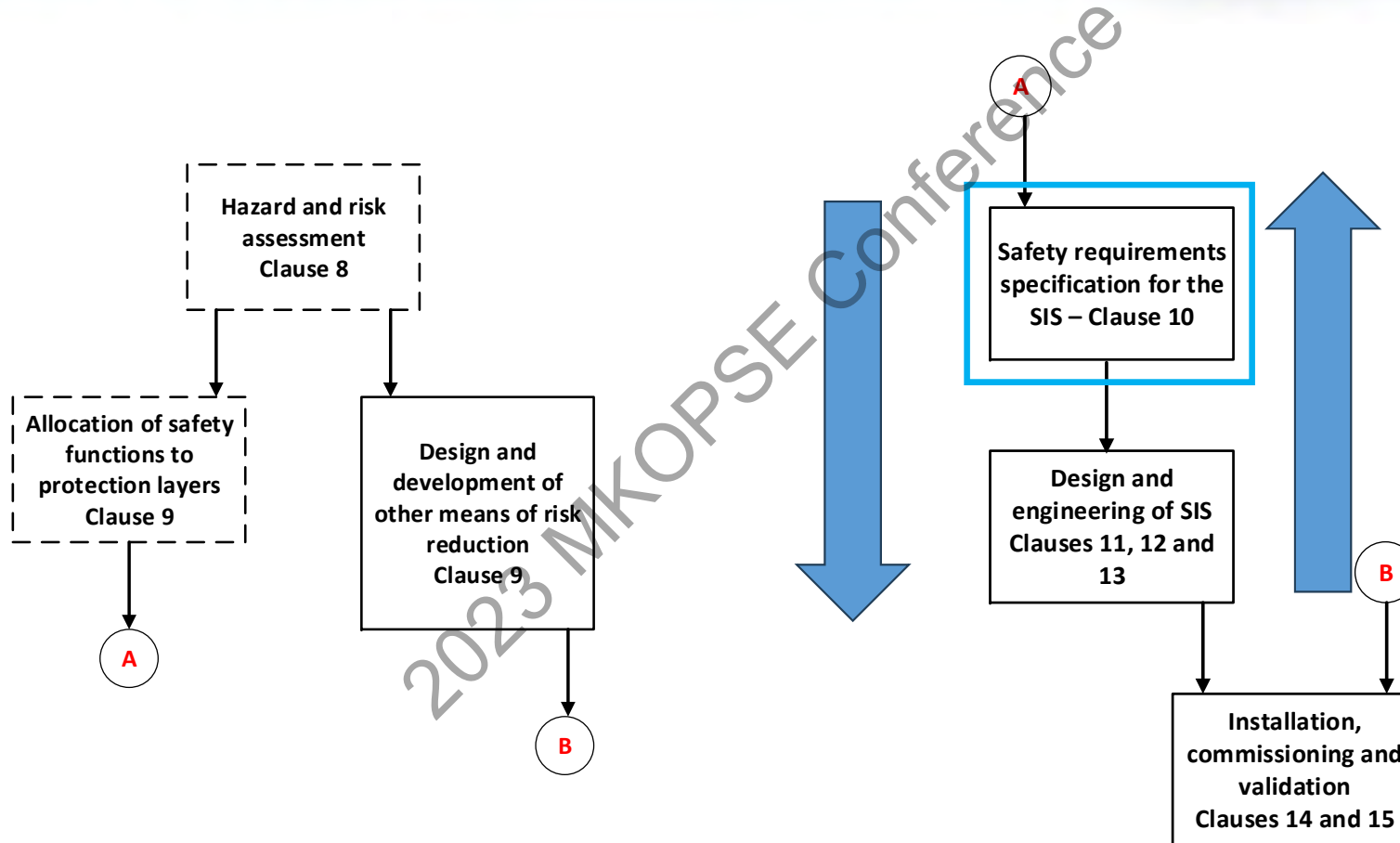
SRS contents

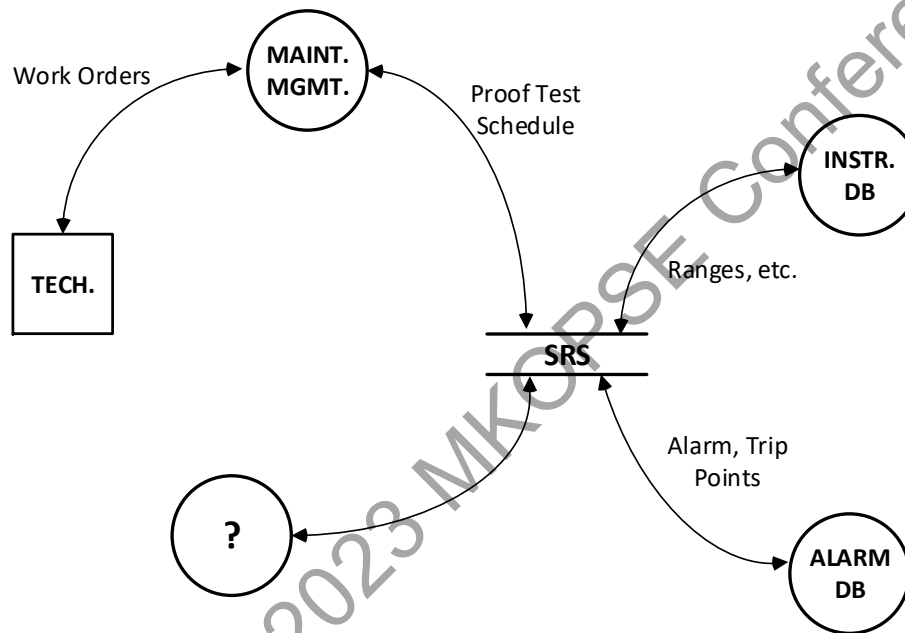
- SIF description
- field devices
- address common cause
- safe state of process
- concurrent safe states -> new hazard
- demands + demand rates
- proof test intervals
- proof test implementation
- response time
- required SIL, demand or continuous
- process measurements
- output actions
- outputs = fn(inputs)
- manual shutdown
- energize/de-energize
- reset
- spurious trip rate
- failure mode + response
- startup/shutdown
- SIS <-> other system interfaces



SRS contents (2)

- plant modes of operation
- application programming requirements
- bypass requirements
- actions in case of faults
- mean repair time
- dangerous combination of output states
- environmental conditions
- normal/abnormal process operating modes
- major accident survival







Problematic Entries

- Process safety time
 - Can be difficult to determine
 - Can significantly impact SIF design
- Hazardous combinations of SIF outputs
- Systematic capability of field devices
- Mission time (overhaul interval) – not one of the required items in the SRS
- Valve leakage requirements, valve closing time



Suggestions

- Put information that applies to most SIFs implemented in a single logic solver in a master document
- Have datasheets for each SIF that document the SIF-specific items and refer to the master document for common items (e.g. what signal from a 4-20mA instrument signifies out of range)
- Depending on the number of SIS logic solvers consider a hierarchy of SRS documents – e.g. site-wide, process unit, single SIS
 - The goal is avoid duplicating data



Questions





TEXAS A&M
UNIVERSITY

Dynamic Risk Assessment Model to Minimize Overall Operational Risks (Oil and Gas Industry)

Master Thesis by Abdullah Alsulieman



Outline

Literature Review

- DRA categories
- DRA studies in O&G industry
- Review findings
- Approach limitations

Proposed Model

- Offline phase
(Risk assessment)
- Online phase
(Dynamic Risk assessment)

Application (case study)

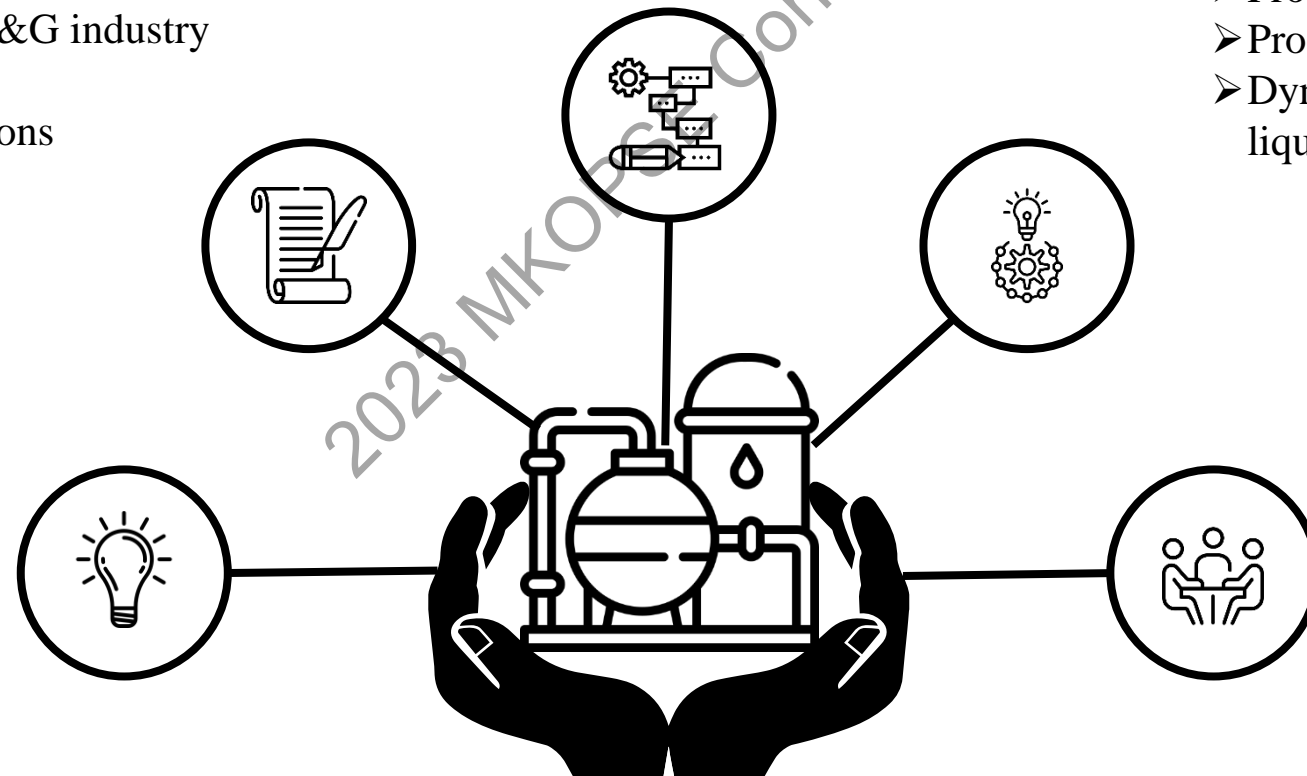
- Process selection
- Process description
- Dynamic risk assessment of liquid carryover

Introduction

- Concepts/Definitions
- Problem statement
- Research aim
- Justification

Discussion /Conclusion

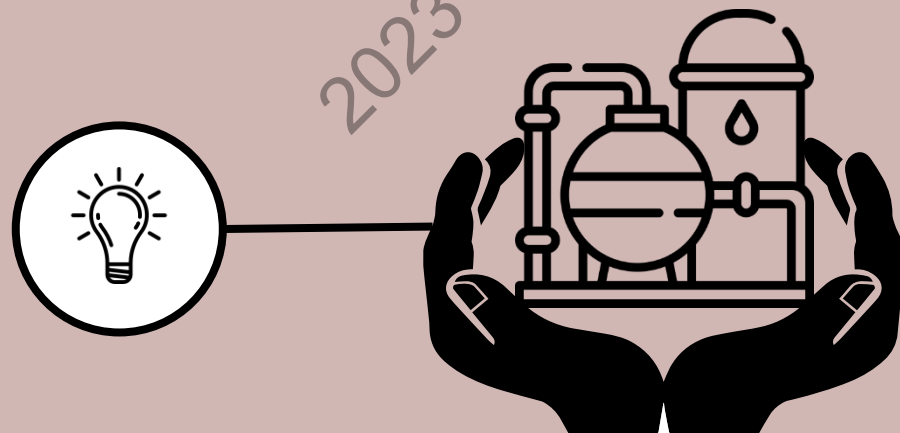
- Results
- Limitations
- Research objectives



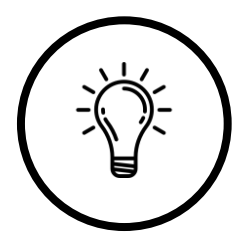
Outline

Introduction

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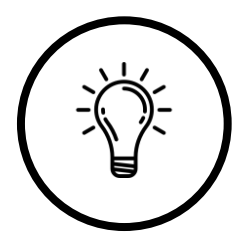
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Key Concepts and Definitions



- What can happen in the future (Rausand & Haugen, 2020)
- Identify, analyze and evaluate
- Update estimated risk of a deteriorated process (Khan et al., 2016)



Problem Statement

Conventional Risk Assessment

- **Static** in nature
- Do not consider **changes** in operations
- Often use **generic** failure data
- Can be **overwhelming**

(Zio, 2018)





Problem Statement



The existing DRA research in the O&G industry is mainly conducted based on: **Bayesian Network (BN)** or **Dynamic Bayesian Network (DBN)**

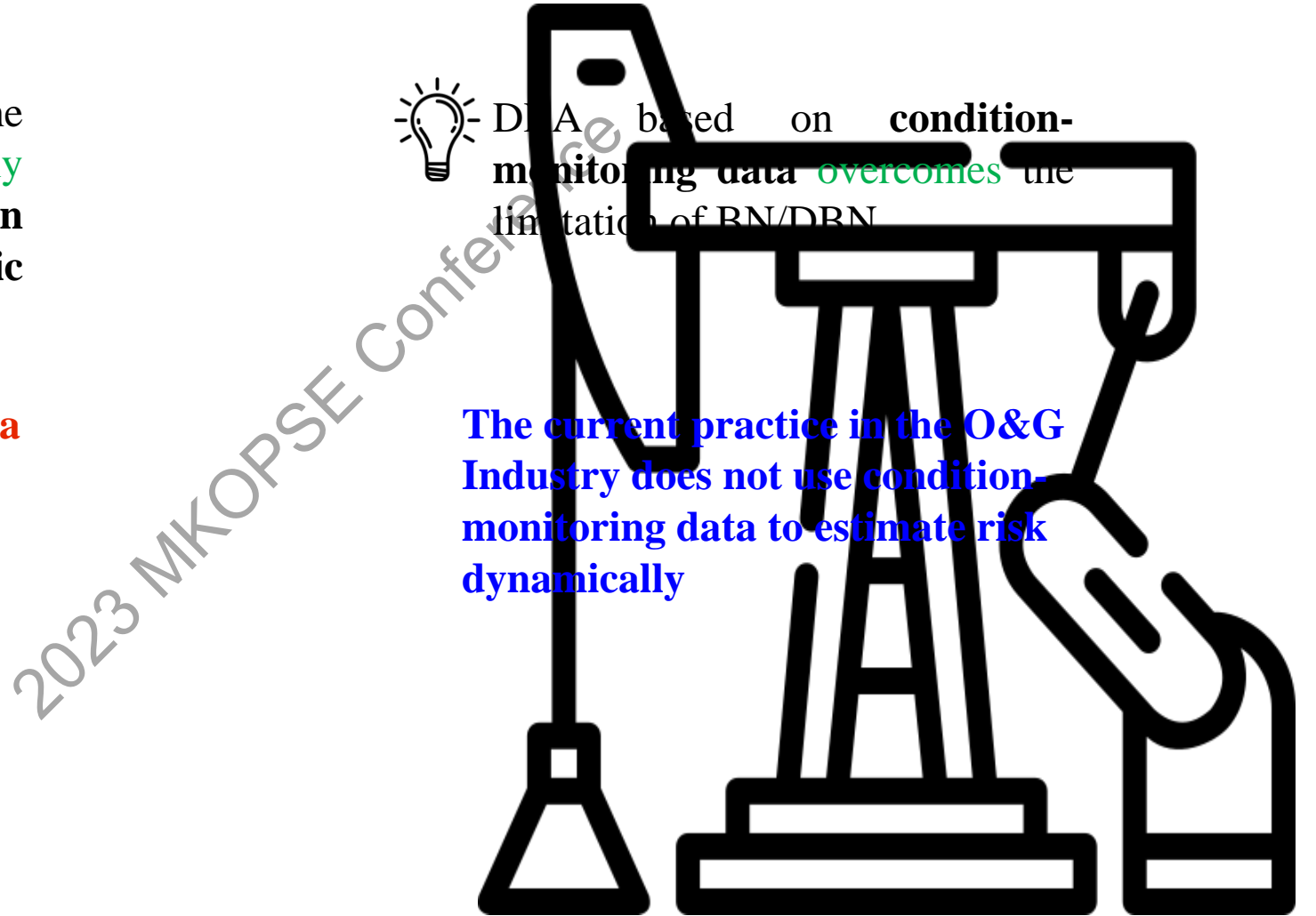


Require event-driven data to be updated, such as failure or accident data from similar systems



DRA based on **condition-monitoring data** **overcomes** the limitation of BN/DBN

The current practice in the O&G Industry does not use condition-monitoring data to estimate risk dynamically

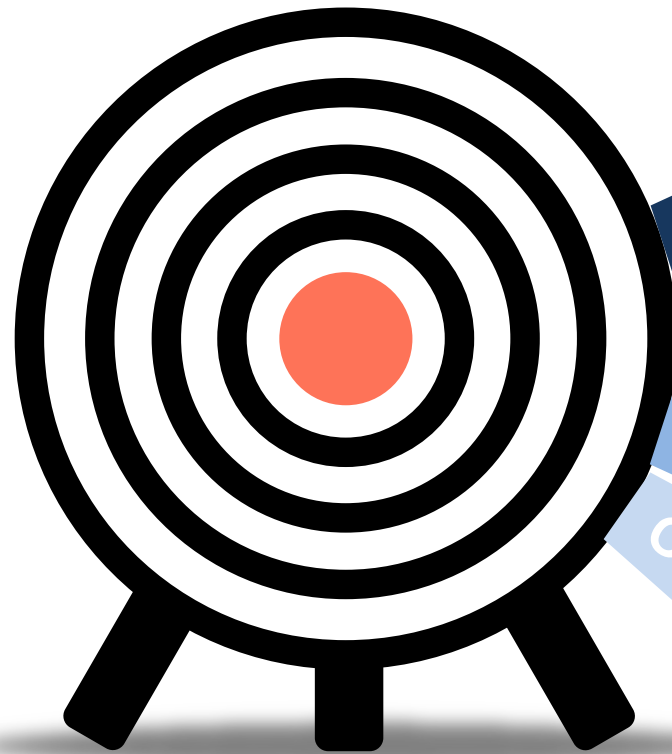




Research Aim

Aim

Apply a DRA technique to an O&G process unit based on condition-monitoring data.



Objective-1

To **contribute** to the development and application of the DRA techniques in the O&G industry

Objective-2

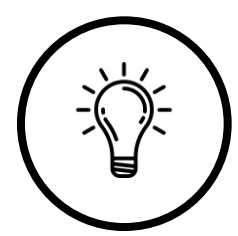
To **obtain the risk level** of an accident scenario in real-time

Objective-3

To **make informed decisions** based on inputs from the DRA technique

Objective-4

To **anticipate failures** of process safety barriers



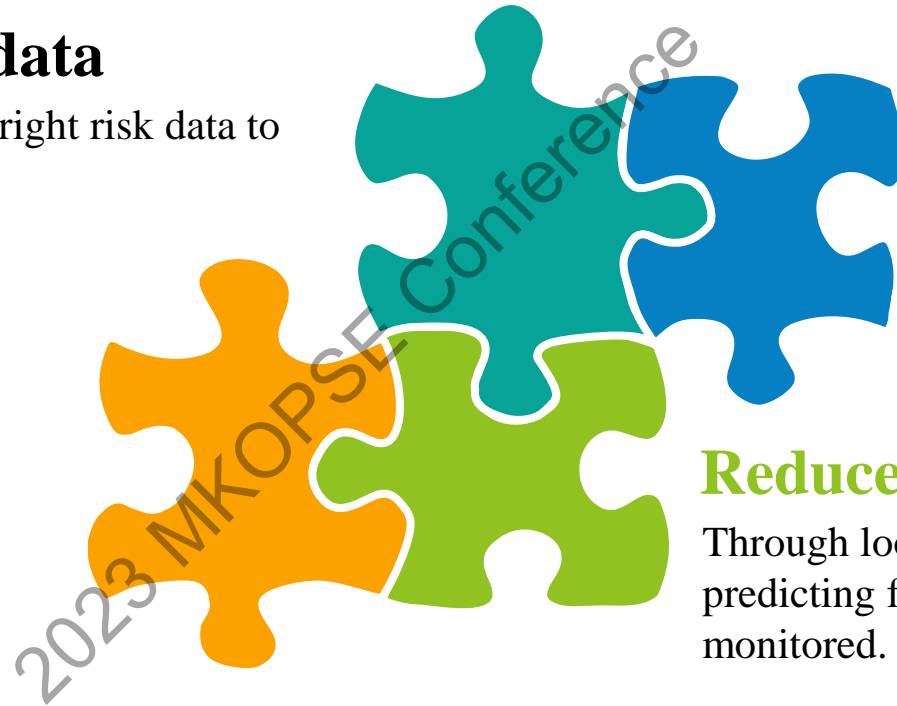
Justification

Obtain **high** certainty data

Operational personnel will have the right risk data to make informed decisions.

Implement the DRA at an oil and gas company

This study will contribute to the ongoing efforts to enhance the development and application of DRA techniques in the O&G industry by integrating conventional QRA methods with condition-monitoring data.



Optimize resources

Risk assessments can be time consuming; DRA will shift the resources to where they are needed the most.

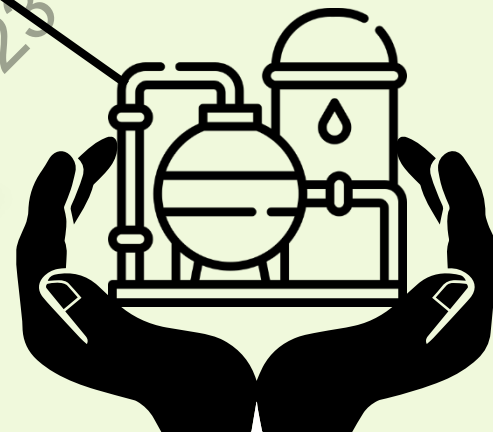
Reduce operational risks

Through looking into the future and predicting failure of safety barriers being monitored.

Outline

Literature Review

- DRA categories
- DRA studies in O&G industry
- Review findings
- Approach limitations



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DRA Categories

Data-based DRA

- Uses statistical failure data
 - *Counts of accidents, incidents, or near misses gathered from similar systems*
- Applies Bayesian theorem with conventional QRA
 - *FT, ET or BT*

Degradation-based DRA

- Employs condition monitoring data to overcome the constraints of the data-based DRA technique
- Focuses on accidents caused by degradation mechanisms such as wear, corrosion, and fracture formation

Process-based DRA

- Examines how process variables interact
- Risk rises when the monitored process parameters deviate from their ideal state
- Applies Bayesian network (BN) to identify dependencies



DRA Studies in the O&G Industry

Some existing DRA studies involving O&G process units include:

Cai et al. (2012)

Used BN methodology for QRA in offshore O&G

Bhandari et al. (2015)

Used BN for dynamic safety analysis in deep-water operations.

Khakzad et al. (2013)

Used BN for evaluating the safety of offshore drilling

Barua et al. (2016)

Converted DFT into DBN for risk assessment

L. Zhang et al. (2018)

Used DBNs in accident scenario analysis and dynamic quantitative risk assessment for managed pressure drilling safety.

Bijay et al. (2020)

Created a BN model to obtain the time dependent variations in kick effects using the real time failure probabilities of SB

Chen et al. (2020)

Developed a BN model of offshore drilling in order to minimize operational risks

Dimaio et al. (2021)

Proposed a multistate BN to model and assess the functional performance of safety barriers in oil and gas plants.



Literature Review Findings

- ❑ Many of the DRA techniques are **not widely applied** in the O&G industry
- ❑ DRA techniques are **practical** and **valid** in the O&G industry
- ❑ The DRA research in the O&G industry is **mainly conducted based on**:
 - Bayesian Networks (BNs)
 - Dynamic Bayesian Networks (DBNs)

DRA using condition-monitoring data **has not been widely applied** within the O&G industry

To bridge the gap, we develop a Dynamic Risk Assessment model based on condition-monitoring data that can be utilized to predict failures, estimate risk in real-time, and support informed decision-making



Limitations of the Approach

Incapable of **consequence assessment**

Ignores **statistical failure data**

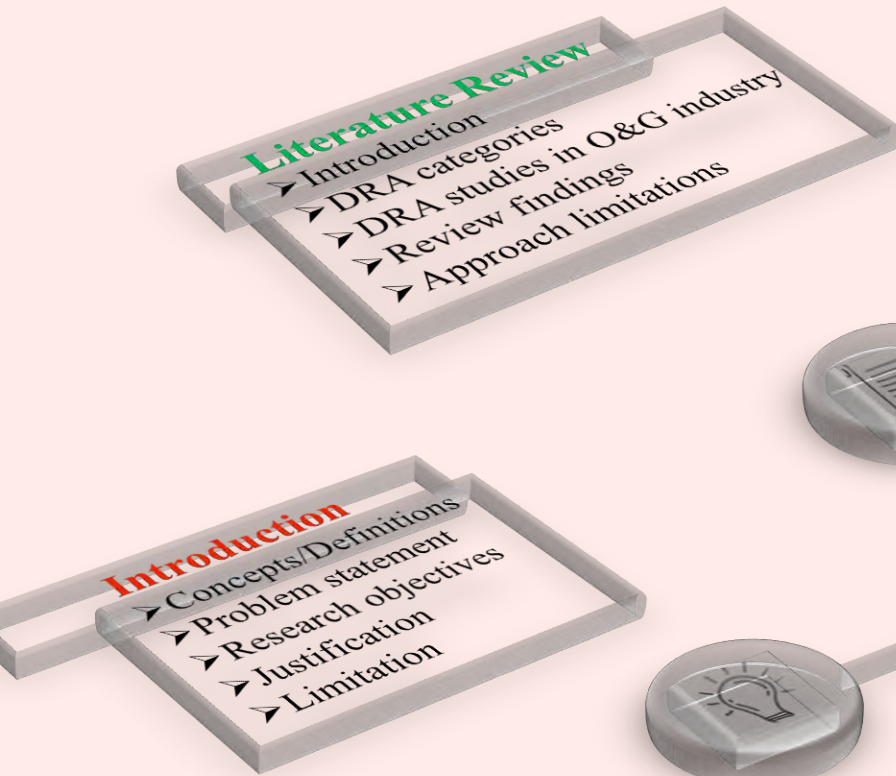
May produce **false positive** or **false negative** readings

Computational **issues**

High expertise in operations and data analysis techniques

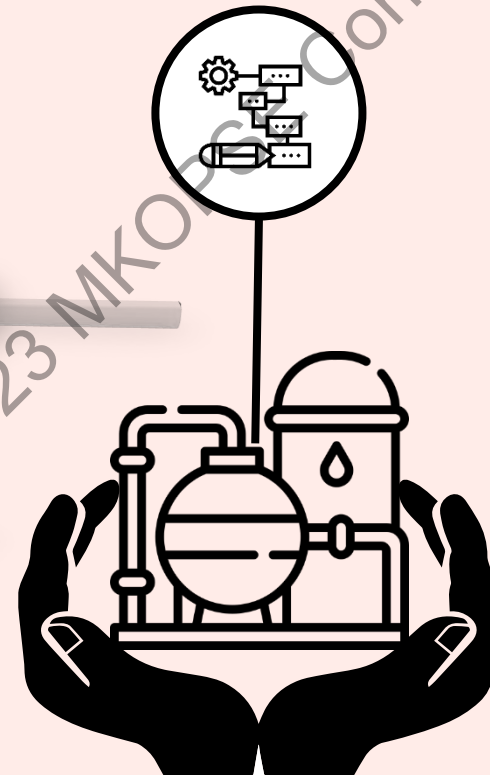


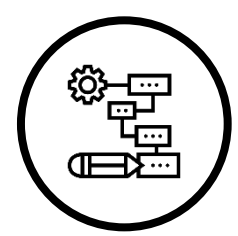
Outline



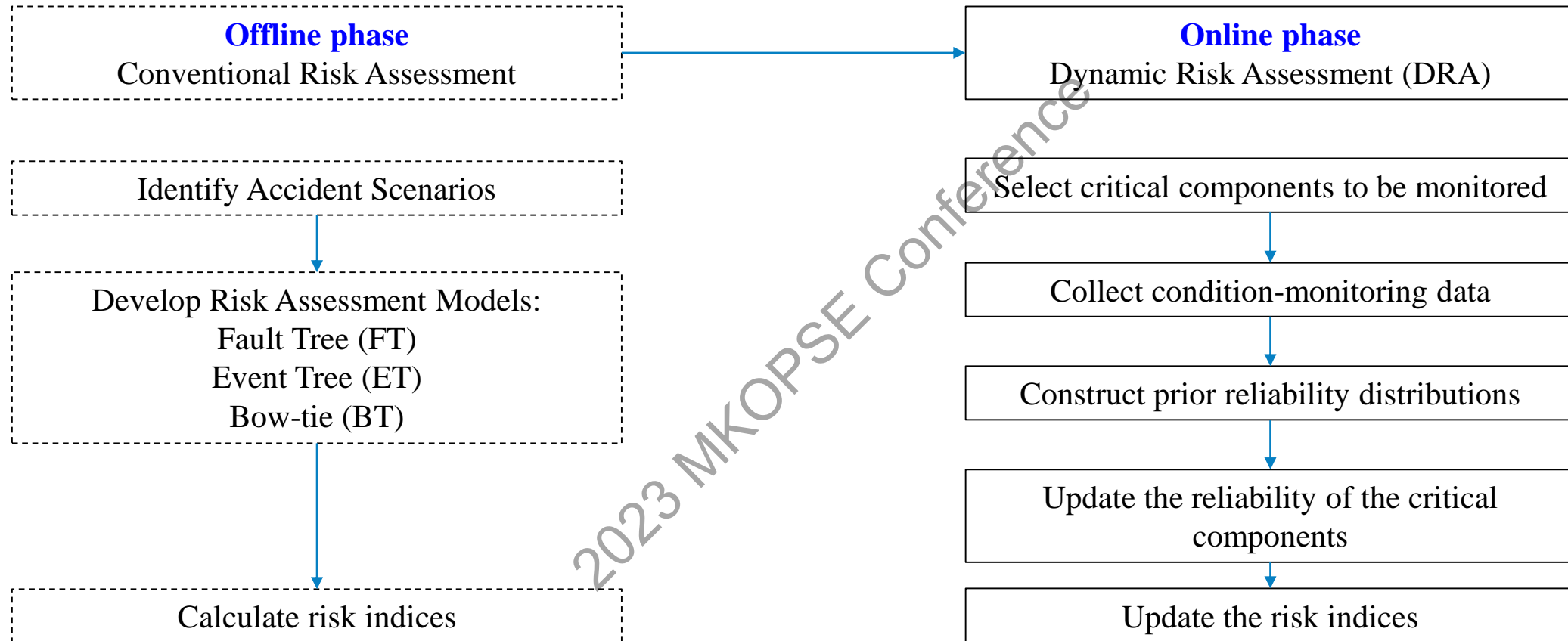
Proposed Model

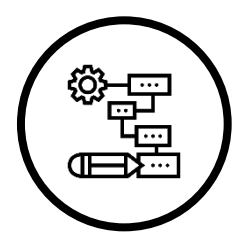
- Offline phase
(*Risk assessment*)
- Online phase
(*Dynamic Risk assessment*)



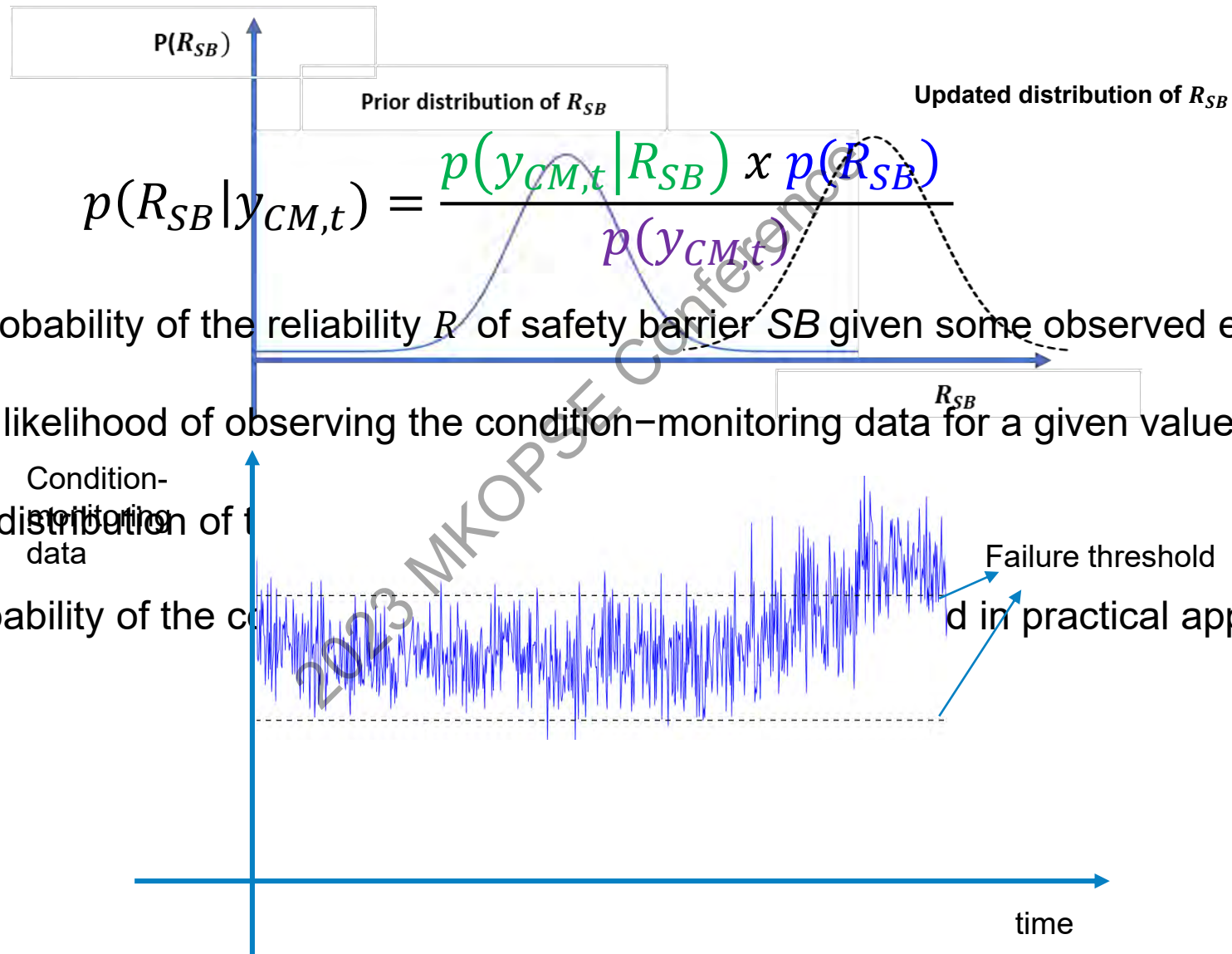


Steps of the Proposed DRA Model

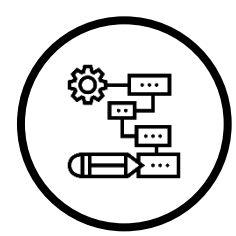




Online Phase



- $p(R_{SB} | y_{CM,t})$ the probability of the reliability R of safety barrier SB given some observed evidence y_{CM}
- $p(y_{CM,t} | R_{SB})$ is the likelihood of observing the condition-monitoring data for a given value of R_{SB}
- $p(R_{SB})$ is the prior distribution of the reliability of the safety barrier
- $p(y_{CM,t})$ is the probability of the condition-monitoring data



Online Phase

Algorithm 1. Dynamic reliability updating through Metropolis Sampling

Input: y_{CM}, t, n_s

Start: $p_{prop} = U(0,1), p_{prior} = p(R_{SB}), p^0 = \text{mean}(p_{prior}), k = 1$

Step 1: $p^{(k)} \leftarrow$ Generate a sample from p_{prop}

Step 2: Calculate $p_{acc} = \min\left(1, \frac{p(y_{CM}, t | p^{(k)}) p_{prior}(p^{(k)})}{p(y_{CM}, t | p^{(k-1)}) p_{prior}(p^{(k-1)})}\right)$

Step 3: $r \leftarrow$ Generate a sample from $U(0,1)$

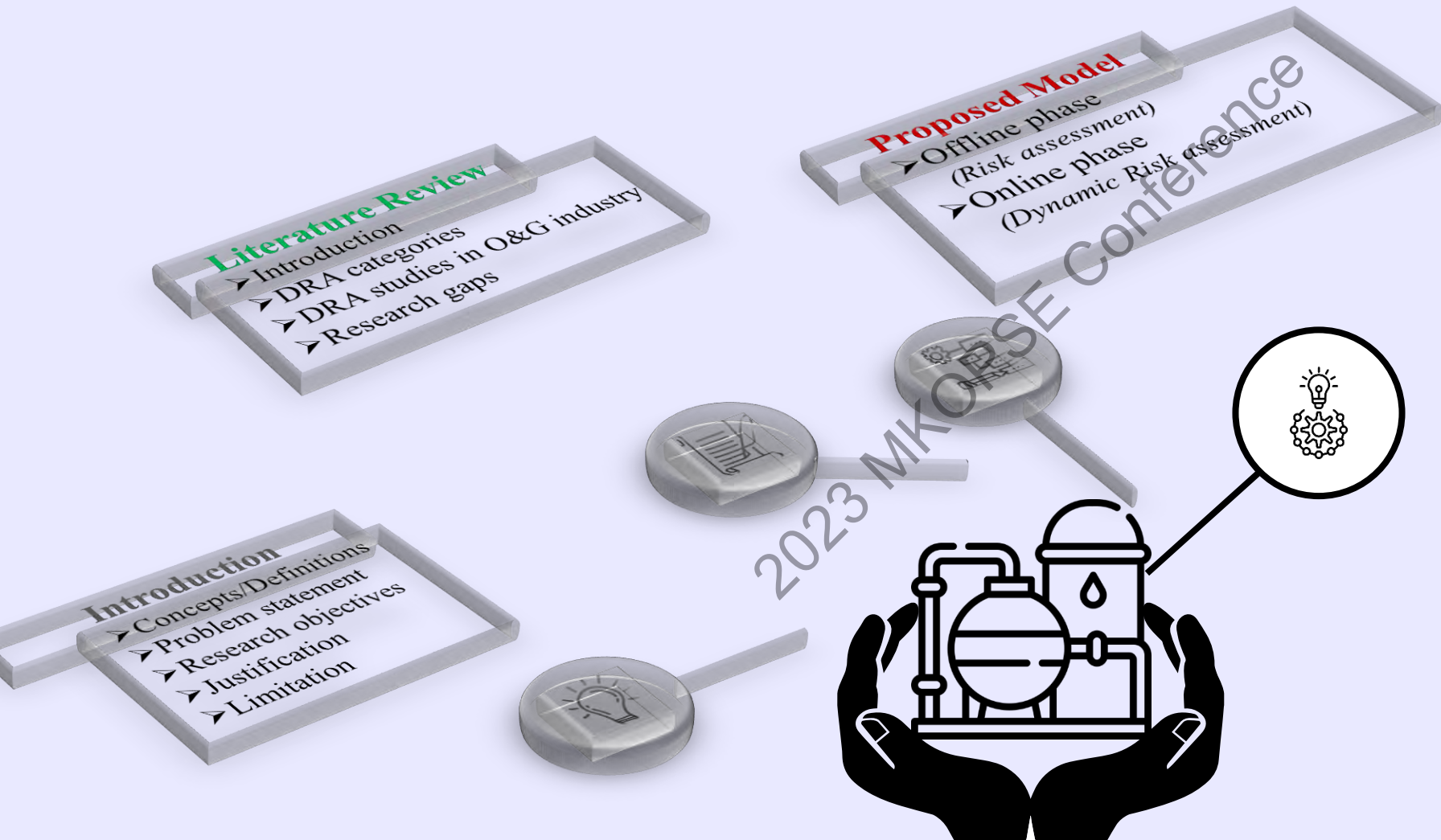
Step 4: *If* $r < p_{acc}$: $p^{(k)} \leftarrow p^{(k)}$
Else : $p^{(k)} \leftarrow p^{(k-1)}$

Step 5: $k = k + 1$

If $k = n_s$: *end*

Else : *Go to step 1*

Outline

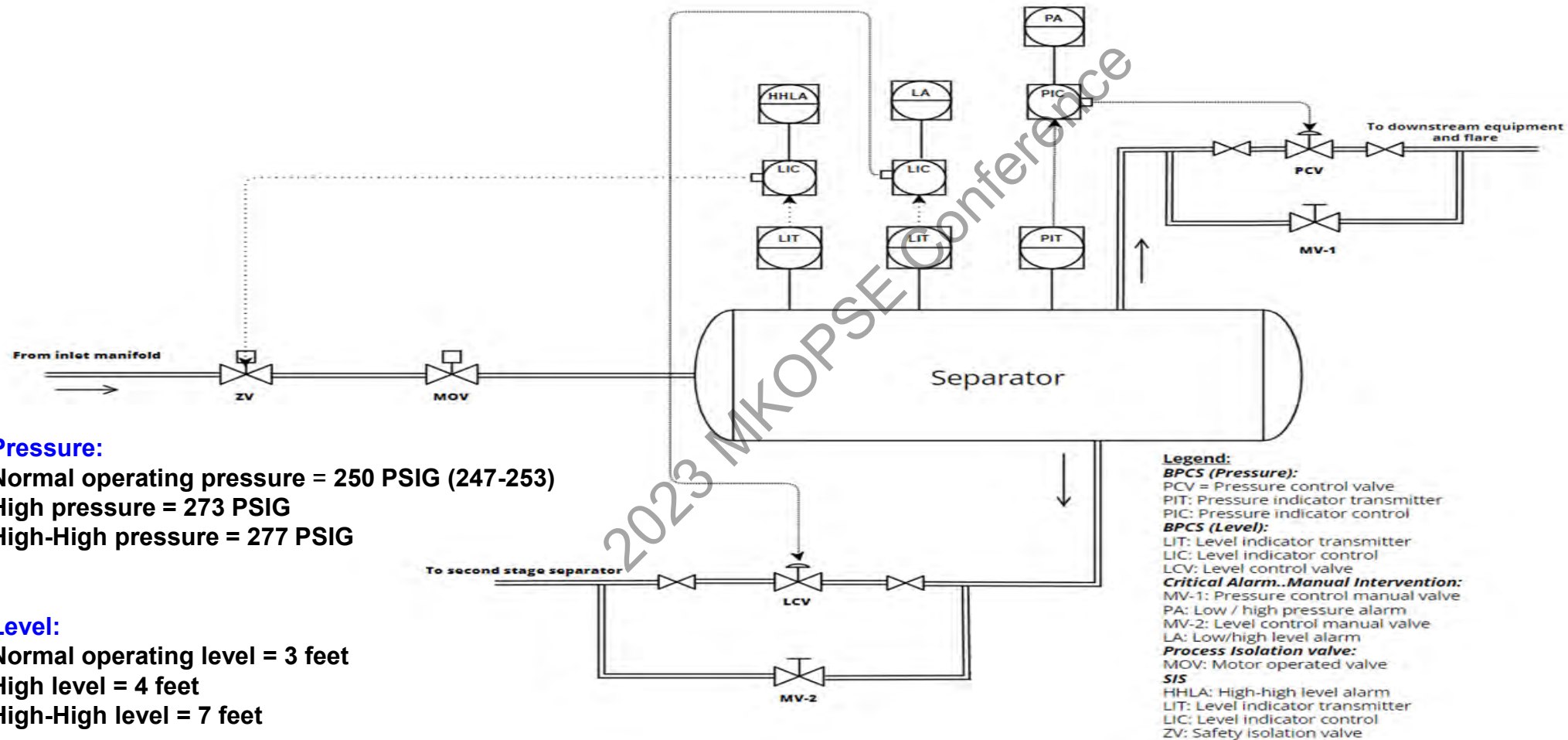


Application (case study)

- Process selection
- Process description
- Dynamic risk assessment of liquid carryover



Application (Case Study)



Pressure:

Normal operating pressure = 250 PSIG (247-253)

High pressure = 273 PSIG

High-High pressure = 277 PSIG

Level:

Normal operating level = 3 feet

High level = 4 feet

High-High level = 7 feet

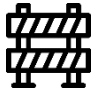


Application (Case Study)

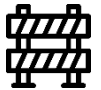
The liquid **carryover scenario** is **controlled** by the following safety barriers:



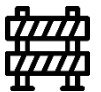
The first safety barrier (SB-1), a pressure control loop



The second safety barrier (SB-2), high-level alarm



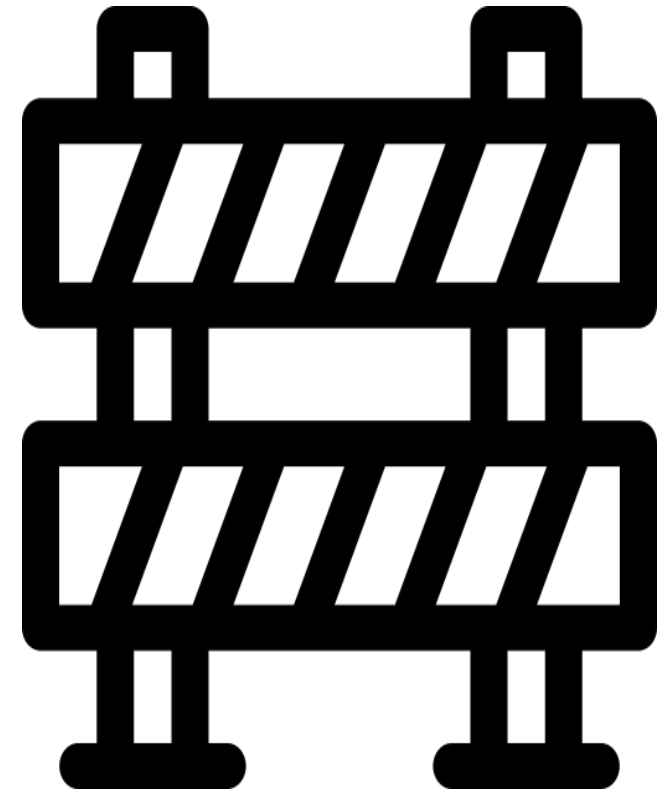
The third and fourth safety barrier (SB-3 and SB-4), operator supervision and manual intervention, respectively.



The fifth safety barrier (SB-5), motor-operated valve (MOV).

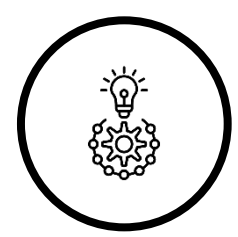


The sixth safety barrier (SB-6), safety instrumented system (SIS)



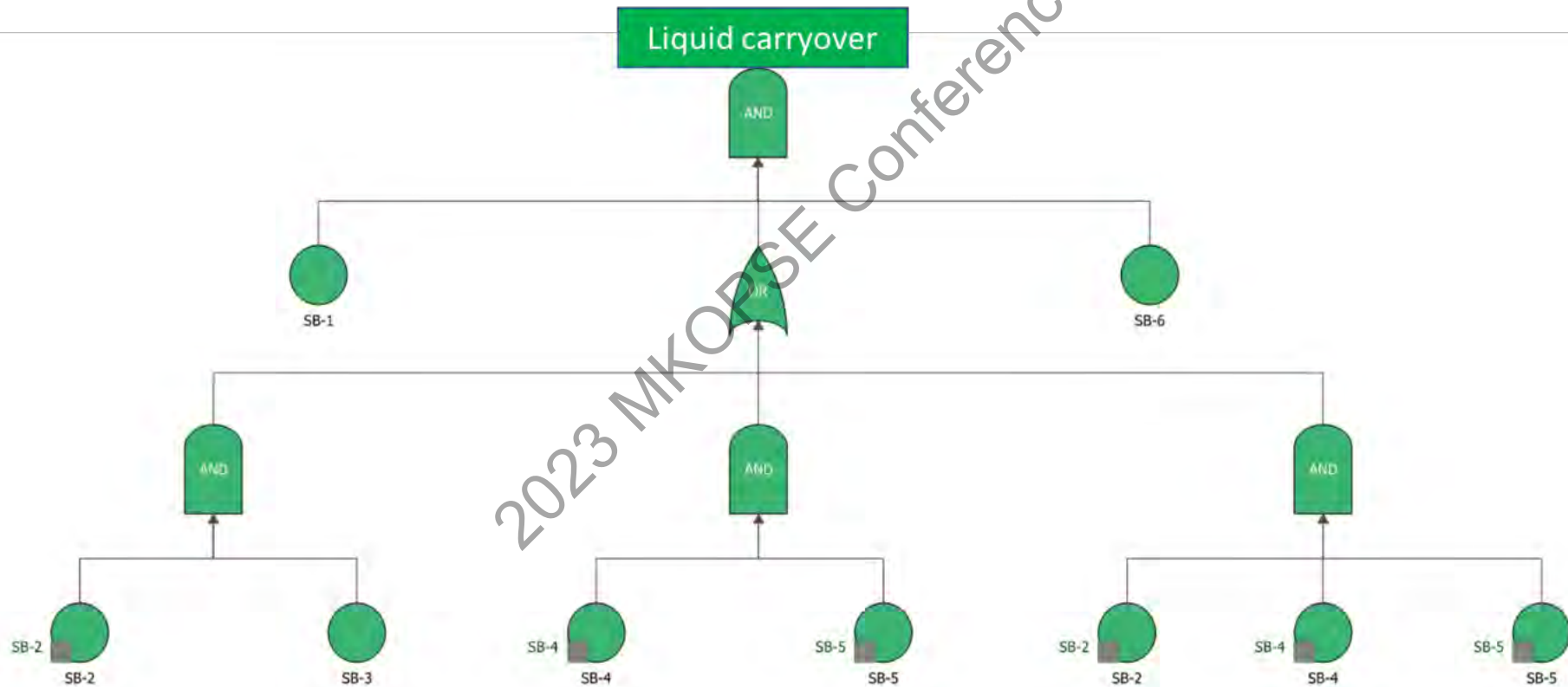
Offline phase

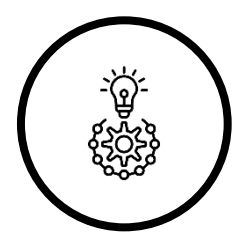
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Risk Assessment – Offline:

ReliaSoft (a reliability software) is a reliability software used to construct a Fault Tree





Risk Assessment – Offline:

Using ReliaSoft, the minimal cut sets (failure scenarios) are as follows:

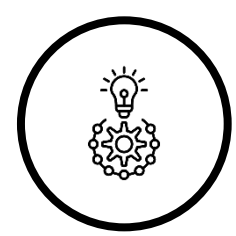
Minimal Cut Set #1

(SB-1) Pressure control loop AND
(SB-2) High-level alarm AND
(SB-3) Operator supervision AND
(SB-4) SIS



Minimal Cut Set #2

(SB-1) Pressure control loop AND
(SB-4) Pressure control manual valve AND
(SB-5) Motor-operated valve AND
(SB-6) SIS



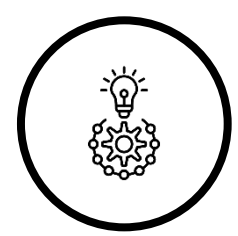
Risk Assessment – Offline:

Next step is to **assign failure probabilities** to the basic events (e.g., SB-1, SB-2, ..., SB-6).

The following **assumptions** are made:

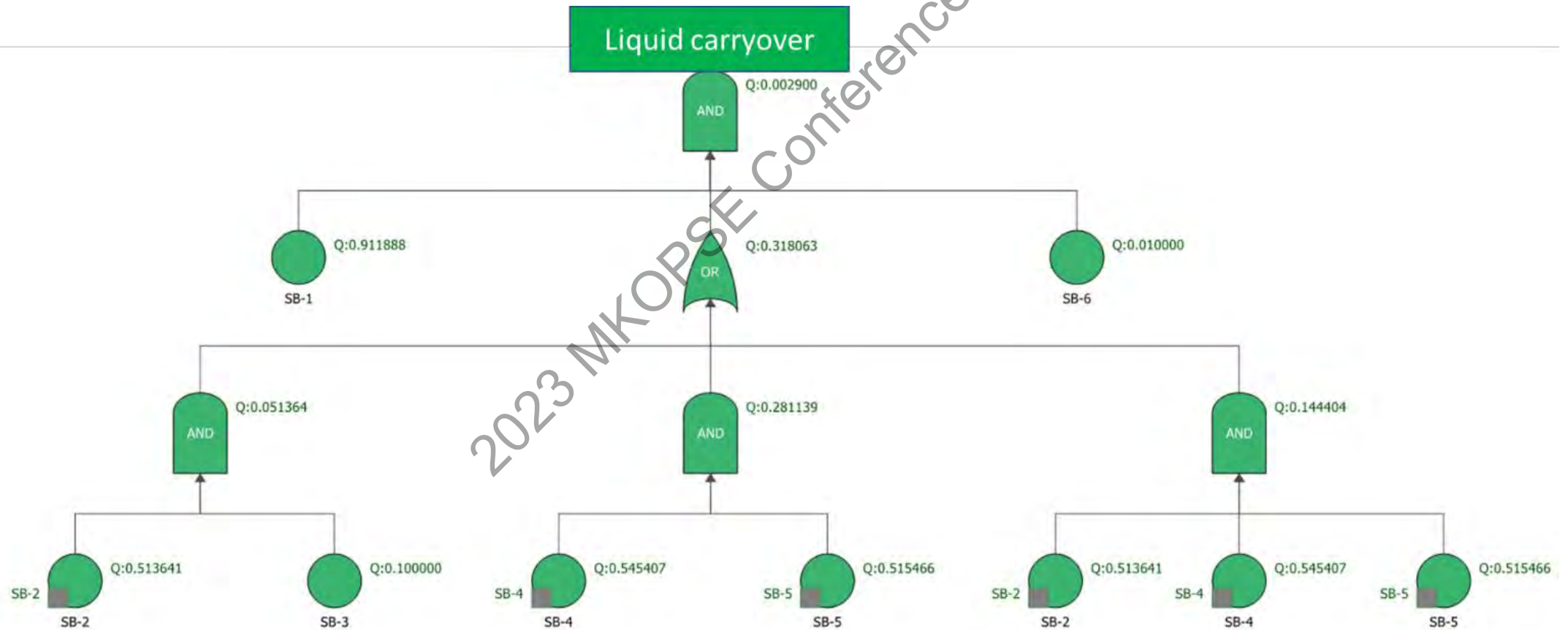
- SB_i are **independent** of each other
- SB-1, SB-2, SB-4 and SB-5 follow the **exponential distribution function** with a constant parameter λ .
- SB-3 and SB-6 have **constant** failure probabilities 0.1 and 0.01, respectively.

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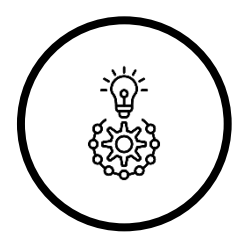
Risk Assessment – Offline:

Using ReliaSoft, the risk of the top event at $t = 3000$ hours is 0.0029



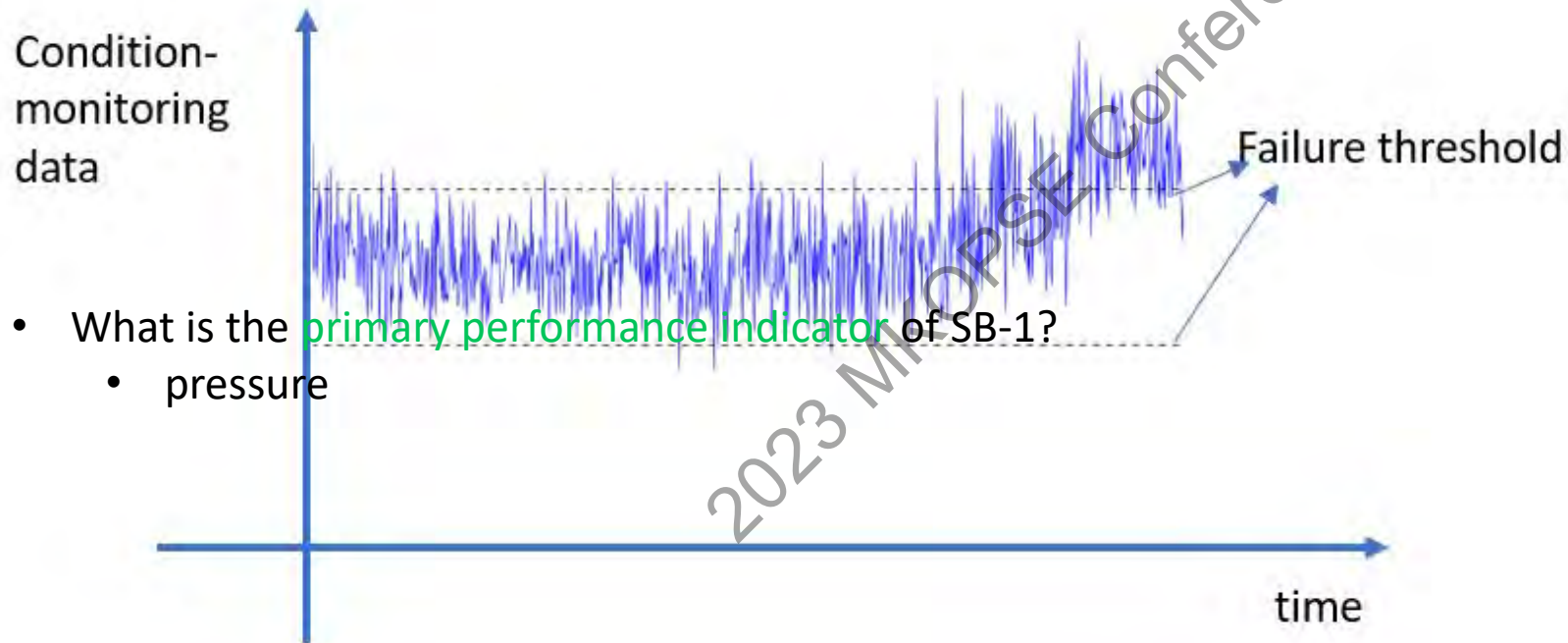
Online phase

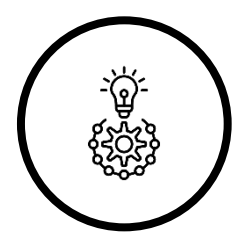
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Risk Assessment – Online:

Step 1: Select SB-1, pressure control loop, for monitoring

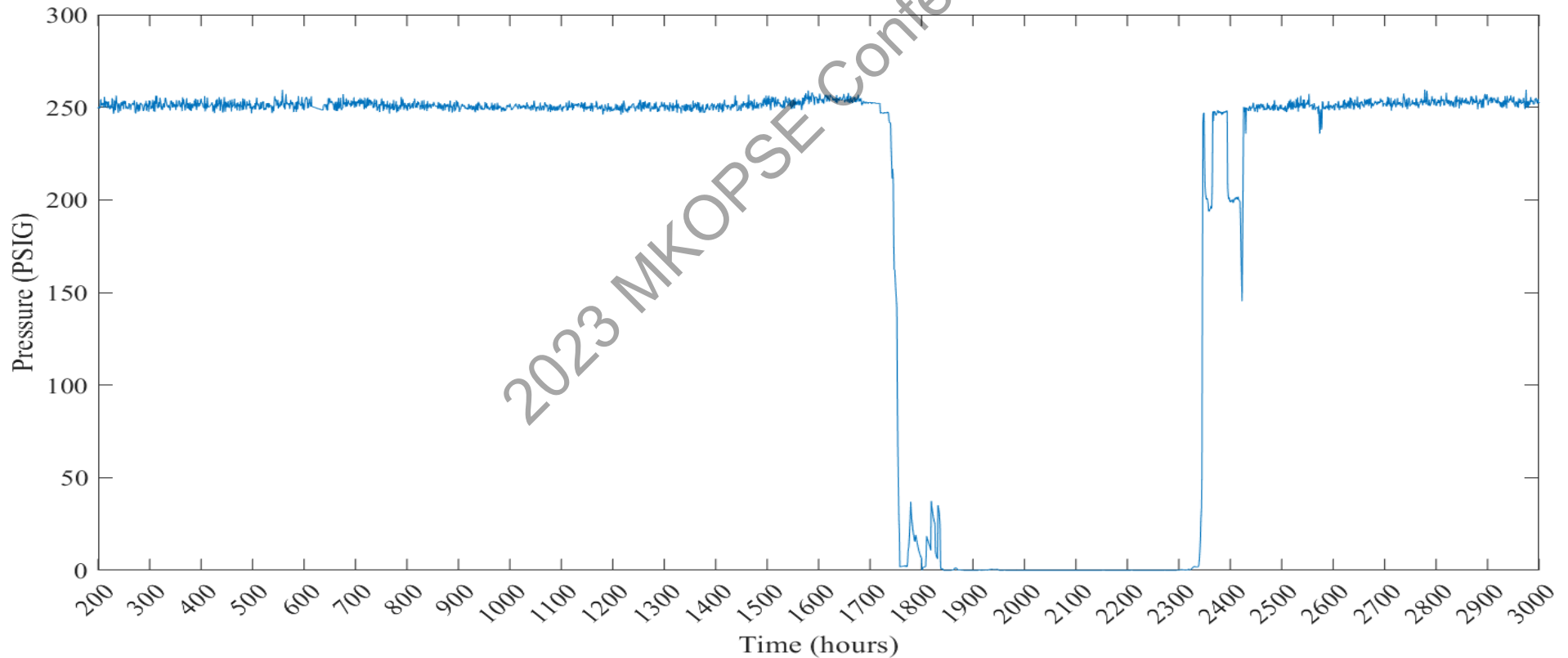


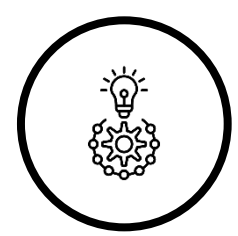


Risk Assessment – Online:

Step 1: **Select** SB-1, pressure control loop, for monitoring

Step 2: **Collect** condition-monitoring data





Risk Assessment – Online:

Step 1: **Select** SB-1, pressure control loop, for **monitoring**

Step 2: **Collect** condition-monitoring data

Step 3: **Construct** prior reliability distribution of SB-1, $p(R_{SB1})$

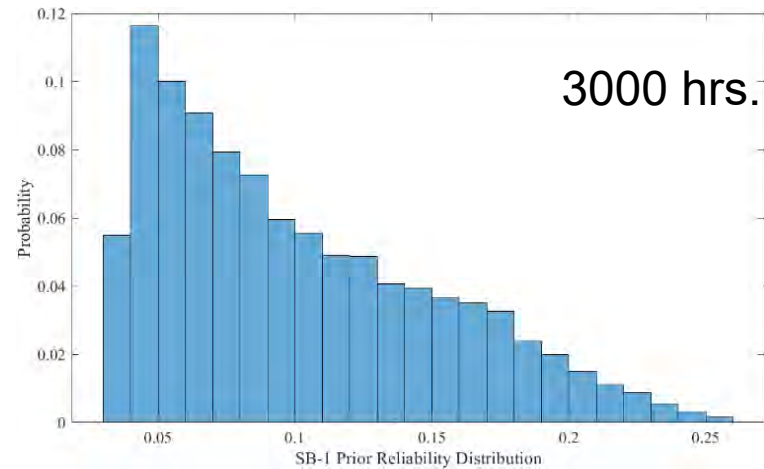
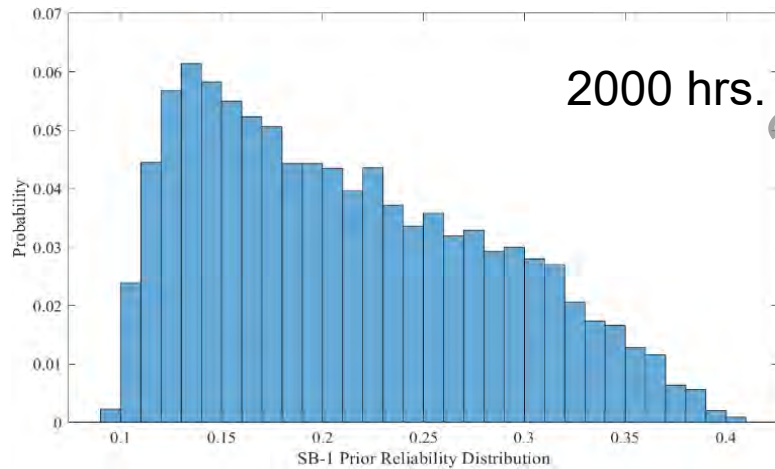
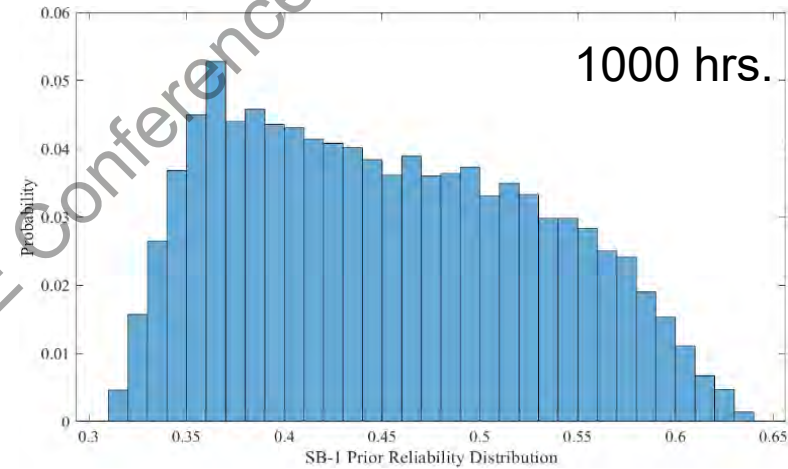
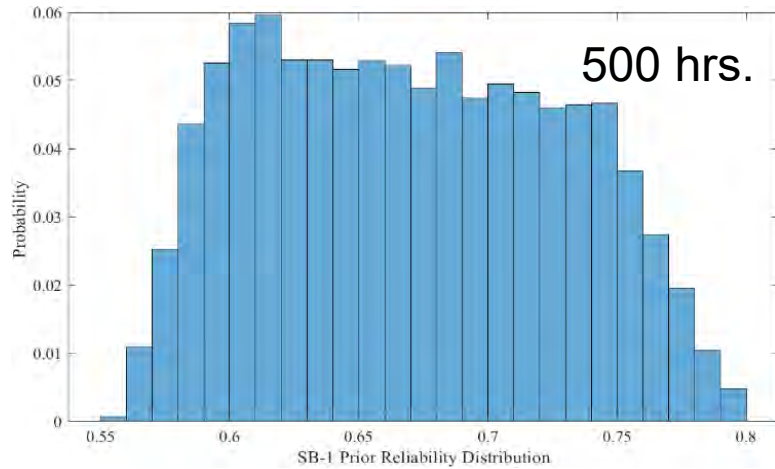
- $R = e^{-\lambda t}$, where $\lambda = [\text{Lower } \lambda, \text{upper } \lambda]$

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Risk Assessment – Online:

The **prior** reliability distribution of SB-1, $p(R_{SB1})$, at $t = 500, 1000, 2000$ and 3000 hours:



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Risk Assessment – Online:

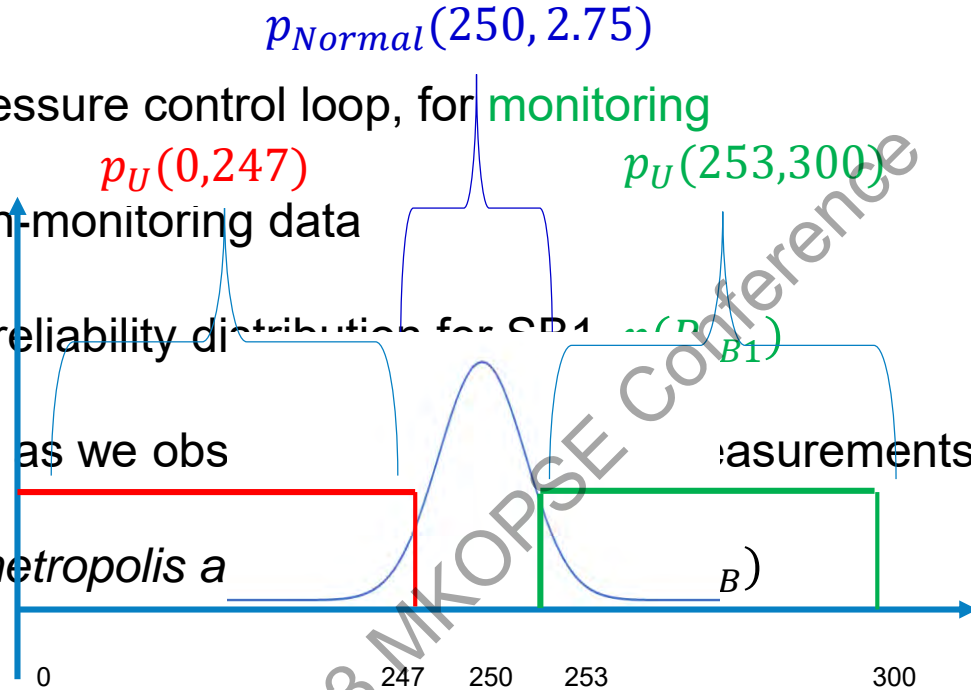
Step 1: Select SB-1, pressure control loop, for monitoring

Step 2: Collect condition-monitoring data

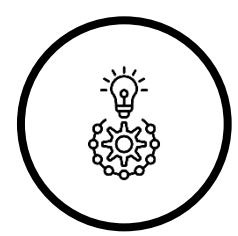
Step 3: Construct prior reliability distribution for SB1

Step 4: Update $p(R_{SB1})$ as we observe measurements

- Apply the metropolis algorithm
- Construct a likelihood function $p(y_{CM,i} | R_{SB})$

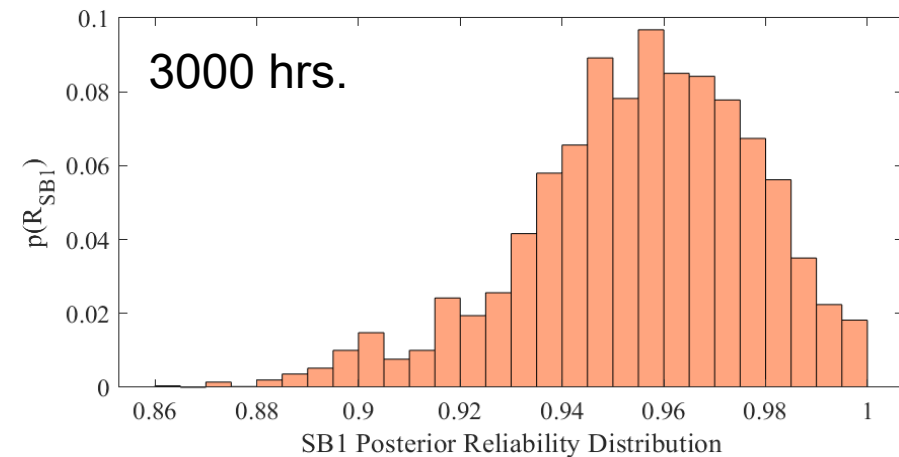
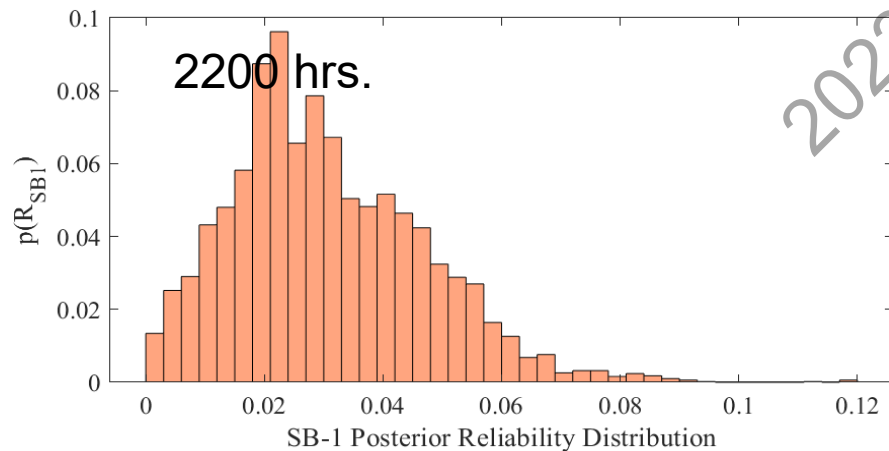
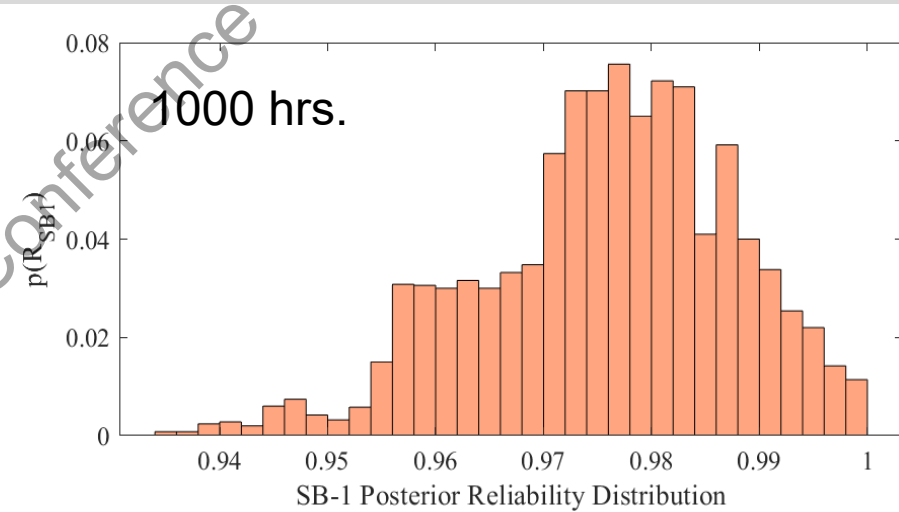
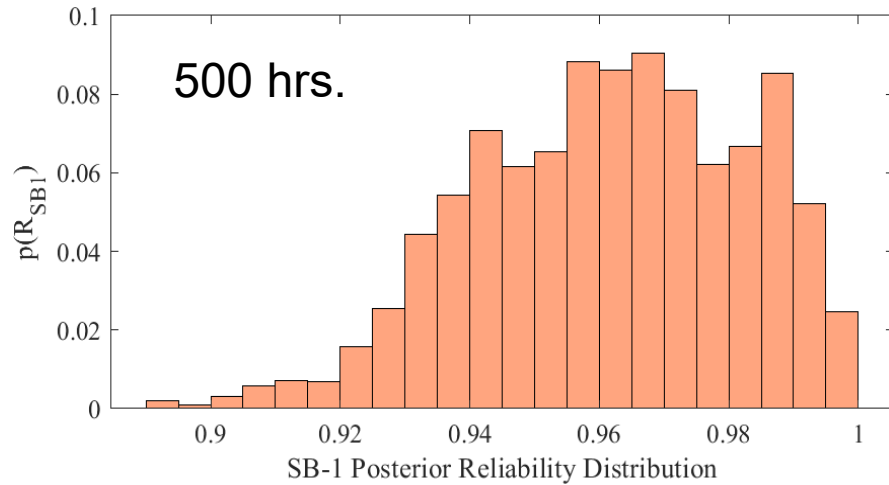


$$p(y_{CM,i} | R_{SB}) = R_{SB} \cdot p_{Normal}(250, 2.75) + \frac{1 - R_{SB}}{2} \cdot p_U(0, 247) + \frac{1 - R_{SB}}{2} \cdot p_U(253, 300)$$



Risk Assessment – Online:

The **posterior** distribution of SB-1, $p(R_{SB} | y_{CM,t})$, at $t = 500, 1000, 2200, 3000$ hours:

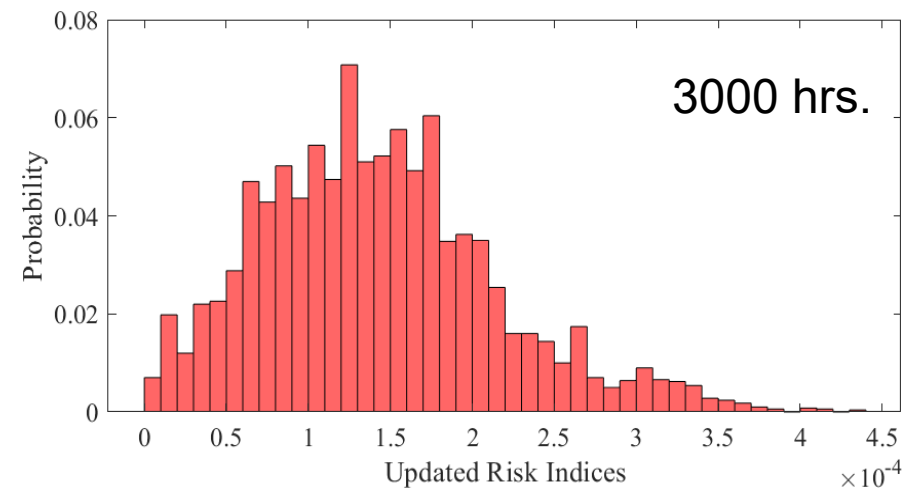
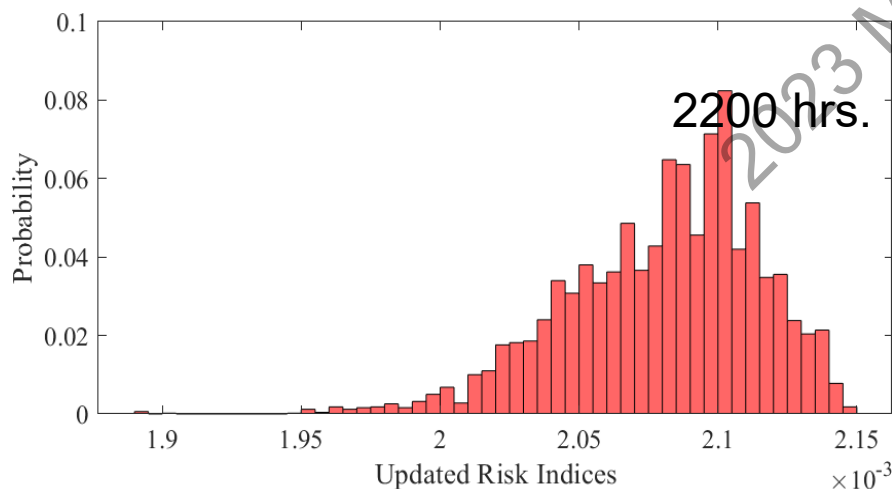
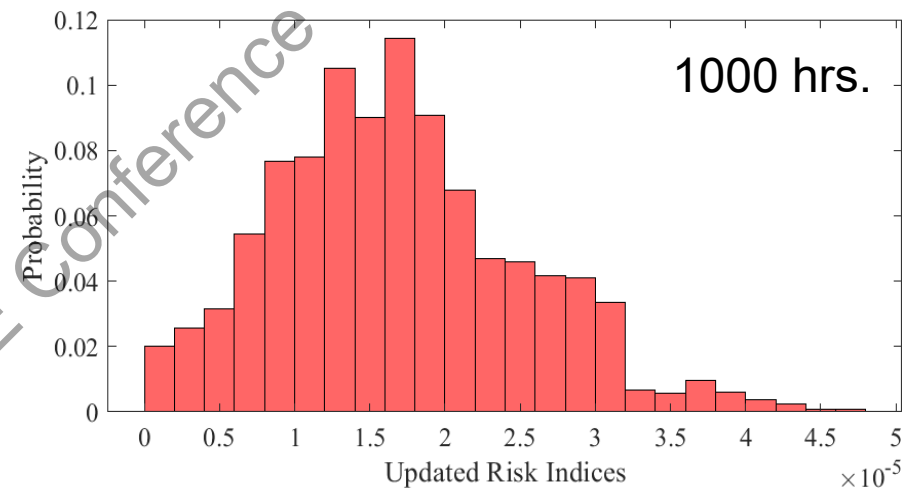
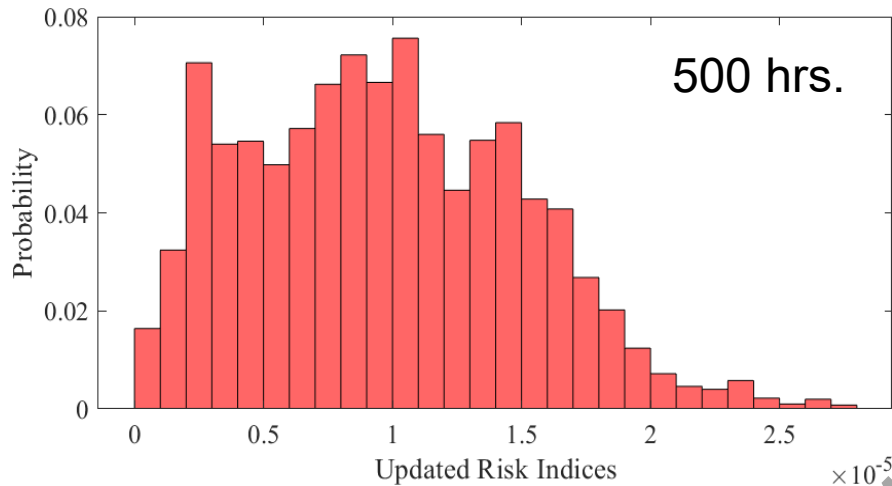


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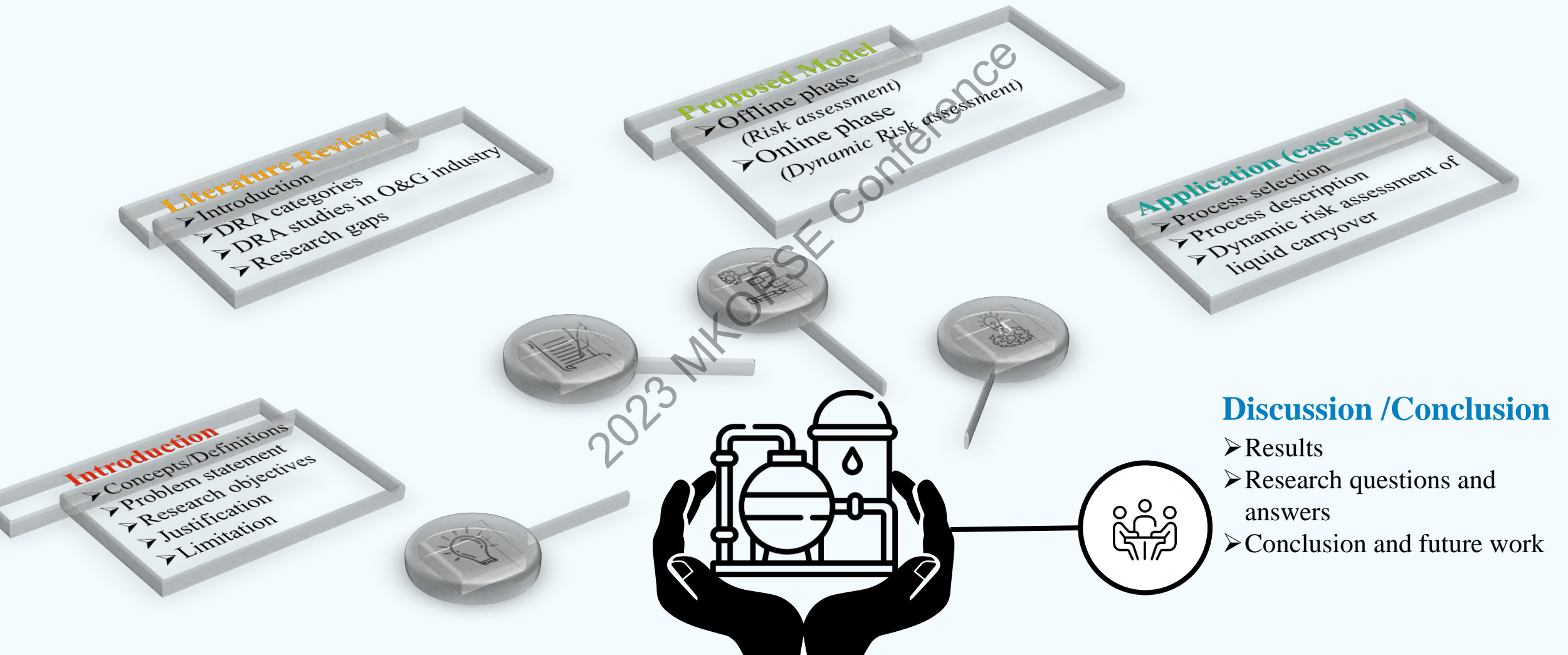


Risk Assessment – Online:

Substitute $p(R_{SB}|y_{CM,t})$ into $Risk = f(R_{SB1} \times R_{SB2} \times R_{SB3})$ to get risk indices distribution



Outline

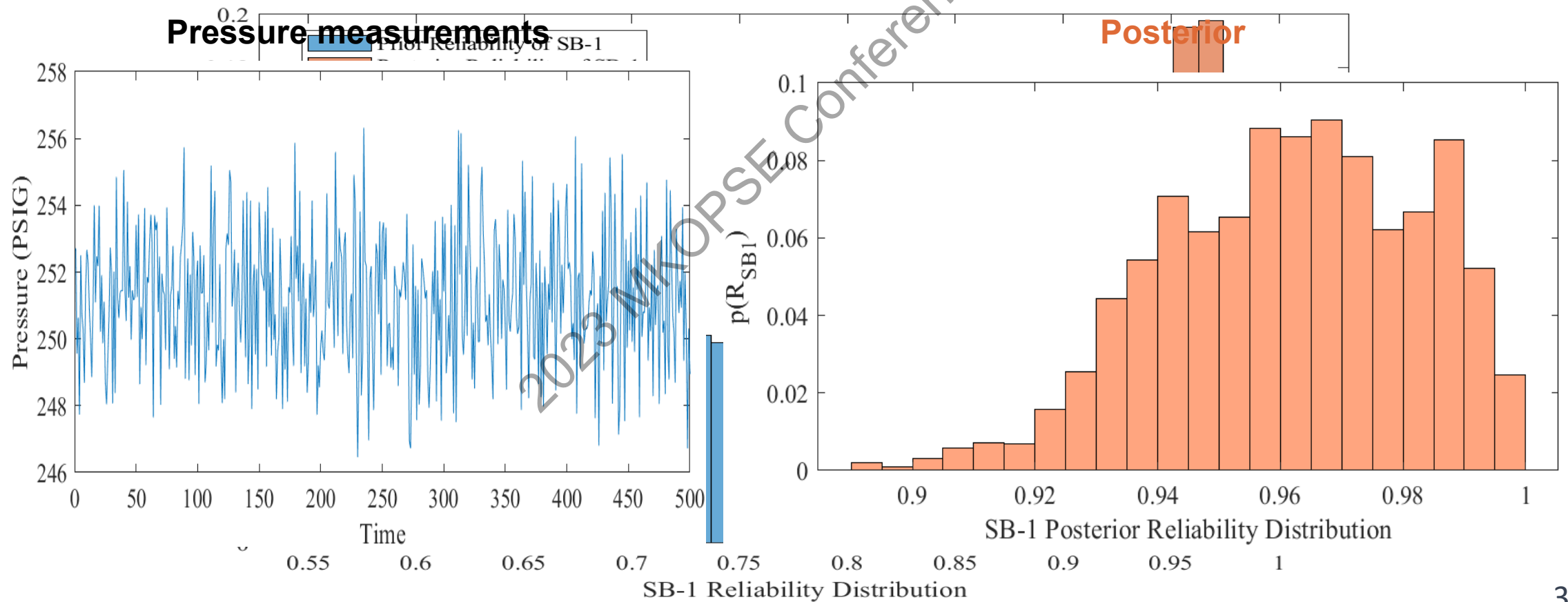




Results and Discussion

At $t = 500$ hours

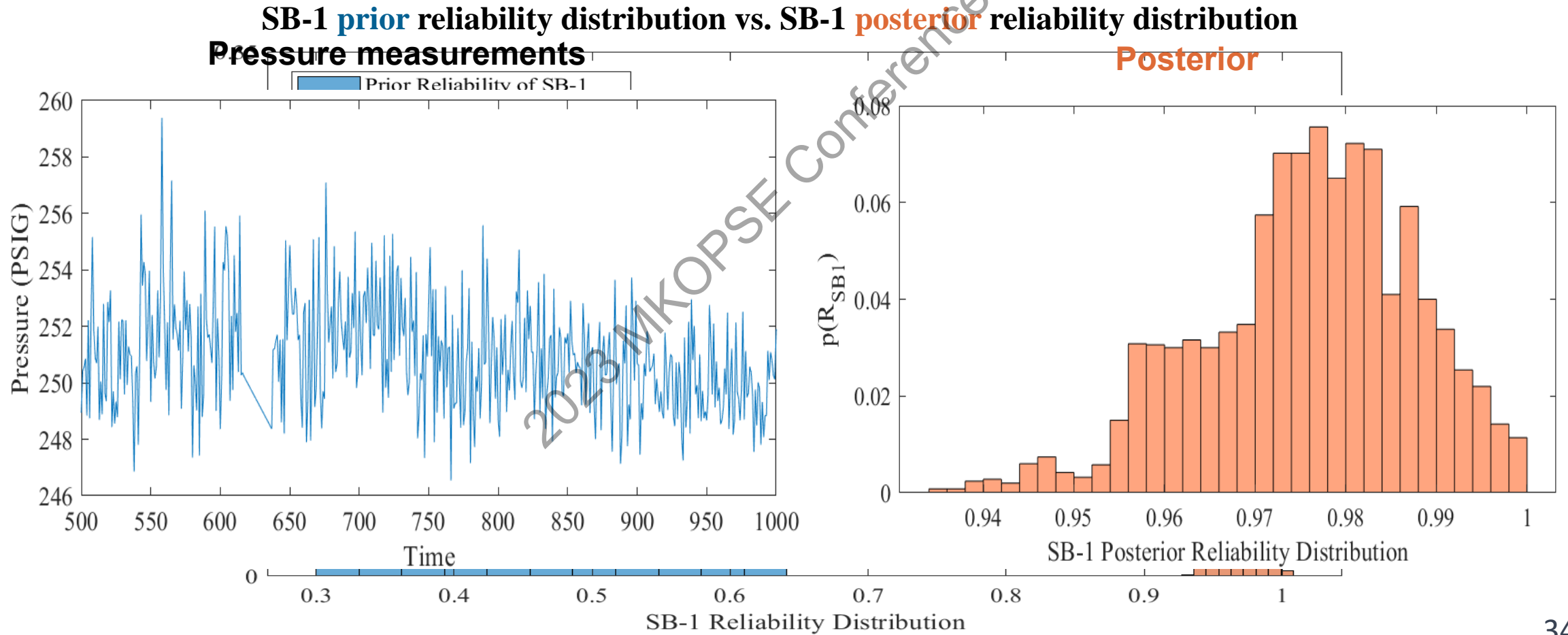
SB-1 prior reliability distribution vs. SB-1 posterior reliability distribution





Results and Discussion

At $t = 1000$ hours

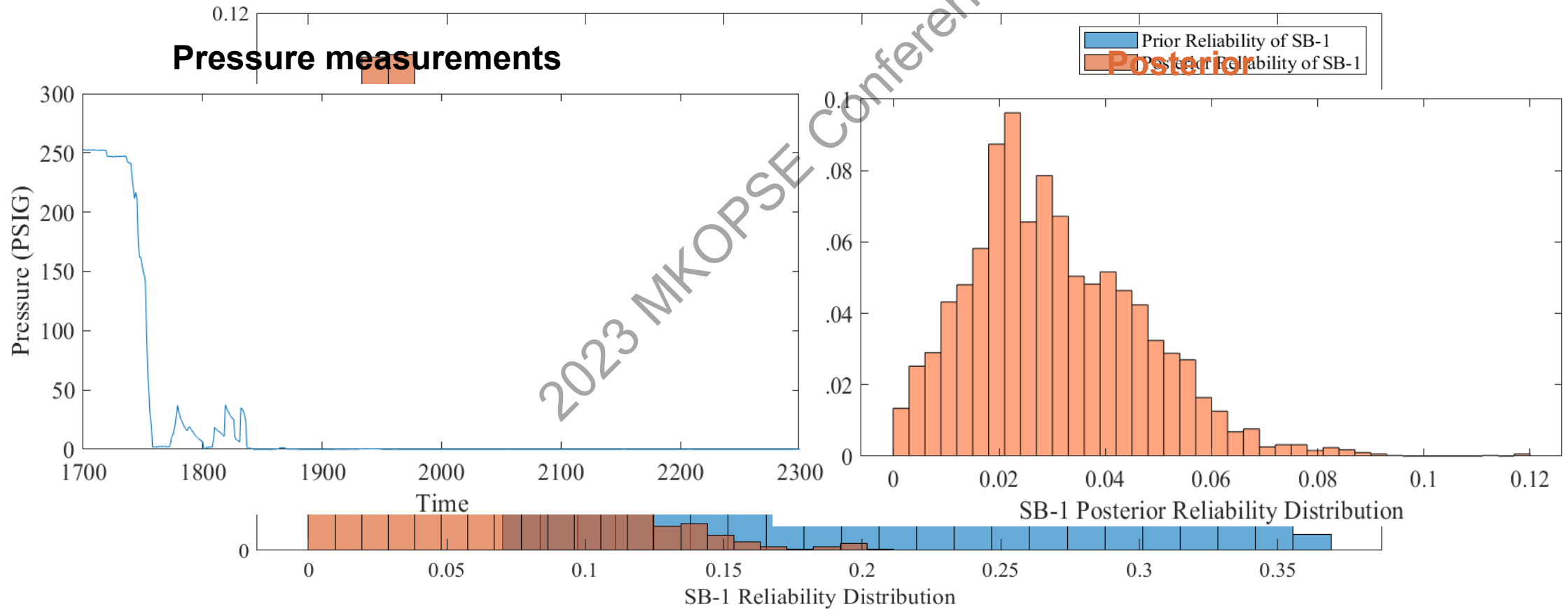




Results and Discussion

At $t = 2200$ hours

SB-1 prior reliability distribution vs. SB-1 posterior reliability distribution

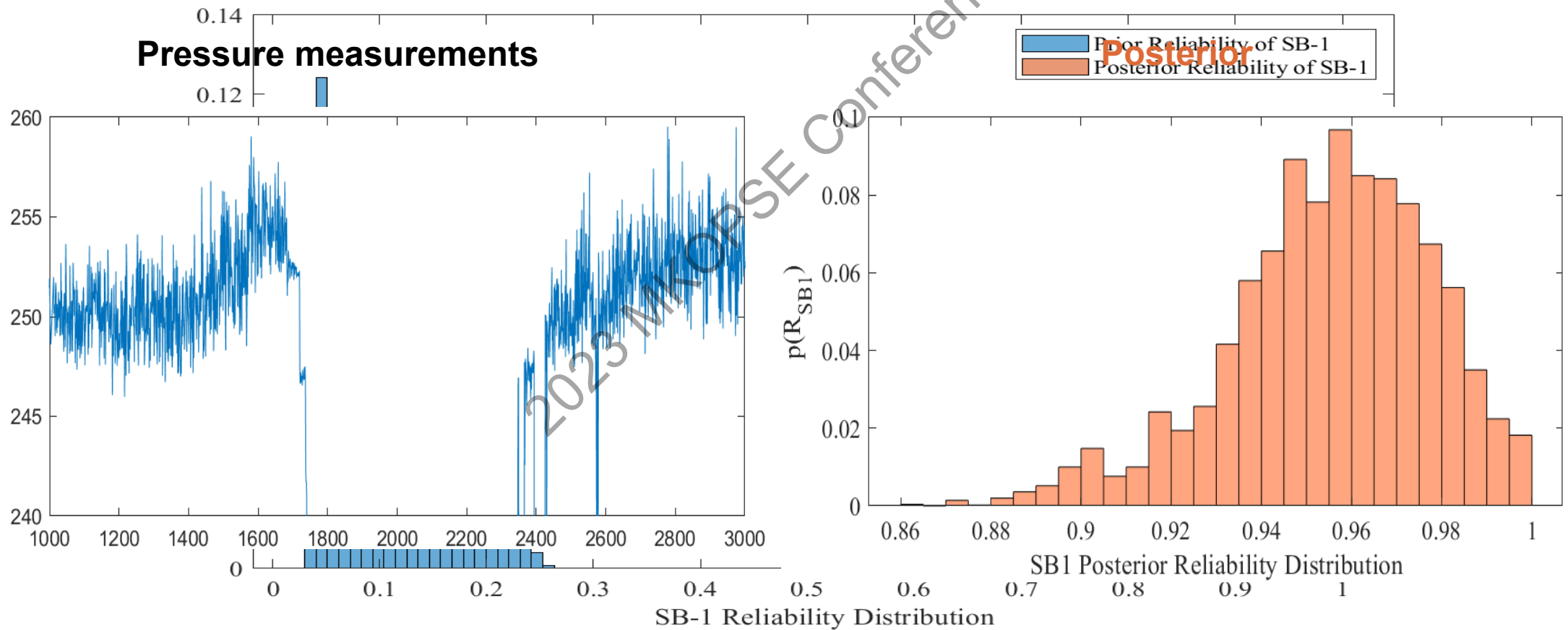




Results and Discussion

At $t = 3000$ hours

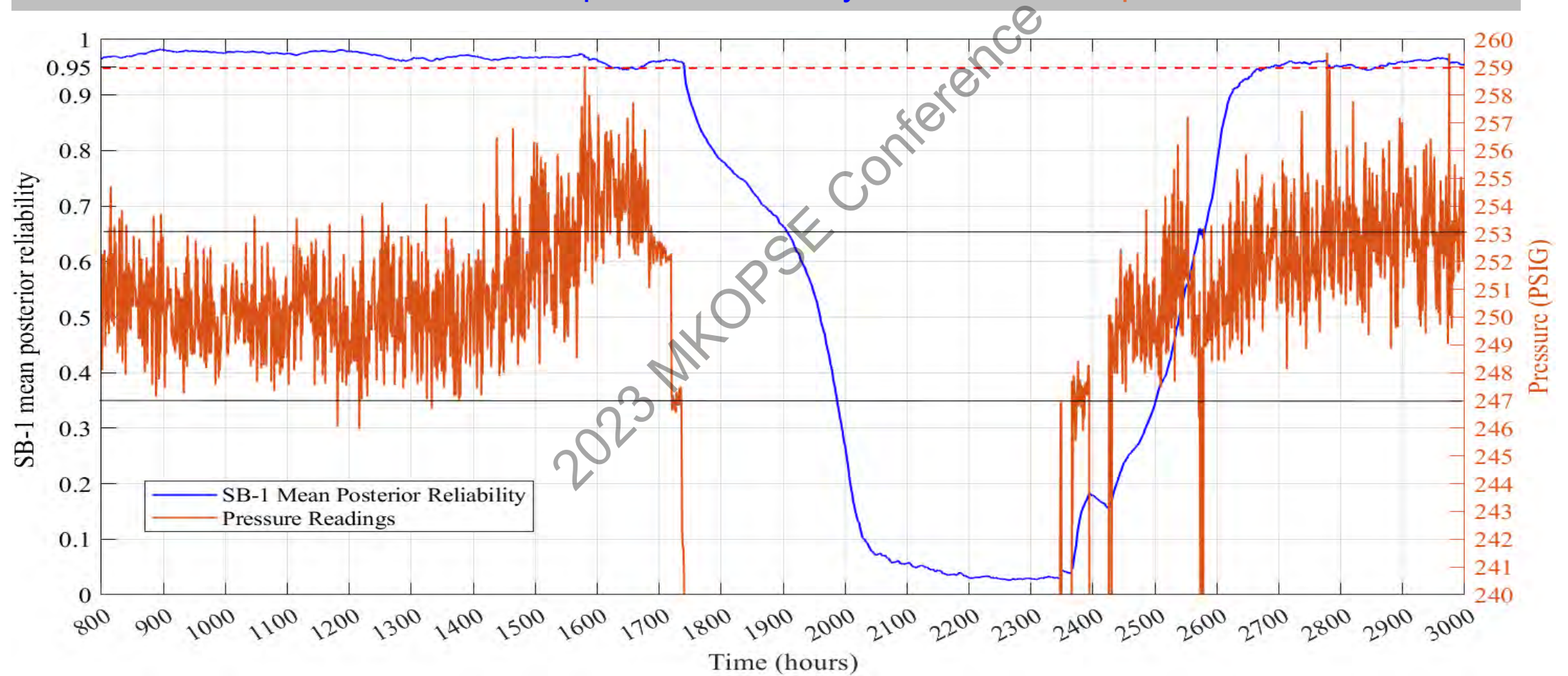
SB-1 prior reliability distribution vs. SB-1 posterior reliability distribution





Results and Discussion

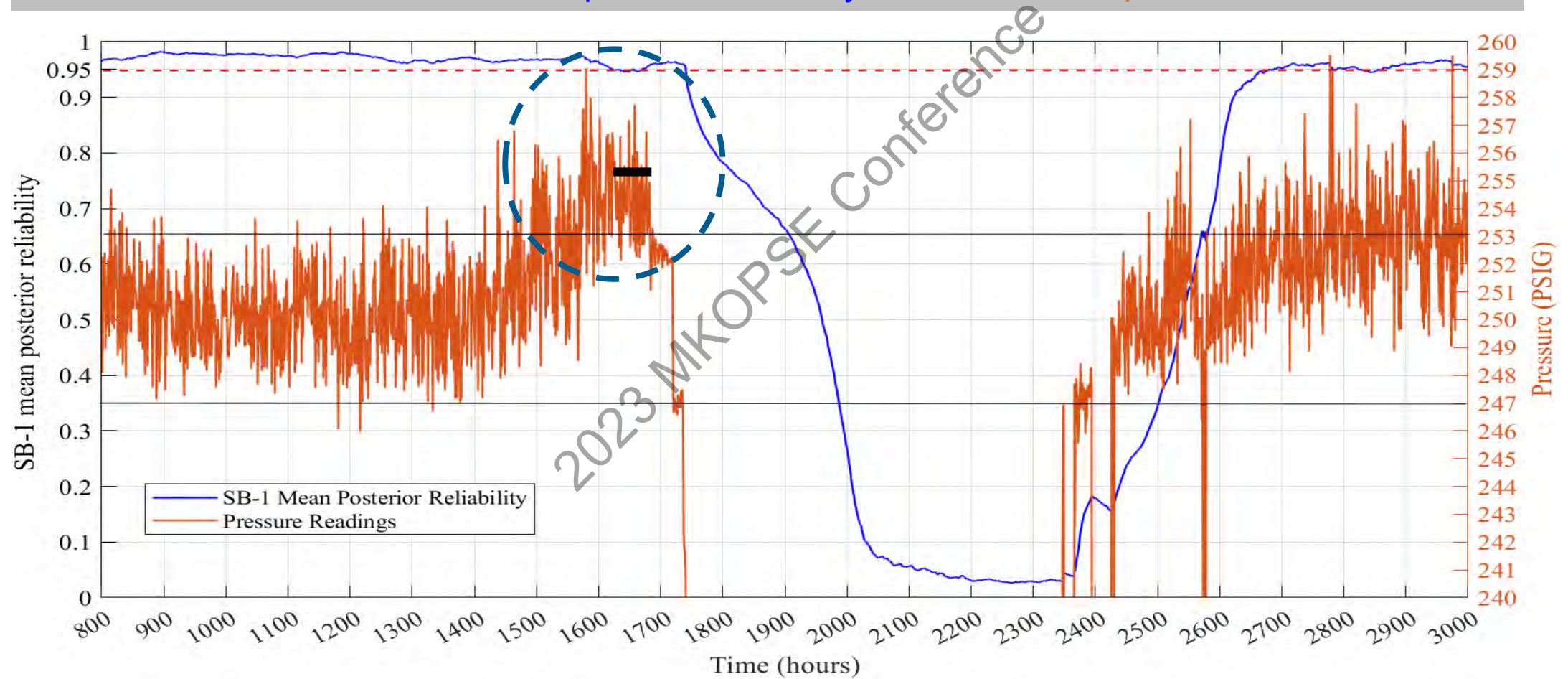
Furthermore, we correlate the mean posterior reliability of SB-1 with the pressure measurements:





Results and Discussion

Furthermore, we correlate the mean posterior reliability of SB-1 with the pressure measurements:

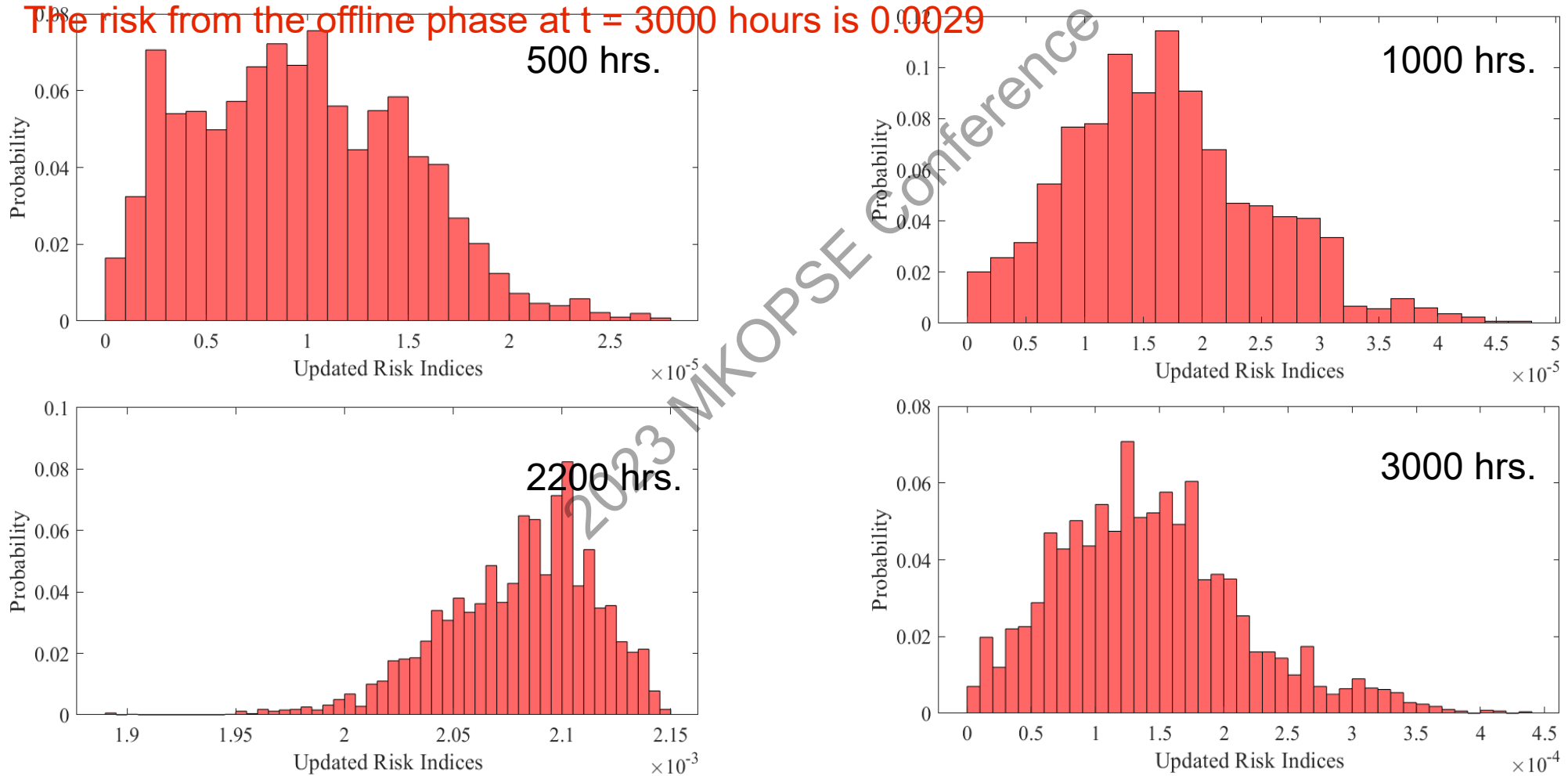




Results and Discussion

Risk of liquid carryover (offline phase vs. online phase)

The risk from the offline phase at $t = 3000$ hours is 0.0029





Results and Discussion

Offline phase (conventional QRA)

- ✗ Does not capture operation changes nor time dependent failure probabilities
- ✗ Unable to predict failures of critical components
- ✗ Requires an update to support decision-making
- ✗ Static, providing an outdated picture of risk

Online phase (Our DRA model)

- ✓ Captures the time-dependent failure probabilities of critical components
- ✓ Predicts failures of critical components
- ✓ Provides real-time data to improve decision-making
- ✓ Dynamic, enabling timely response to risk changes

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Limitations of the Study

Study and analyze the **human errors** as part of the model

Incorporate **inspection data** into the model

Select more than **one critical component** for monitoring

Test the model on **a different process** within the O&G industry





Conclusion

Objective 1: To contribute to the development and application of the DRA techniques in the O&G industry

Our model applies a DRA technique involving a process from the O&G industry

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Conclusion

Objective 1: To contribute to the development and application of the DRA techniques in the O&G industry

Objective 2: To obtain the risk level of an accident scenario in real-time

The model can provide evolving picture of risk level in real time.

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Conclusion

Objective 1: To contribute to the development and application of the DRA techniques in the O&G industry

Objective 2: To obtain the risk level of an accident scenario in real-time

Objective 3: To make informed decisions based on inputs from the DRA technique

Decisions, concerning, for example production increase can be made based on inputs from this model.

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Conclusion

Objective 1: To contribute to the development and application of the DRA techniques in the O&G industry

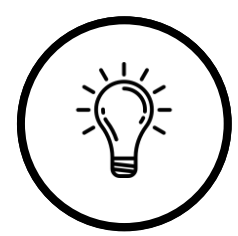
Objective 2: To obtain the risk level of an accident scenario in real-time

Objective 3: To make informed decisions based on inputs from the DRA technique

Objective 4: To anticipate failure of process safety barriers

The model provides a window of 40 hours for maintenance/operation team to address and prevent SB-1 from failing.

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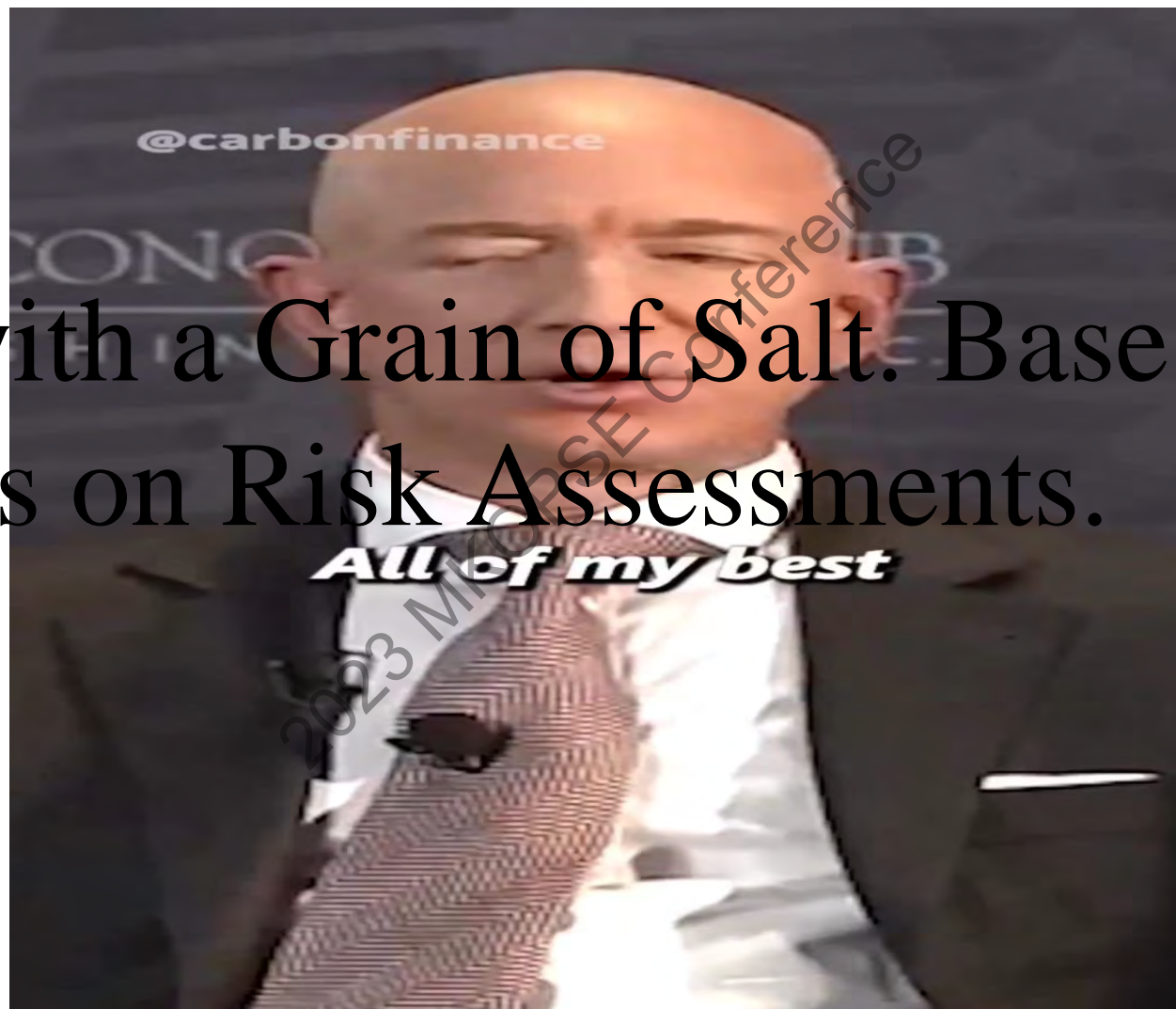
Conclusion (achieving the Goal)



Apply a DRA technique to an O&G process unit by integrating conventional risk assessment with condition-monitoring data.

By realizing all 4 objectives, we can say that the goal of this study has been achieved.

Take it with a Grain of Salt. Base Your
Decisions on Risk Assessments.



Thank you

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2023 Mary Kay O'Connor Safety & Risk Conference

Safe and Sustainable Energy Transition



Texas A&M Engineering Experiment Station

Mary Kay O'Connor
Process Safety Center

In Association with IChemE

October 11-13, 2023

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2023 Mary Kay O'Connor Safety & Risk Conference

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Mary Kay O'Connor
Process Safety Center
Texas A&M Engineering Experiment Station

Application of Inherently Safe Principles to Projects

Presenter: Tim Hoff

ExxonMobil Technology and Engineering Company

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Tim Hoff

- ExxonMobil Process Safety SME for Global Projects
- B.S. in ChemE from Purdue University (2001)
- Variety of roles within EM
 - Project Development, Process Design, and Execution/Start-up
 - Senior Operations Engineer for Alkylation and Light Ends Fractionation
 - Site Process Safety Engineer
 - Technical Process Safety Lead for Northeastern Operating Sites



What you don't have can't leak.

People who aren't there can't be killed.

- Trevor Kletz

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Bhopal Disaster - 1984

- Estimated 4k-20k fatalities due to exposure of highly toxic gas cloud of methyl isocyanate (MIC)
- Liquid MIC stored in three 18,000 US gal underground tanks
- Introduction of water to tank resulted in large production of vapor MIC to ATM via overpressure protection devices



Source: Wikipedia

Beirut Explosion - 2020

- At least 218 deaths from an explosion of 2,750 tons of ammonia nitrate that was being stored in a port warehouse
- Explosion was preceded by a large fire in the same warehouse
- Ammonia nitrate had been stored without safety precautions for 6 years after being confiscated by authorities



Source: New York Post

Aqaba Chlorine Leak - 2022

- At least 13 people killed after a 25 ton chlorine cylinder dropped from a crane and ruptured
- Wire rope sling of crane was rated for 8.5 tons
- Senior port officials had delegated critical safety tasks to untrained personnel



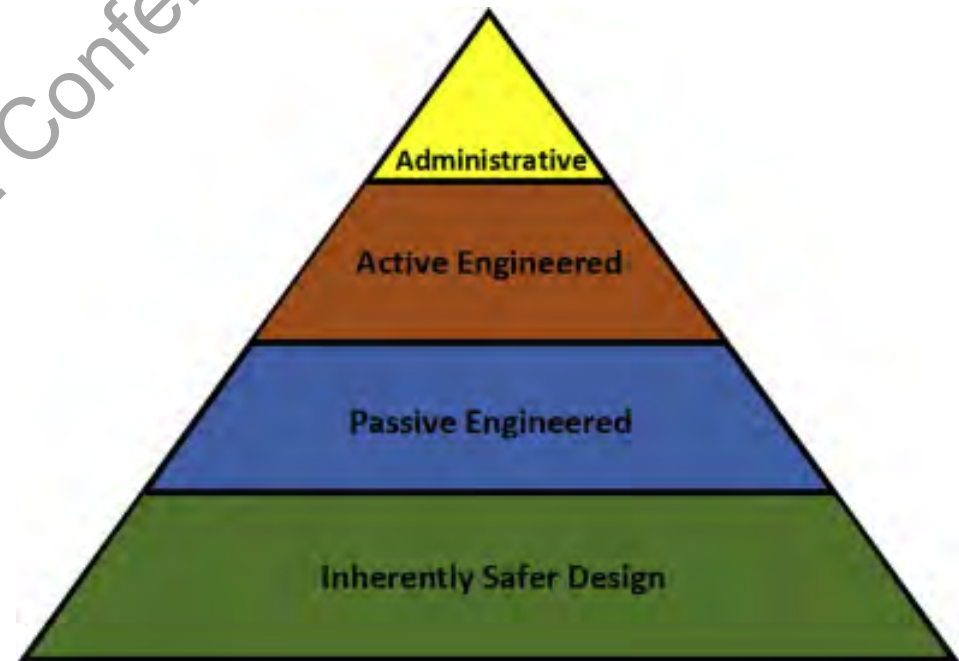
Source: Reuters

The public isn't responsible for hazards!!



What is Inherent Safety?

- Avoiding creation of hazards or minimizing hazards if design requires their inclusion
- Elimination or reduction of hazards is accomplished through application of the 4 common Inherent Safety Principles



Source: Methods in Chemical Process Safety, Volume 4



Inherent Safety Principles

- Substitution
 - Substitute more hazardous material with less hazardous one
- Reduction
 - Reduce inventory in storage and process vessels
- Attenuation
 - Reduce severity of processing/operating conditions
- Simplification
 - Simplify the process to reduce potential for operator error

Inherent Safety in Projects

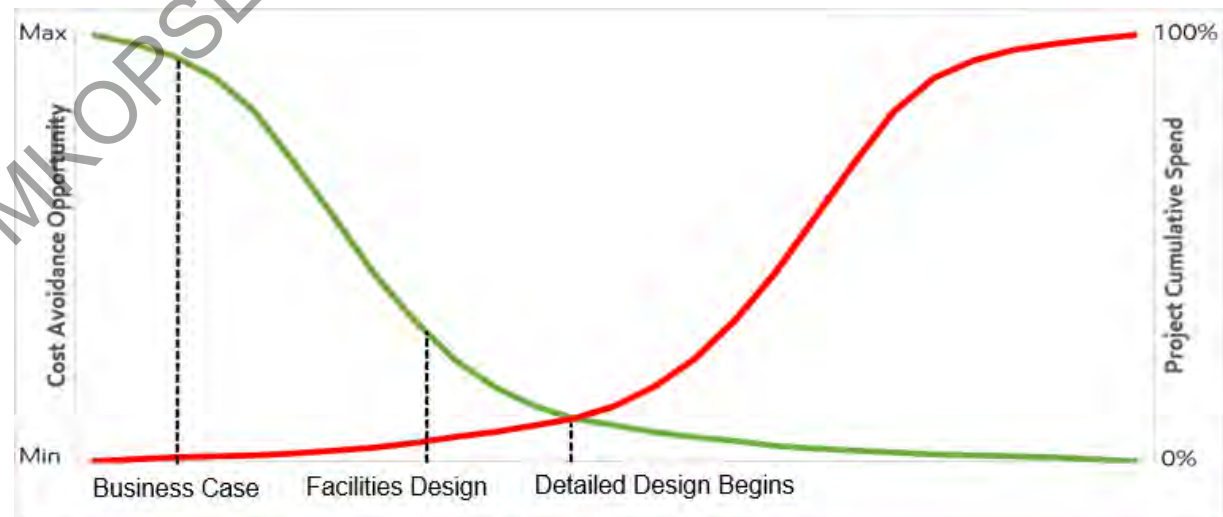
- Projects modify or introduce new hazards, altering an operating facility's risk profile
- Design philosophies might not recognize risks or new technologies/chemicals or changing risk philosophies over time
- Inherently Safest Design has a more substantial and permanent reduction in risk profile



Source: Mammoet.com

Inherent Safety Review and Timing

- Inherent Safety Reviews should be completed with a focus on a project's specific hazards and proposed design
- Early identification and review of hazards is critical to ensure inherently safest design has been considered





Inherent Safety Review Structure

- Formal review of the most representative design and hazard information available in early stages of project
 - Business Case review should focus on 'show stopper' hazards
 - Facilities Design review should focus on reduction of designed safeguards
- Effective review methodologies are “what-if” or checklist review
 - “What-if” is fit-for-purpose brainstorming approach
 - Checklist review requires development of questions in advance by experienced facilitator



Inherent Safety Review Participants

- Highly effective review is dependent on knowledge of the participants on the inherent hazards of the process or technology
- Team size should be based on complexity of process or technology
- Potential review members:
 - Process Safety Engineer
 - Process Technology Expert
 - Industrial Hygienist
 - Project Representative
 - Operations/Maintenance Representative

• More details on Inherent Safety Reviews can be found in "CCPS: Guidelines for Hazard Evaluation Procedures", 3rd edition

Inherent Safety Challenges in Projects

- Early application of Inherently Safest Technology may still incur a larger overall project cost
- Resolution of one risk can introduce another that requires further evaluation
- Inherently Safest Technology cannot be applied for logistical reasons



Source: The Hangover

Inherent Safety Questions for Bhopal

- “What if a large volume of water is introduced into the MIC tank when closed relief system is unavailable?”
 - Was consideration given to reducing the tank sizes and liquid inventory of MIC?
 - Was consideration given to alternate process that makes MIC in-situ or doesn't require MIC at all?



Source: Wikipedia

Inherent Safety Questions for Beirut

- “What if there is a large uncontrolled fire in the warehouse?”
 - Was consideration given to storing ammonia nitrate in a fire-safe area?
 - Was consideration given to isolating ammonia nitrate from all other flammable material?



Source: New York Post

Inherent Safety Questions for Aqaba

- “What if one of the chlorine cylinders gets dropped from elevation and breaks?”
 - Was consideration given to an alternate means of cylinder transfer that didn't involve elevated lift?
 - Was consideration given to limiting size of cylinders to within weight limit of smallest sling?



Source: Reuters



Inherent Safety Summary

- Highly effective reduction in a project's risk profile can be achieved through timely application of Inherent Safety Principles
 - Impact on project cost and schedule is lessened the earlier hazards are identified and Inherent Safety Principles applied
- Application of Inherent Safety Principles can decrease the quantity of designed mechanical and procedural safeguards
- Inherently Safest Technology cannot always be applied, but hazard identification and review is key in aiding a project in their rationale of safeguards and meeting an operating site's endorsed risk profile

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**“If you think safety is
expensive...., try an accident”**

- an old saying.

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SreeRaj R Nair

Technical Safety
Engineering Leader
Chevron Corporation

- Steward process safety performance and governance, Global experience (23 years)
- Chartered Engineer (IET)
- PhD, MSc (Eng.), B.Tech

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Harigopal Attal

Process Safety
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- Process safety management, inherently safer design, Relief and flare system design (40 years)
- Professional Engineer (Texas)
- M.Chem Eng, B. Chem Eng

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You have “safeguard” in place, sounds promising;
have you tested it?

Act before it is too late !!

- Effective safeguards are critical for effective risk management
- Ensure safeguards are in place and effective throughout the lifecycle.



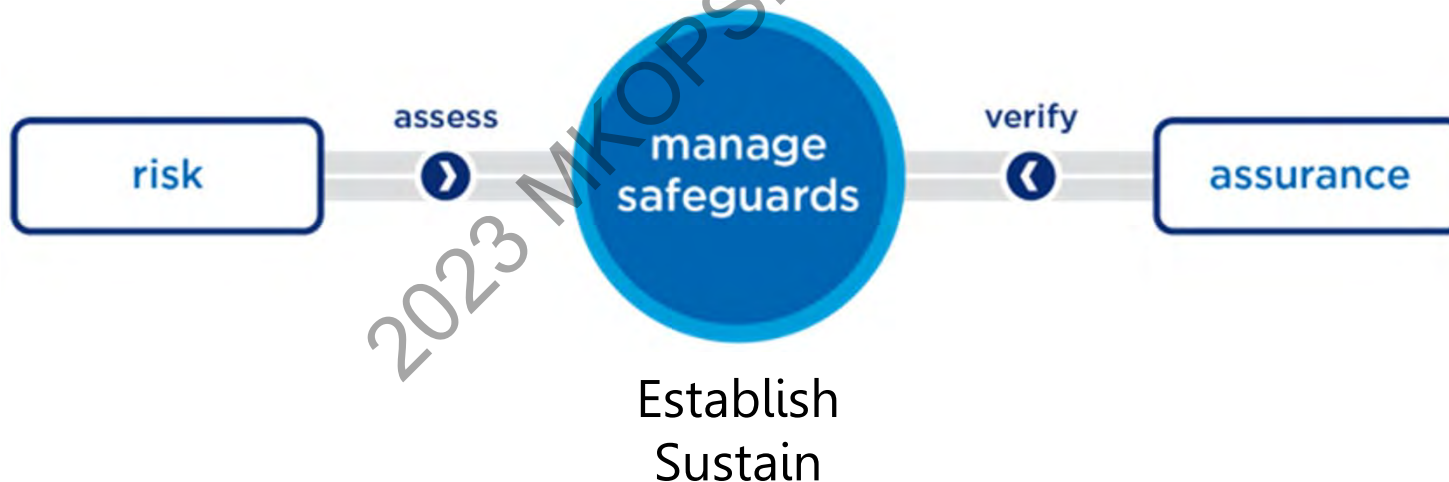
Agenda

- Basics of safeguards
- Why safeguards fail?
- Safeguard assurance

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Safeguard centric risk management

Prevent things from going wrong to make sure things go right.



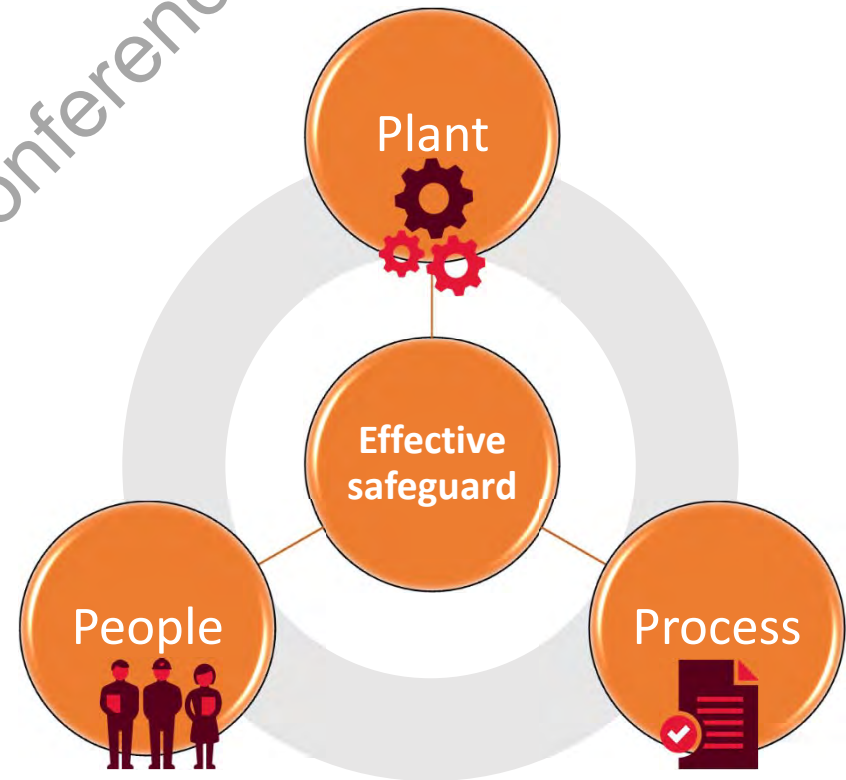
Safeguards – a measure to protect from harm or damage



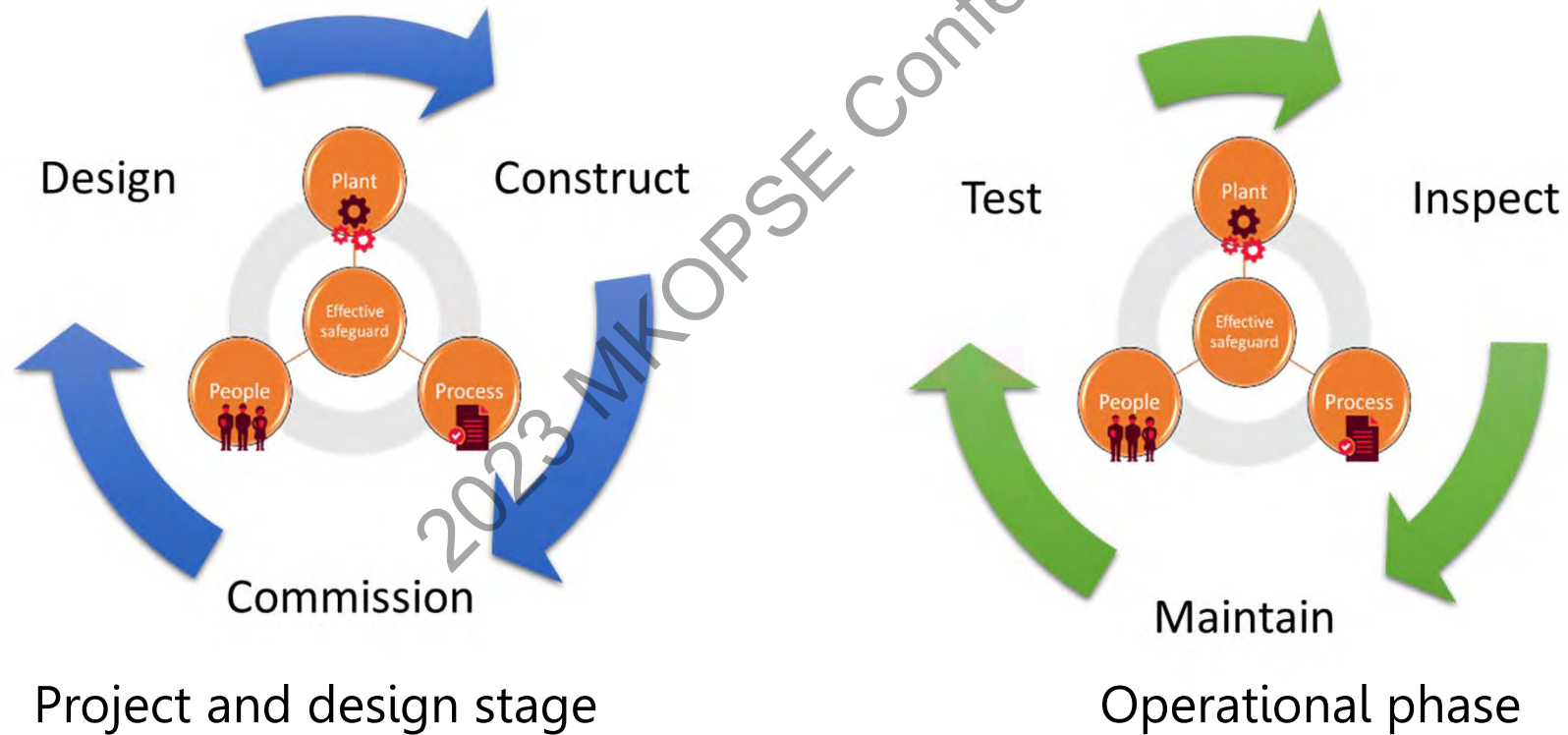
	Preventive safeguards	Mitigative safeguards
	prevent a loss of control over energy	reduce the severity, minimize impact
(i) leaks / hazardous material release	the primary equipment integrity management system, relief system.	Emergency shutdown, firewall, fire & gas detection, suppression system
(ii) vehicles and collision	Braking system, driver competence Alerts, Lane assist, electronic stability control	Seat belts, airbags

3Ps of Safeguard

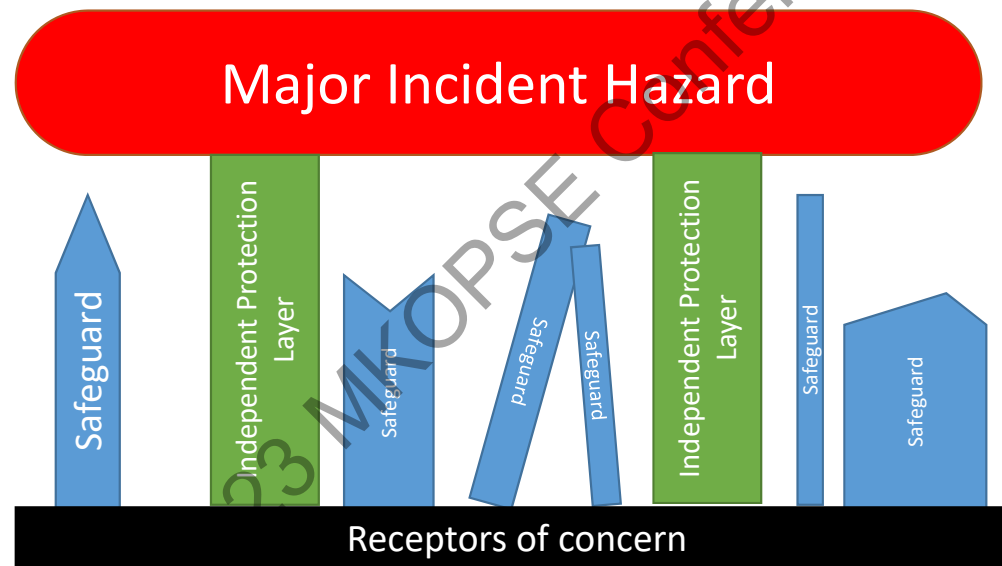
- **Plant** or the engineered devices and the physical barriers
- **Processes** or management systems to ensure that plant operations are safe and available when called for service.
- **People:** suitably qualified and experienced personnel to upkeep of the plant and the processes.



Safeguard – in place and effective



“All safeguards are not equally effective”

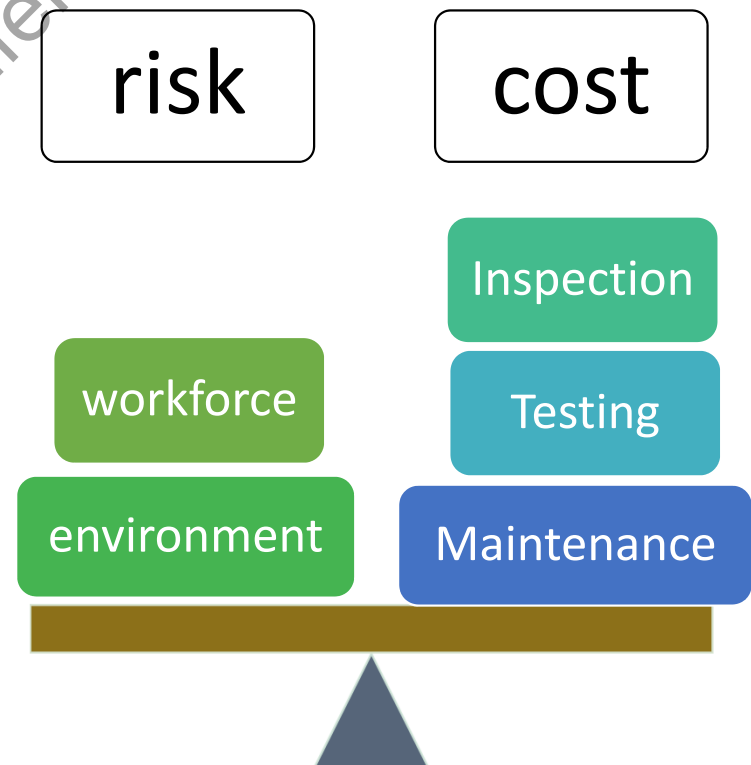


- Safeguard functionality
- Demand on the safeguard

“More is not necessarily safer”

- Resource (manhours, equipment, time) required for safeguard Inspection, Testing and Maintenance (ITPM).
- Safeguards should have functionality and workforce risk exposure from safeguard ITPM should be justified.


Safeguards should not create new hazards.



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Why do safeguards fail?

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Assurance and incident investigations

Typical findings:

- Safeguard not in place or
- Safeguard not effective

Failures:

- Engineering factors
- Human factors
- Life-cycle factors

Generally, major incidents occur due to the failure of more than one safeguard.

Failure reasons

Engineered safeguards

- Design aspects
 - Documentation, Risk-based
- Construction quality
- Commissioning
- Maintenance program inadequacy
- Inconsistency between records and what is in the field



Failure reasons

Human factors

- Competence of personnel
- Suitably qualified, experience, knowledge, skill
- Operational discipline

Life cycle considerations

- Changes on the demand during asset life
- Vendor support, life expectancy
- Spare part availability

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Safeguard testing

- Is the safeguard(s) in place and match the design specifications and meet the design intent?
 - Does the design meet the RAGAGEP?
 - Is safeguard functional?
- Asset integrity, availability, reliability.
- Competency:
 - Understand the design intent and are knowledgeable on responding when safeguard is on demand.
 - Maintenance and functional testing requirements.
- Systemic, recurring issues identified and addressed?

'who?' to 'what?'

- stop seeing workers as problems to be fixed
- blame and punish

Who failed?

What failed?

- start seeing workers as solutions to be harnessed
- learn and improve



Key take aways

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Effective safeguards are critical for risk management

- Establish and periodically review
 - Functionality, demand.
- Establish and maintain safeguard's 3Ps
 - People, Plant, and Process.
- Ensure safeguard is in place and effective throughout the lifecycle.
- Address change in demand.
- Consider inherently safer alternatives.





**“Safety is not the absence of accidents,
but the presence of safeguards”**

Todd Conklin

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Thank you

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Hierarchy of Safeguards

Strategic More reliable					Tactical Less Reliable		
Inherently Safer					Dependent on add-on Safeguards		
Elimination	Substitution	Minimization	Moderation	Simplification	Passive	Active	Procedural
No likelihood and no consequence	Reduce hazard Severity			Reduce the likelihood of the hazard	Reduce the Likelihood or Severity of a hazard		
	No Add-on Safety Systems				By Add-on Safety Systems		Human Centric
change the design or remove the need for hazardous material, equipment, activity	less dangerous material in a Process or Activity	smaller quantities of dangerous material inventory or limiting the hazardous activities	material in a less dangerous form or operating in less severe conditions	by designing processes, equipment, and procedures to eliminate opportunities for failures	available at all times but without the active functioning of the device	requires initiation during the event by active functioning of devices	by using administrative control procedures.

Hierarchy

Traditional Safety

- Preventing things from going wrong
- Safety is the absence of accidents

Safeguard centric

- Making sure things go right
- Safety is the presence of safeguards

Inherent Safety

- Absence of safeguard
- Minimum demand on safeguard



COMMUNITY EMERGENCY RESPONSE

PLANT EMERGENCY RESPONSE

PHYSICAL PROTECTION (DIKES, IMPOUNDS)

PHYSICAL PROTECTION (RELIEF DEVICES)

AUTOMATIC ACTION (ESD)

CRITICAL ALARMS, OPERATOR
SUPERVISION, MANUAL INTERVENTION

BASIC CONTROLS, PROCESS ALARMS,
OPERATOR SUPERVISION AND
MANUAL INTERVENTION

PROCESS DESIGN

WEAKER
PROTECTION





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7. US CSB Videos on incident investigation.

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Jeff Marx, P.E., Quest Consultants Inc.

- Principal Engineer; 30 years at Quest
- BSME, OU; MSME, GaTech
- Consequence & risk analysis, facility siting, building siting
- Serving full petrochemical industry; LNG, LPG, H2, pipelines
- CANARY software





A Comparative Study: Transporting Hydrogen or Ammonia

Jeff Marx & Ben Ishii

Quest Consultants Inc.
Norman, OK

www.questconsult.com



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Purpose

- Hydrogen as a transportation fuel: increasingly popular topic
- Primary use is gaseous hydrogen in fuel cells
- Gradual build-out of hydrogen fueling infrastructure
 - Hydrogen generation & storage
 - Hydrogen transportation
 - Hydrogen storage & fueling
- Limitations in gaseous hydrogen (GH₂) supply range/feasibility
- Proposals for alternate hydrogen carriers have emerged
 - Solids
 - Liquid hydrocarbons
 - Ammonia (NH₃)

Background and History

- 1766: Hydrogen identified as a discrete gas
- 1800: electrolysis
- 1800s
 - Early fuel cells (not vehicular)
 - Thermal reforming → town gas
- 1900s: hydrogen dirigibles
- 1931: methane reforming (produced H_2 from CH_4)
- 1950s/60s: NASA uses H_2 as propellant and in fuel cells
- 1970s-2000s: hydrogen-fueled vehicle research
- 2010s: Commercial hydrogen fuel cell passenger vehicles



Etienne Lenoir's "Hippomobile"

Hydrogen as a Vehicular Fuel

- Mostly hydrogen fuel cell electric vehicles (HFCEVs)
- Some internal combustion hydrogen engines
- Hydrogen market is mature...
 - Petrochemical applications
 - Industrial gases: generation, distribution
- Vehicular fueling infrastructure small but growing
 - Mostly compressed gaseous transports, storage
 - Some liquid hydrogen storage with regas/fueling
- Need extensive production, transportation, storage, fueling network

Ammonia as a Fuel?

- Ammonia is a mature market – fertilizers and others
- Direct combustion possible, but...
 - Energy density lower than other liquid fuels
 - Fuel storage technology different (in comparison)
 - Engines may need fuel spiking to maintain sufficient compression ratios
 - NO_x formation high
- Fuel cell use?
 - Ammonia is typically poisonous to fuel cells
 - Solid-oxide fuel cells (SOFC) show promise for NH₃ use
- Or.... Just use ammonia as a hydrogen carrier



Comparison Case

- Assume a hydrogen production and distribution network for vehicular fueling (HFCEVs)
- Beginning is hydrogen production
- End is gaseous fueling systems
- Consider four transportation options:
 1. Moderate pressure gaseous hydrogen
 2. High pressure gaseous hydrogen
 3. Liquid hydrogen
 4. Liquid ammonia

Comparison Cases

1. MP GH2 transport, tube trailer: (9) 40'x22"ID



2. HP GH2 transport: (75) Al/carbon fiber cylinders



Comparison Cases

3. LH2 transport: 15,000 gallon vacuum-insulated vessel



4. Ammonia transport: 12,600 gallon pressurized vessel



How to Evaluate?

- Technical feasibility? ✓
- Economic? Market demand analysis? ✗
- Life cycle analysis? ✗
- Energy balance? ✗
- “Hydrogen Logistics” ✓
- Consequence Analysis ✓
- Risk Analysis



Hydrogen Logistics

System	Transportation Type	Available Storage Volume [ft ³]	Total Mass Transported [lb]	KiloMoles Hydrogen Transported	Equivalent Tube Trailers
1	Moderate Pressure Gaseous Hydrogen (tube trailer)	950	779	175	1



Hydrogen Logistics

System	Transportation Type	Available Storage Volume [ft ³]	Total Mass Transported [lb]	KiloMoles Hydrogen Transported	Equivalent Tube Trailers
1	Moderate Pressure Gaseous Hydrogen (tube trailer)	950	779	175	1
2	High Pressure Gaseous Hydrogen (HP tube trailer)	848	1,512	340	1.94



Hydrogen Logistics

System	Transportation Type	Available Storage Volume [ft ³]	Total Mass Transported [lb]	KiloMoles Hydrogen Transported	Equivalent Tube Trailers
1	Moderate Pressure Gaseous Hydrogen (tube trailer)	950	779	175	1
2	High Pressure Gaseous Hydrogen (HP tube trailer)	848	1,512	340	1.94
3	Cryogenic Hydrogen	2,005	9,309	2,095	11.95



Hydrogen Logistics

System	Transportation Type	Available Storage Volume [ft ³]	Total Mass Transported [lb]	KiloMoles Hydrogen Transported	Equivalent Tube Trailers
1	Moderate Pressure Gaseous Hydrogen (tube trailer)	950	779	175	1
2	High Pressure Gaseous Hydrogen (HP tube trailer)	848	1,512	340	1.94
3	Cryogenic Hydrogen	2,005	9,309	2,095	11.95
4	Liquefied Ammonia	1,432	53,993	2,158	12.31



Consequence Analysis

- Definition: The use of mathematical models to predict the potential extent of specific hazard zones or effect zones that would result from specific accident event sequences
- Context is transportation of hydrogen (or hydrogen carrier)
 - Truck-based road transport
 - Vehicular accident causes a loss of containment
- Hazards introduced to the surrounding area

Consequence Analysis

- Tube trailers use 9/16" tubing, occasionally 1/2" tubing
- Liquid hydrogen trailers 1" or 1.5" piping
- Liquid ammonia trailers 2" or 3" piping
- How to evaluate on an equal basis?
 - ◆ Set release hole size to 1/2"
 - ◆ Assumed discharge from:
 1. MPGH2: 1 of 9 tubes
 2. HPGH2: 5 of 75 tubes
 3. LH2: container
 4. NH3: container

Consequence Analysis

- Hazard Definition
 - Gaseous hydrogen: flash fire, jet fire, VCE
 - Liquid hydrogen: cryogenic exposure, flash fire, jet fire, VCE
 - Ammonia: toxic vapor cloud

Hazard Type	Injury Level	Threshold of Fatality Level
Flammable Vapor Cloud	Extent of released gas mixed to the lower flammable limit (LFL) in air	
Thermal Radiation	1,600 Btu/hr-ft ² for 30 second exposure; results in 2 nd degree burns to unprotected skin	4,000 Btu/hr-ft ² for 20-30 second exposure; potential fatality due to burns
Toxic Gas	Extent of released gas mixed to the AEGL-2 level, 10-minute exposure	Extent of released gas mixed to the AEGL-3 level, 10-minute exposure



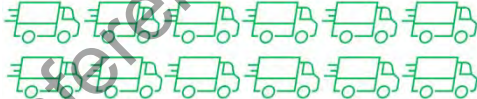



CANARY
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Consequence Analysis Results

System	Transportation Type	Release Rate [lb/sec]	Event Duration	Distance to Threshold of Fatality [feet]	Distance to Injury [feet]
1	Moderate Pressure Gaseous Hydrogen (1 of 9 tubes)	1.074	> 4 minutes	35	40
2	High Pressure Gaseous Hydrogen (5 of 75 tubes)	1.53	< 3 minutes	55	60
3	Cryogenic Hydrogen	1.635	> 1 hour	80	80
4	Liquefied Ammonia	5.34	> 1 hour	1,050	3,500

Qualitative Risk Assessment

- Set MP GH2 (tube trailer) as basis 
- HP GH2 Consequences approximately equal 
- LH2 consequences slightly larger
- Ammonia consequences much larger 
- Assuming an equal accident rate per mile, hydrogen options would have similar risk corridors, ammonia larger 
- On a risk (probability) basis: LH2 < HPGH2 < MPGH2 < NH₃



Concluding Remarks

- Transport of GH₂ seems to favor higher pressures
- Transport of LH₂ slightly less risky, but more complicated
- Use of ammonia as a carrier reduces the probability of accident scenarios, but introduces significant toxic impacts and system complexity
- Conversion to, and reforming from, ammonia requires extra resources (equipment, energy, plot space...)
- Ammonia may or may not fit the needs of a given market



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Thank You!

Jeff Marx, jdm@questconsult.com

Process Safety and Risk Management Services



MKOC 2023 - Explosion Workshop

Ali Rangwala, Ph.D.
Alfonso F. Ibarreta, Ph.D., PE, CFEI

Mary Kay O'Connor Process Safety Conference,
October 13, 2023

Ali Rangwala, Ph.D.

- Professor of Fire Protection Engineering at WPI, Worcester, MA
- Education
 - Ph.D. in Mechanical and Aerospace Engineering, University of California, San Diego
- Interests
 - Combustion
 - Industrial fire protection
 - Explosion protection
 - Combustible dust



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Alfonso Ibarreta , Ph.D., PE, CFEI

- Managing Engineer at Exponent, Natick, MA
- Education
 - Ph.D. in Aerospace Engineering, University of Michigan
- Interests
 - Vapor cloud explosions
 - Explosion protection of process equipment
 - Combustible dust
- Memberships
 - NFPA Technical Committee on Explosion Protection Systems
 - Mechanical engineering representative at the Massachusetts Board of Fire Prevention Regulations



Presentation Outline (1/2)

- **PART I - Deflagration and Explosion Fundamentals**
 - Introduction to explosions and flammability (Dr. Ibarreta)
 - Case studies of gas explosions (Dr. Rangwala)
- **PART II – Closed Vessel Deflagrations**
 - Theory and calculations (Dr. Rangwala)
 - Explosion prevention methods (Dr. Ibarreta)

Presentation Outline (2/2)

- **PART III – Vented Explosions**
 - **Analysis methods (Dr. Rangwala)**
 - **Explosion protection via deflagration venting (NFPA 68) (Dr. Ibarreta)**

TYPES OF EXPLOSIONS

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Definitions - I

- **Explosion:** The sudden conversion of potential energy (chemical or mechanical) into kinetic energy with the release of gas(es) under pressure. These gases then do mechanical work such as defeating their confining vessel or moving, changing, or shattering nearby materials. [NFPA 921]
- **Deflagration:** Propagation of a combustion zone at a velocity that is less than the speed of sound in the unreacted medium.[NFPA 68]
- **Detonation:** Propagation of a combustion zone at a velocity greater than the speed of sound in the unreacted medium. [NFPA 921]

Definitions - II

- **Flammable Gas**: Any substance that exists in the gaseous state at normal atmospheric temperature and pressure and is capable of being ignited and burned when mixed with the proper proportion of air, oxygen, or other oxidizers. [NFPA 2]
- **Flammable Liquid**: A liquid with a closed-cup flash point below 100 °F (37.8 °C) and Reid vapor pressures not exceeding 40 psia at 100 °F (37.8 °C) [NFPA 30]
- **Explosive**: Any chemical compound, mixture, or device, the primary or common purpose of which is to function by explosion. [NFPA 495]

Explosions

- **Types of Explosions (NFPA 921)**
 - **Mechanical Explosion**
 - Pressure vessel burst
 - Boiling Liquid Expanding Vapor Explosion (BLEVE)
 - **Combustion Explosion**
 - Flammable gases
 - Vapors of flammable liquids
 - Combustible dust
 - Chemical Explosion
 - Electrical Explosion
 - Nuclear Explosion

Combustion Explosion

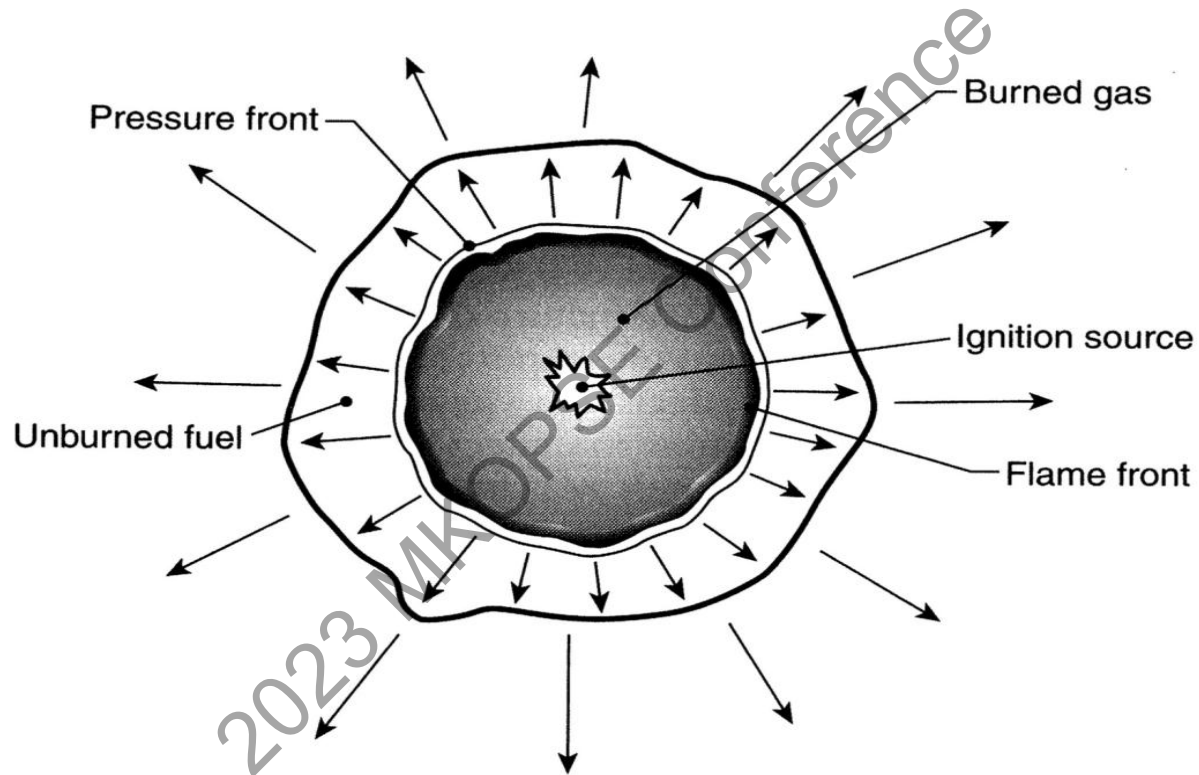
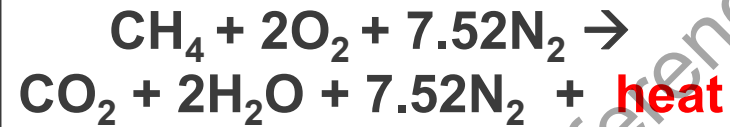


FIGURE 21.4.1.4(a) Idealized Propagating Flame and Pressure Fronts [After Harris (1983) p.3]

Gas Expansion During Combustion Explosion



1 ft³
methane

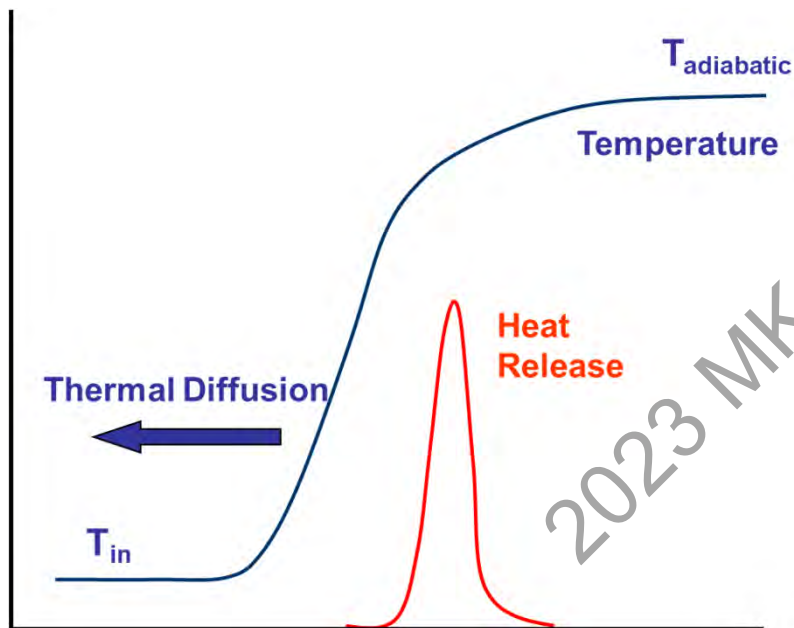
10.5 ft³
stoichiometric
mixture

X 7.6

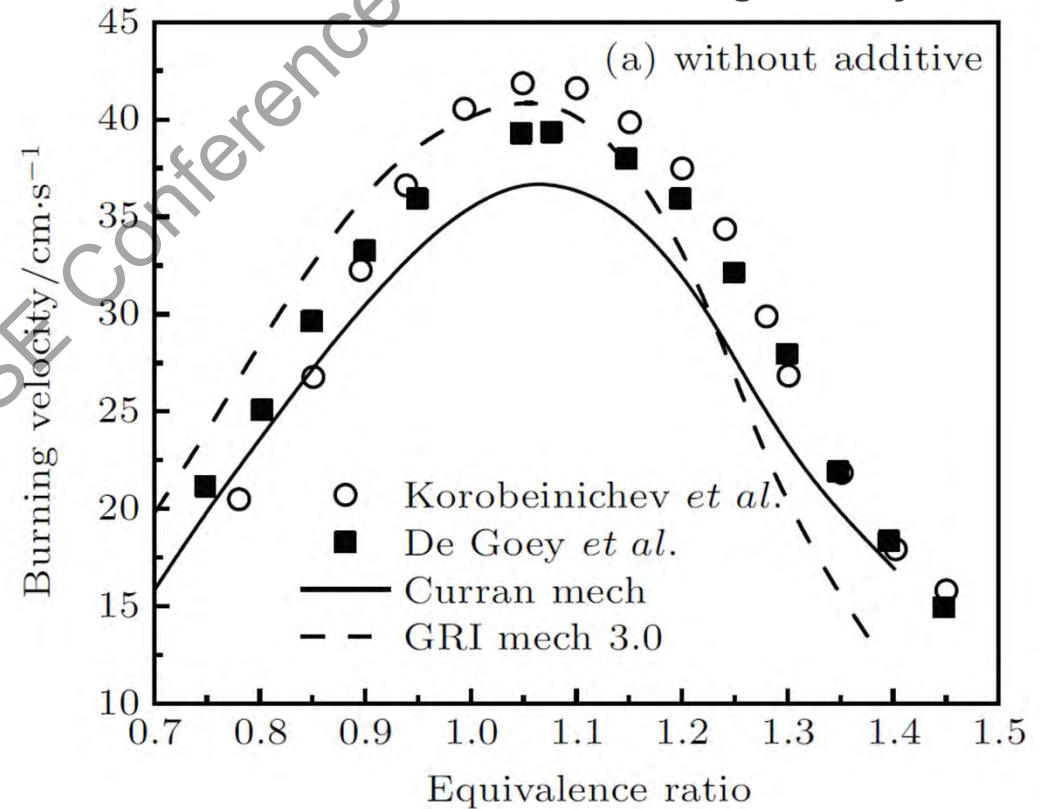
~80 ft³
combustion
products

Flame Propagation and Burning Velocity

Premixed Flame Structure

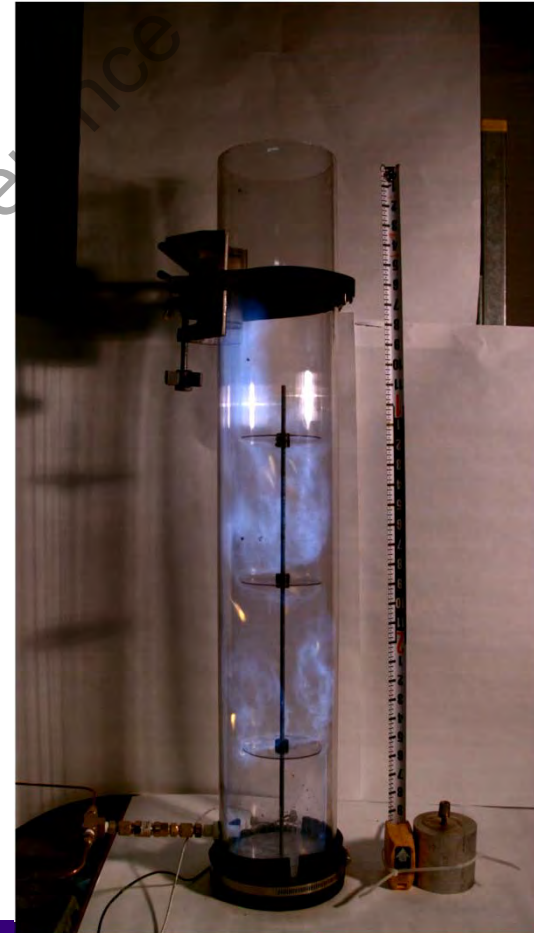
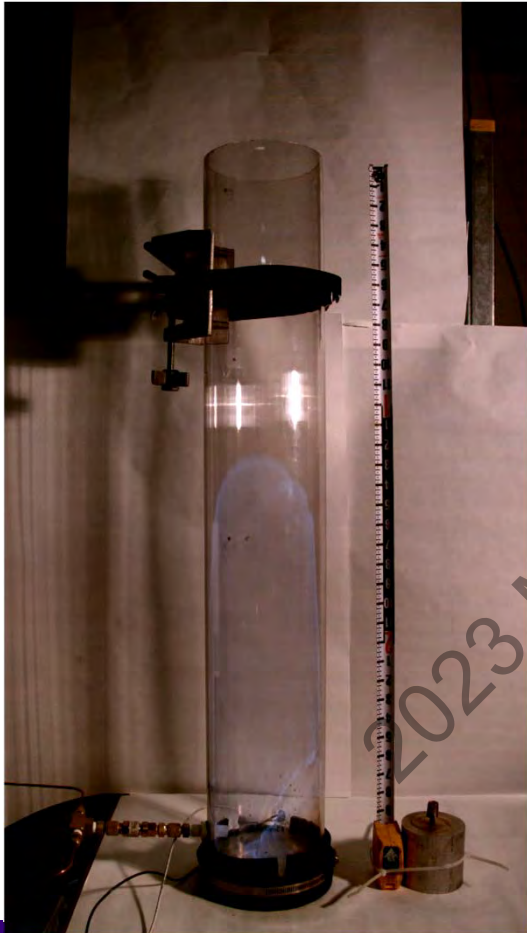


Methane/Air Flame Burning Velocity



Source: Yin et al. "Physical and chemical effects of phosphorus-containing compounds on laminar premixed flame" Chin. Phys. B Vol. 27, No. 9 (2018) 094701

Effect of Congestion – Propane / Air Flame



Confined Deflagration

- Reaction wave propagates below speed of sound.
- Confinement required to generate significant overpressure.
- Relatively uniform pressure in an enclosure.



Photograph taken by Exponent

Vapor Cloud Explosion (VCE)

- Reaction wave propagates below speed of sound.
- Overpressure generated by congestion over large area.
- Pressure no longer uniform. Pressure pulse travels as a wave ahead of combustion front.



Tests performed by BakerRisk for the 2001 Explosion Research Cooperative

VCE Pressure Wave Propagation

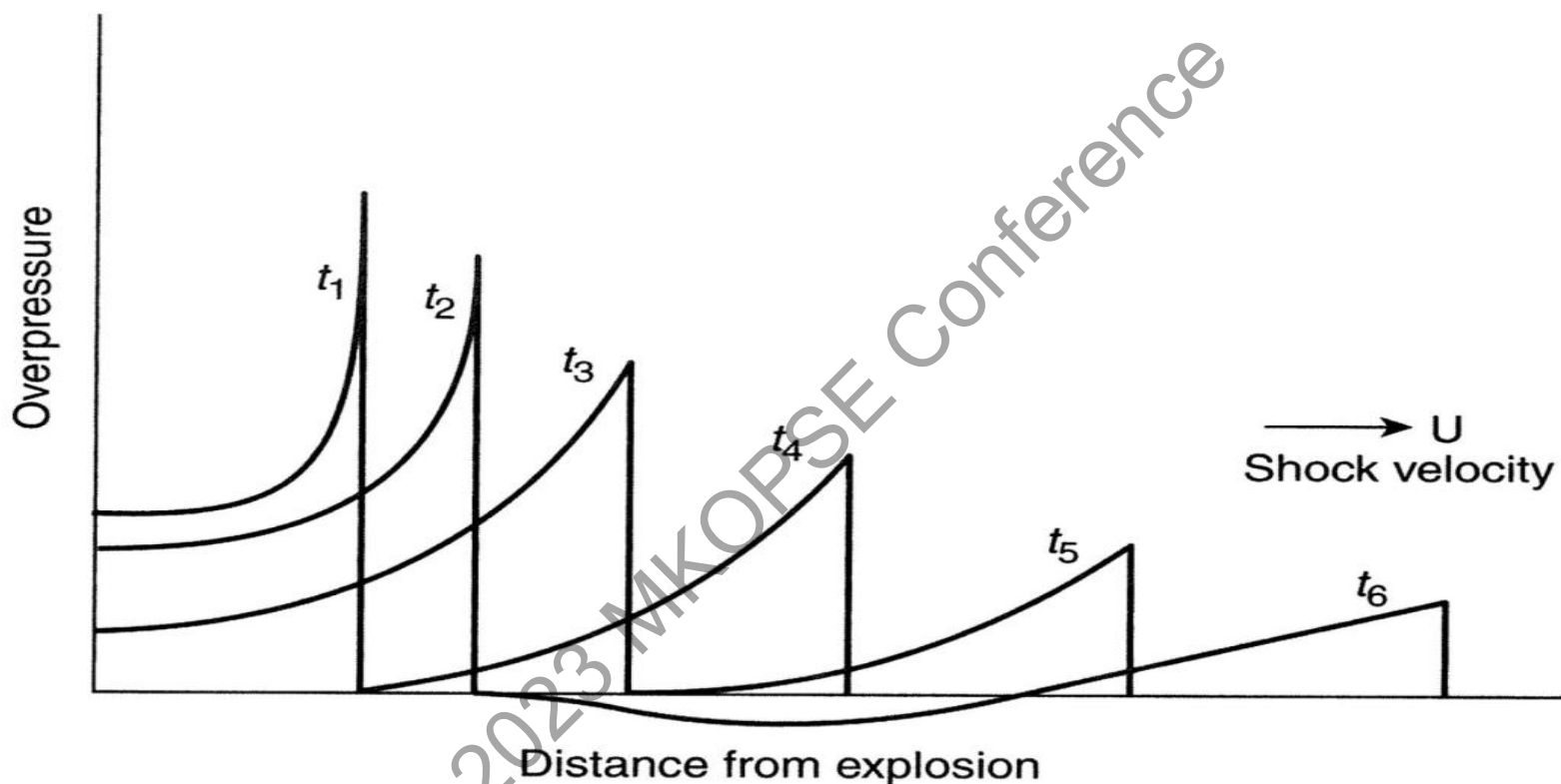


FIGURE 21.4.1.4.3 Typical Overpressure History at Locations Distant from Center of Explosion.

Methane VCEs

Low Congestion



High Congestion



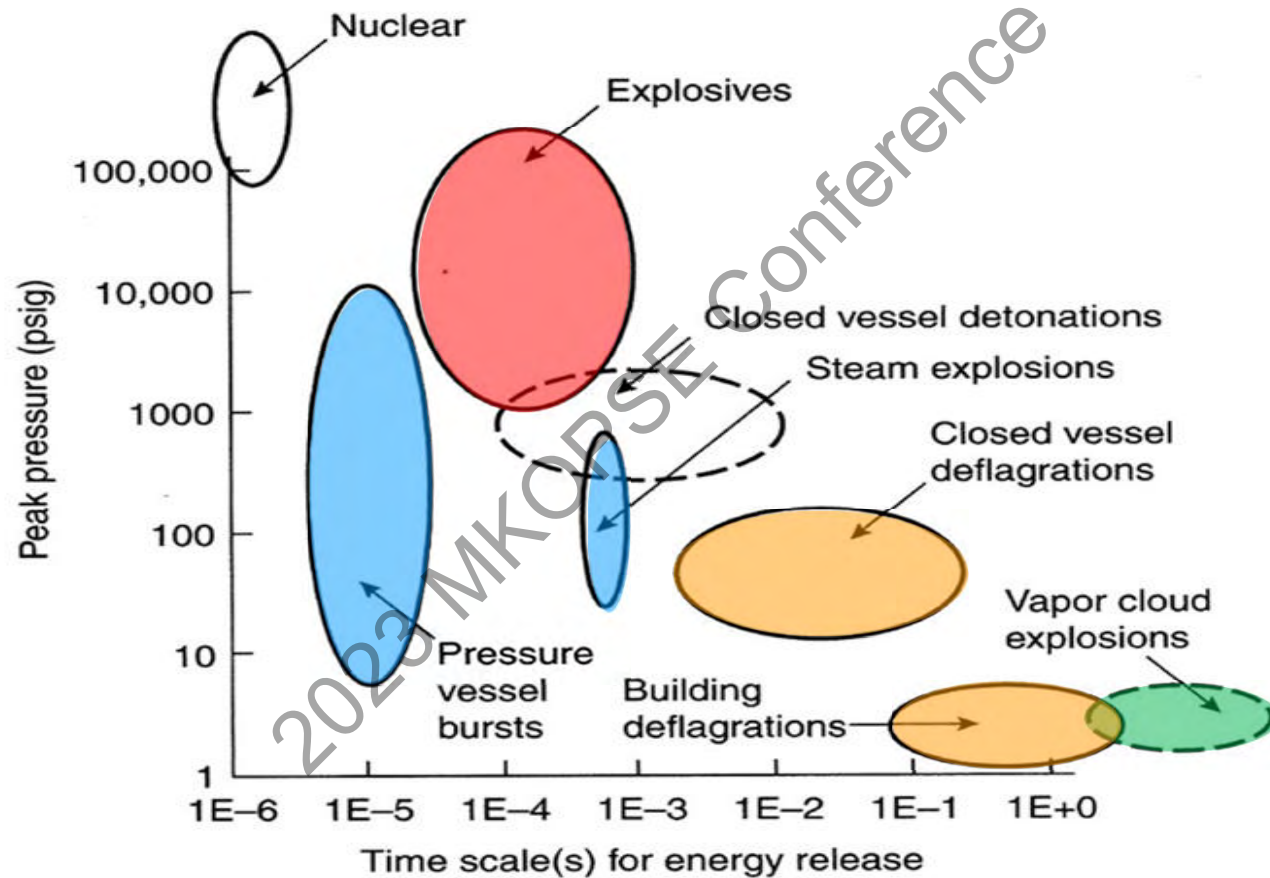
Tests performed by BakerRisk for the 2001 Explosion Research Cooperative

Detonation

- Reaction wave propagates above speed of sound
- Very high, localized pressure
- Localized shattering of objects

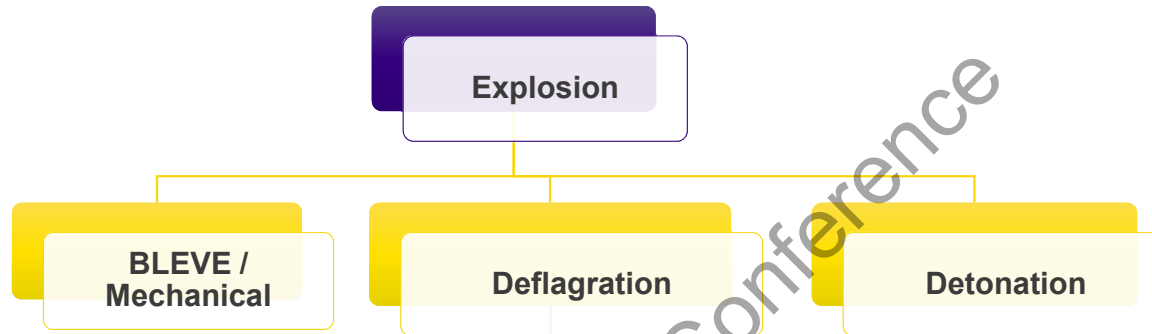


Vapor Cloud Explosion Pressure Scale Comparison



Analysis of Main Explosion Categories

• $P \cdot V$ energy
+ TNT Model



• TNT
Model

Damage Overpressures

Component	PSI (for failure)
Shattering of glass windows	0.5 - 1.0
Threshold for Injury from flying glass	0.6
Partial collapse of walls and roofs of houses	2.0
Lower limit of serious structural damage	2.3
50% destruction of brickwork house	2.5
1% Eardrum Rupture	3.4
Loaded train wagons overturn	7.0
Threshold lung hemorrhage	10.0

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FLAMMABILITY OF GASES



Fire Tetrahedron

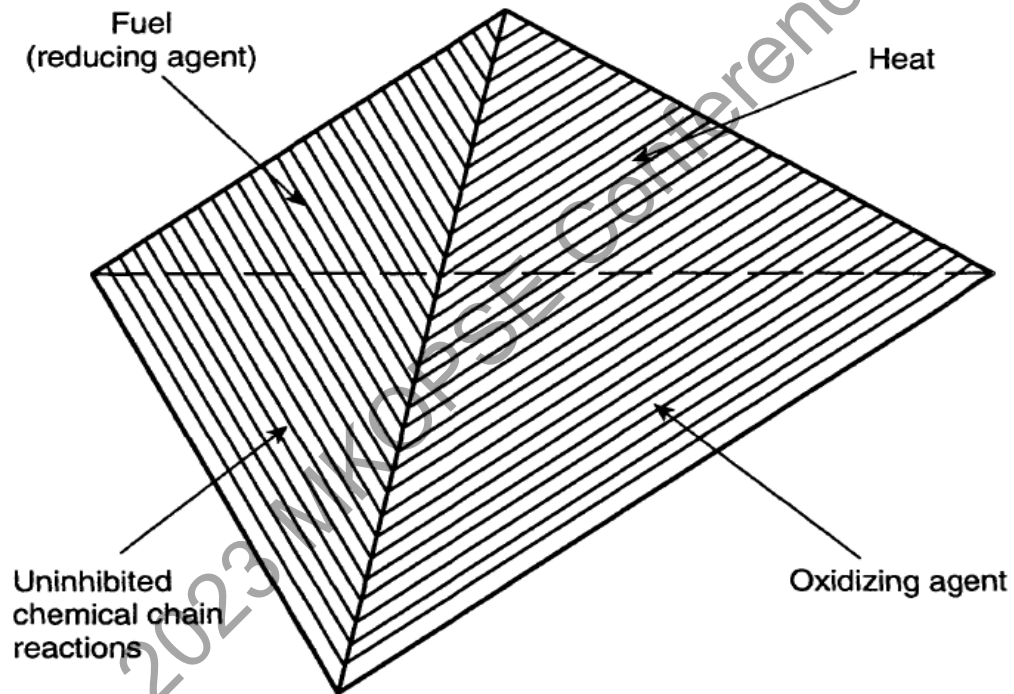
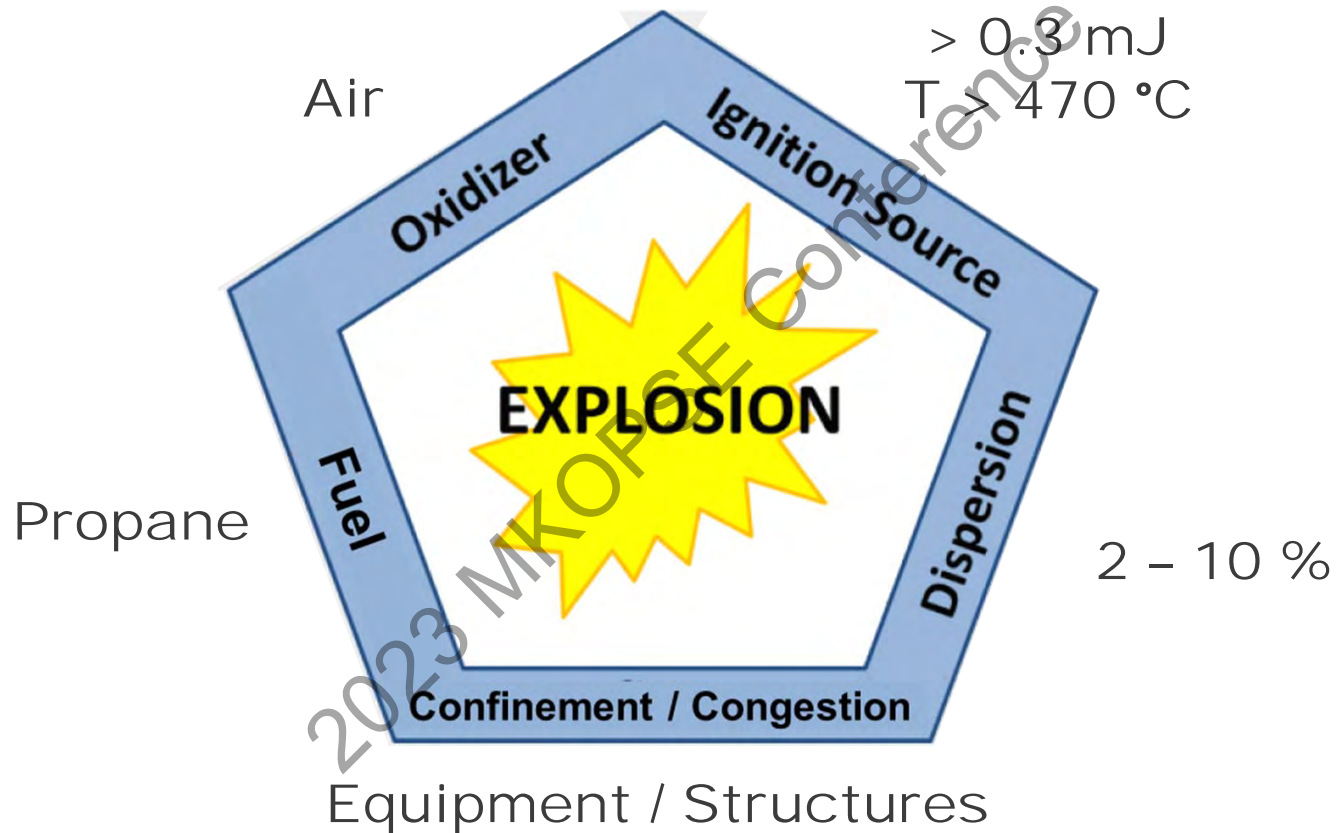
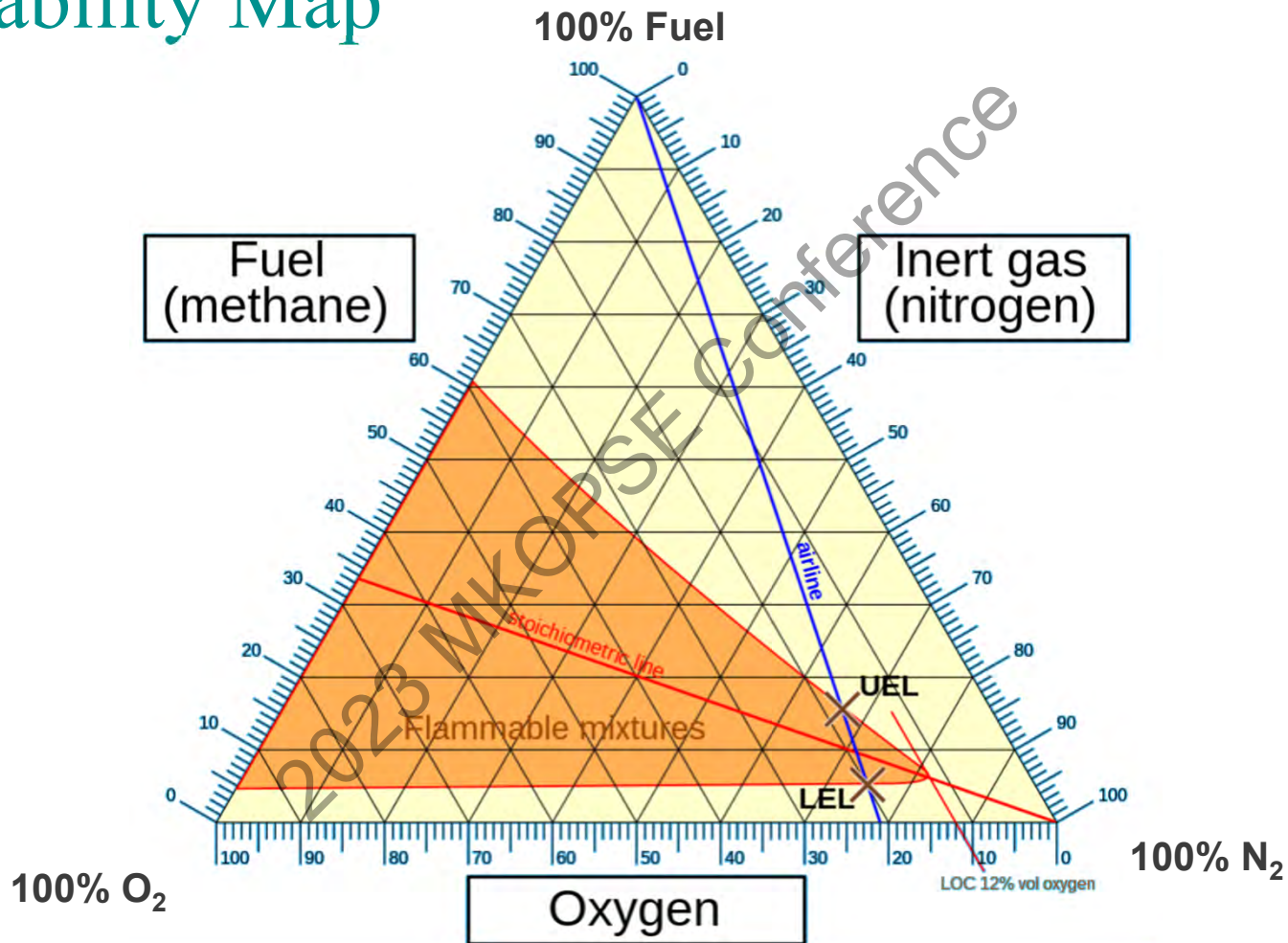


FIGURE 5.1.2 Fire Tetrahedron.

Explosion Pentagon



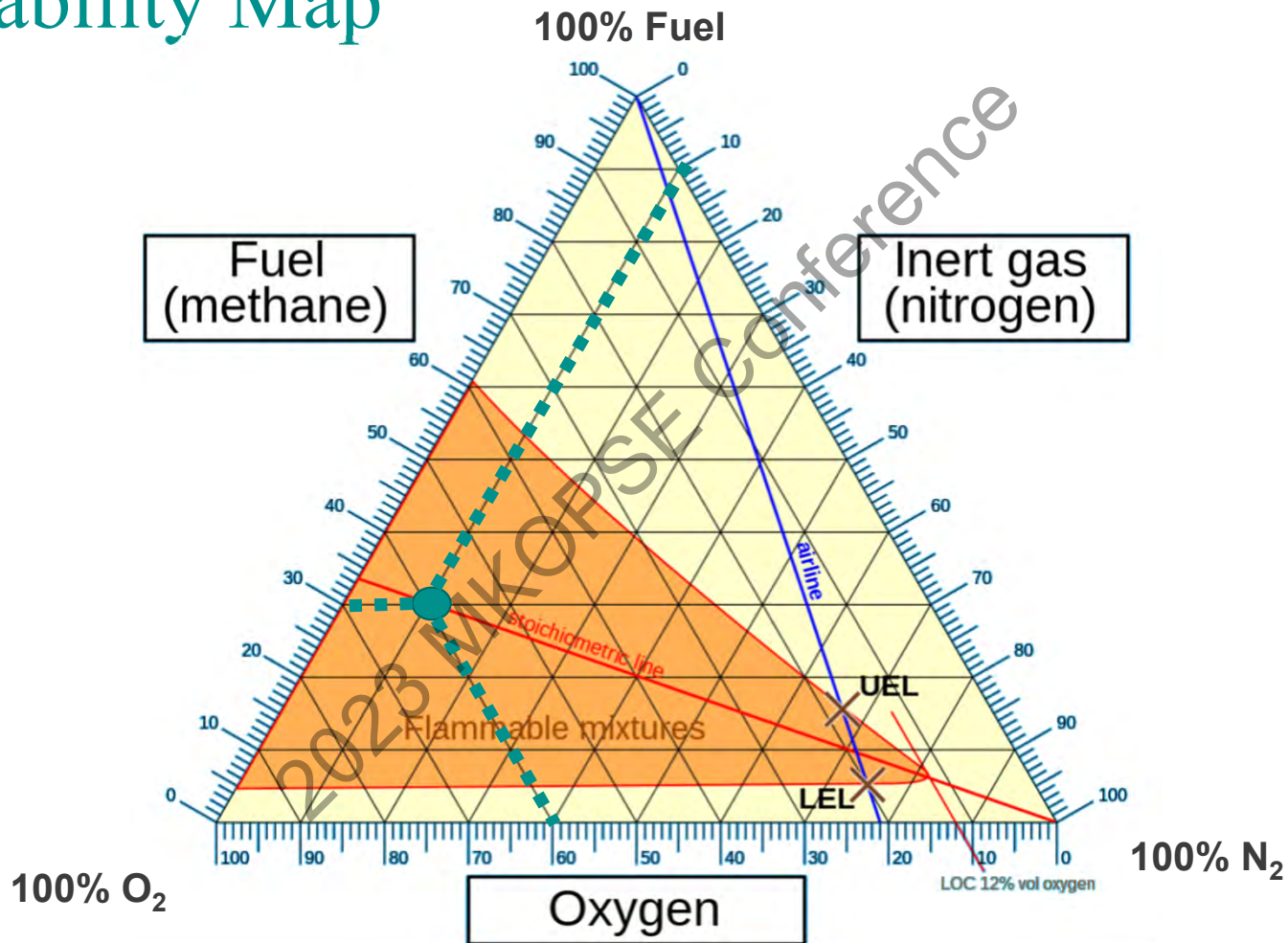
Flammability Map



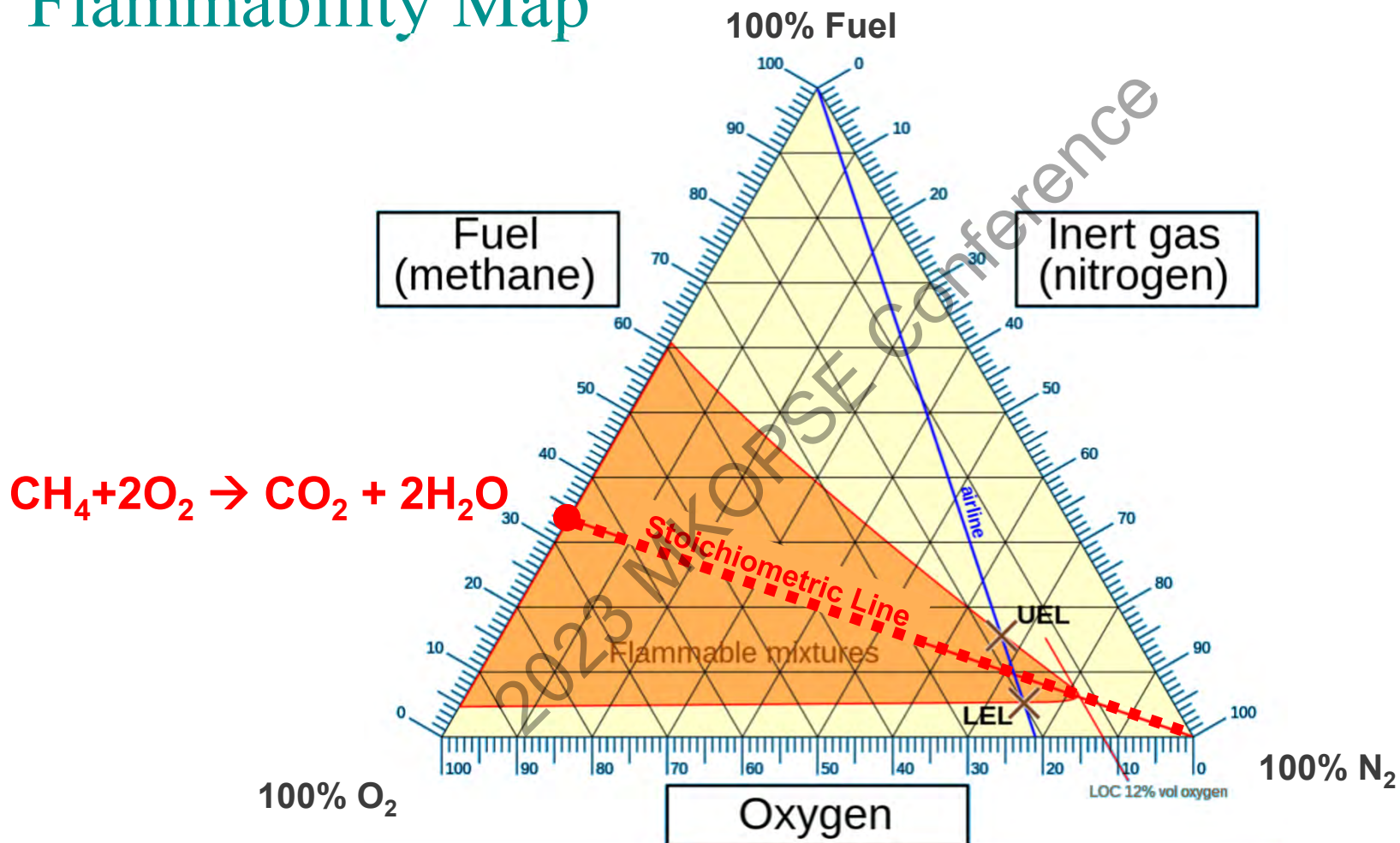
Flammability Map

Point:

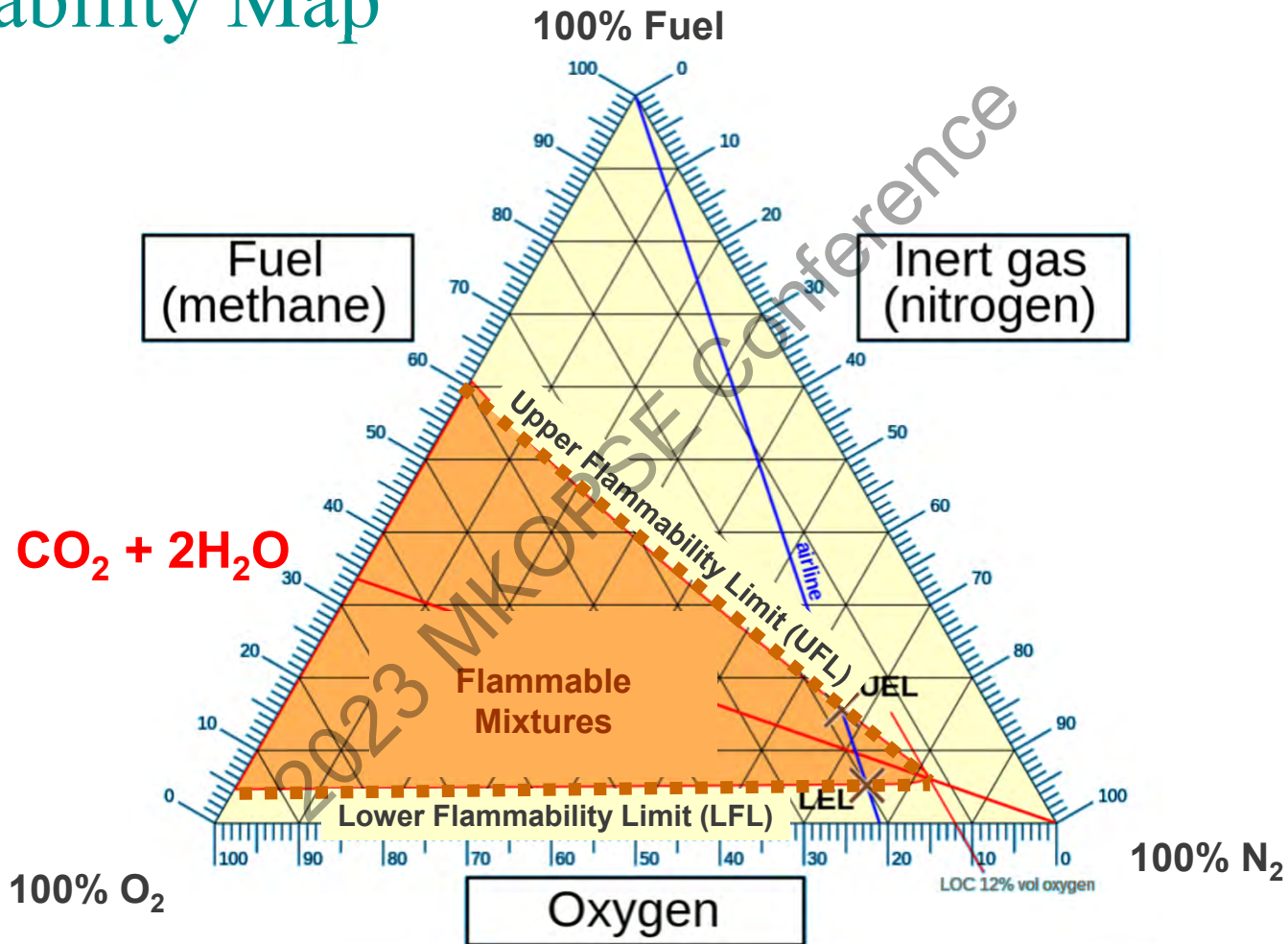
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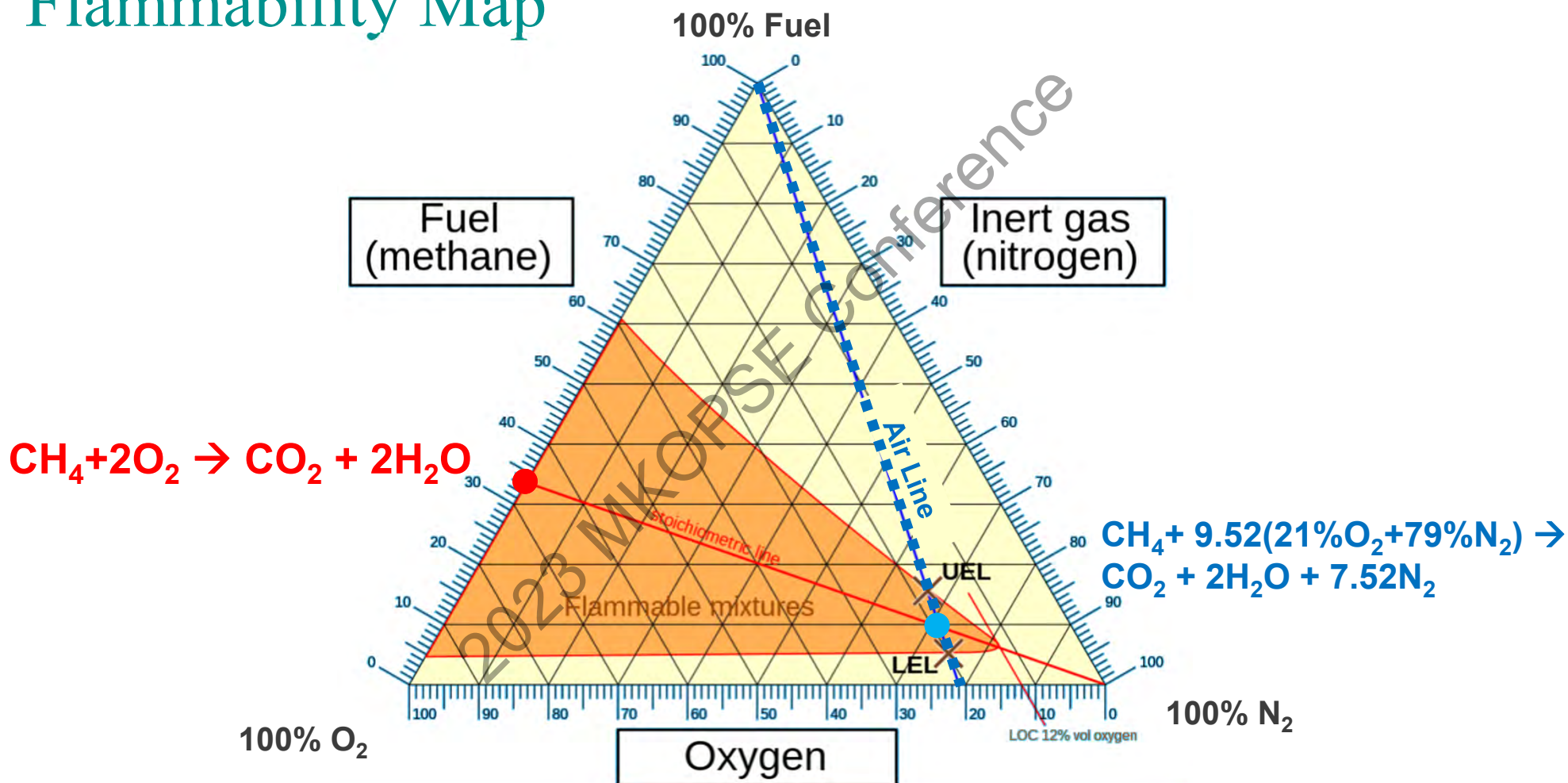
Flammability Map



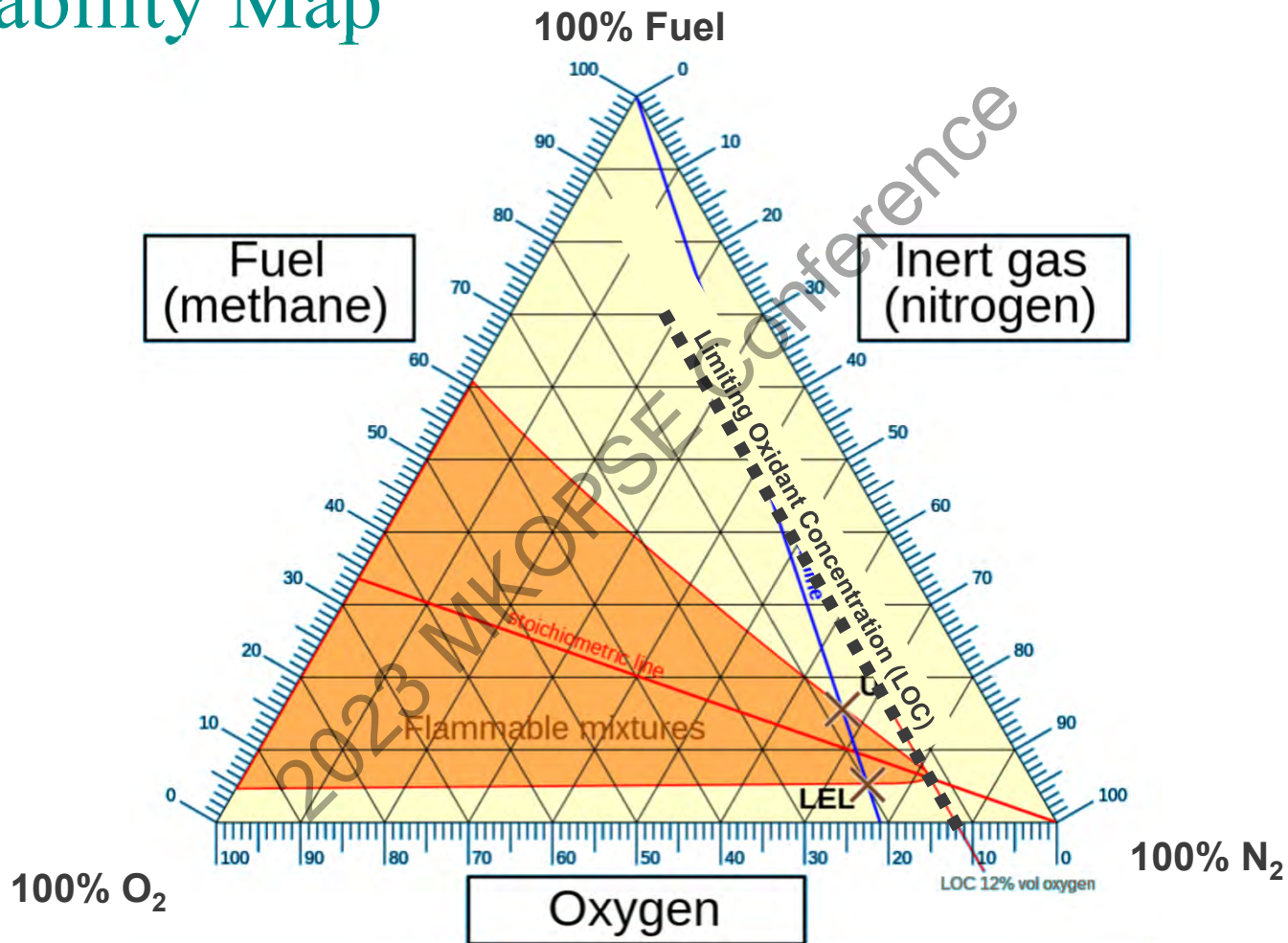
Flammability Map



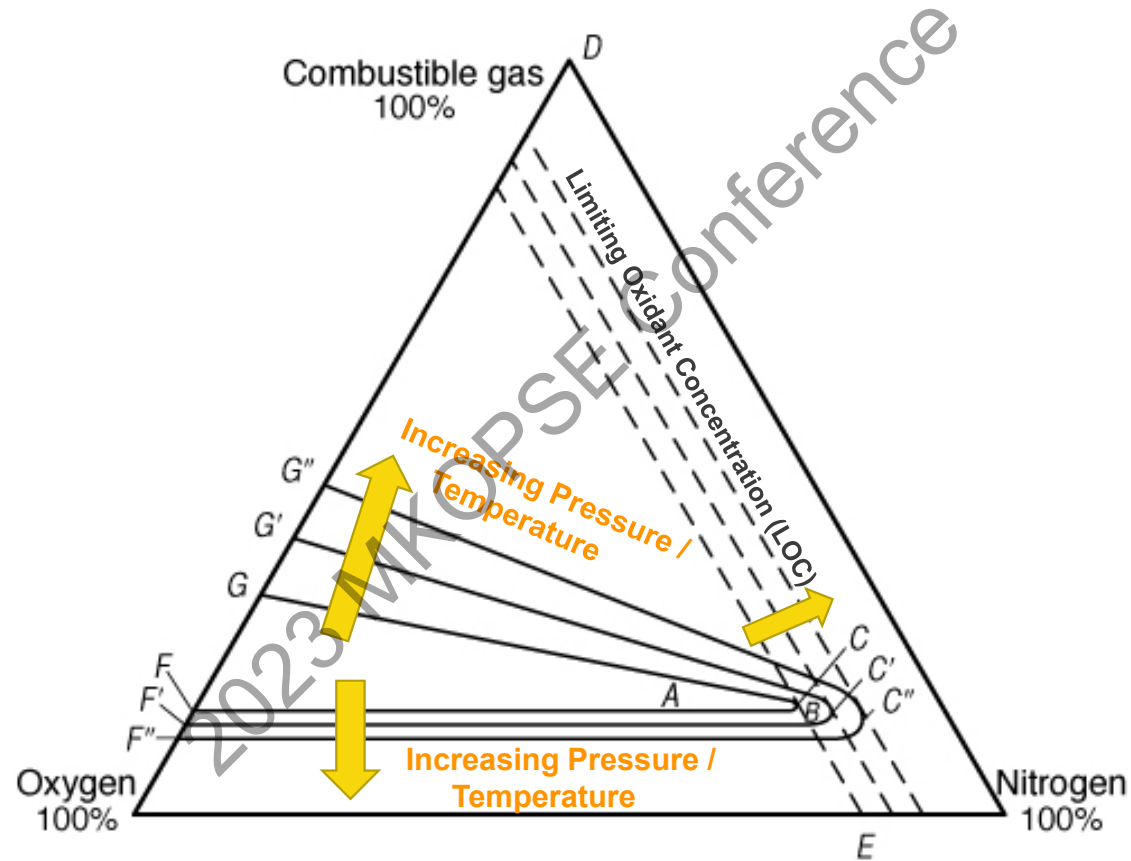
Flammability Map



Flammability Map



Effect of Pressure / Temperature on Flammability



Flammability / Explosibility Parameters

- **Flammable Gases**

- Laminar Burning Velocity
- Lower and Upper Flammability Limits (LFL/UFL)
- Limiting Oxidant (Oxygen) Concentration (LOC)
- Minimum Ignition Energy (MIE)
- Minimum Autoignition Temperature (MAIT)
- Hot surface ignition temperature

- **Flammable Liquids (additional)**

- Flash point
- Vapor Pressure / Boiling Temperature

Minimum Ignition Energy (MIE)

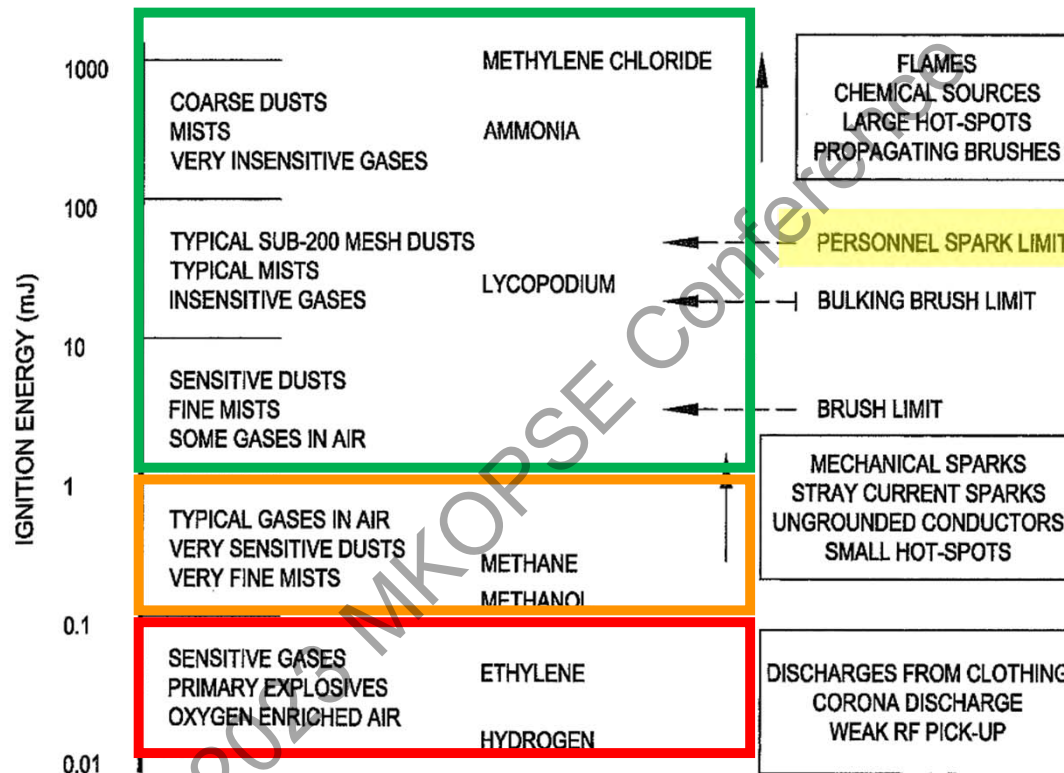


Figure 1.4. Ignition energies of various materials and types of ignition source that may ignite them (updated from Britton, 1999).

Potential Ignition Sources

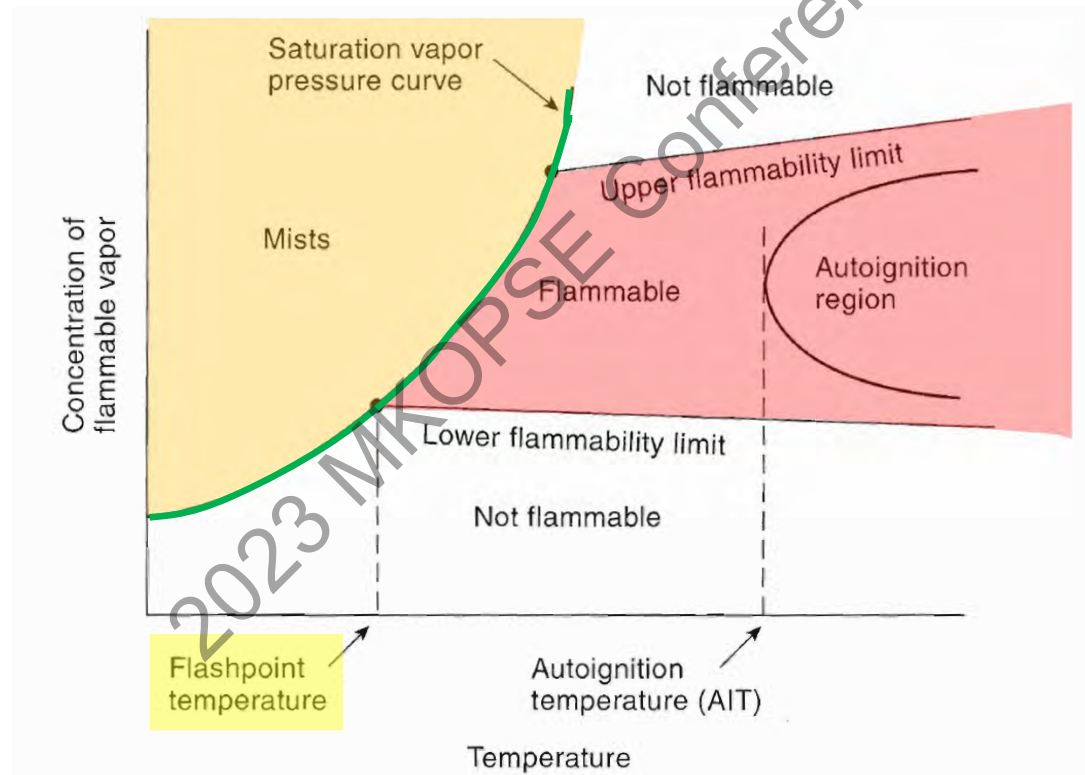
- Open flames and hot work
- High temperature sources
 - Hot surfaces
- Electrical sources
 - Powered equipment
 - Electrostatic accumulations
- Physical sources
 - Compression
 - Friction / impact
- Chemical sources
 - Catalytic materials
 - Pyrophoric materials

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FLAMMABILITY OF LIQUIDS



Flammability Limits





Take a
Break

Mechanical Explosion – Pressure Vessel Burst



BLEVE

- Boiling Liquid Expanding Vapor Explosion (BLEVE)
- Portion of liquid evaporates and expands after vessel rupture, converting thermal energy to mechanical energy.



Source:

<https://www.slideshare.net/HARSHALKHODE1/bleve-52334425>

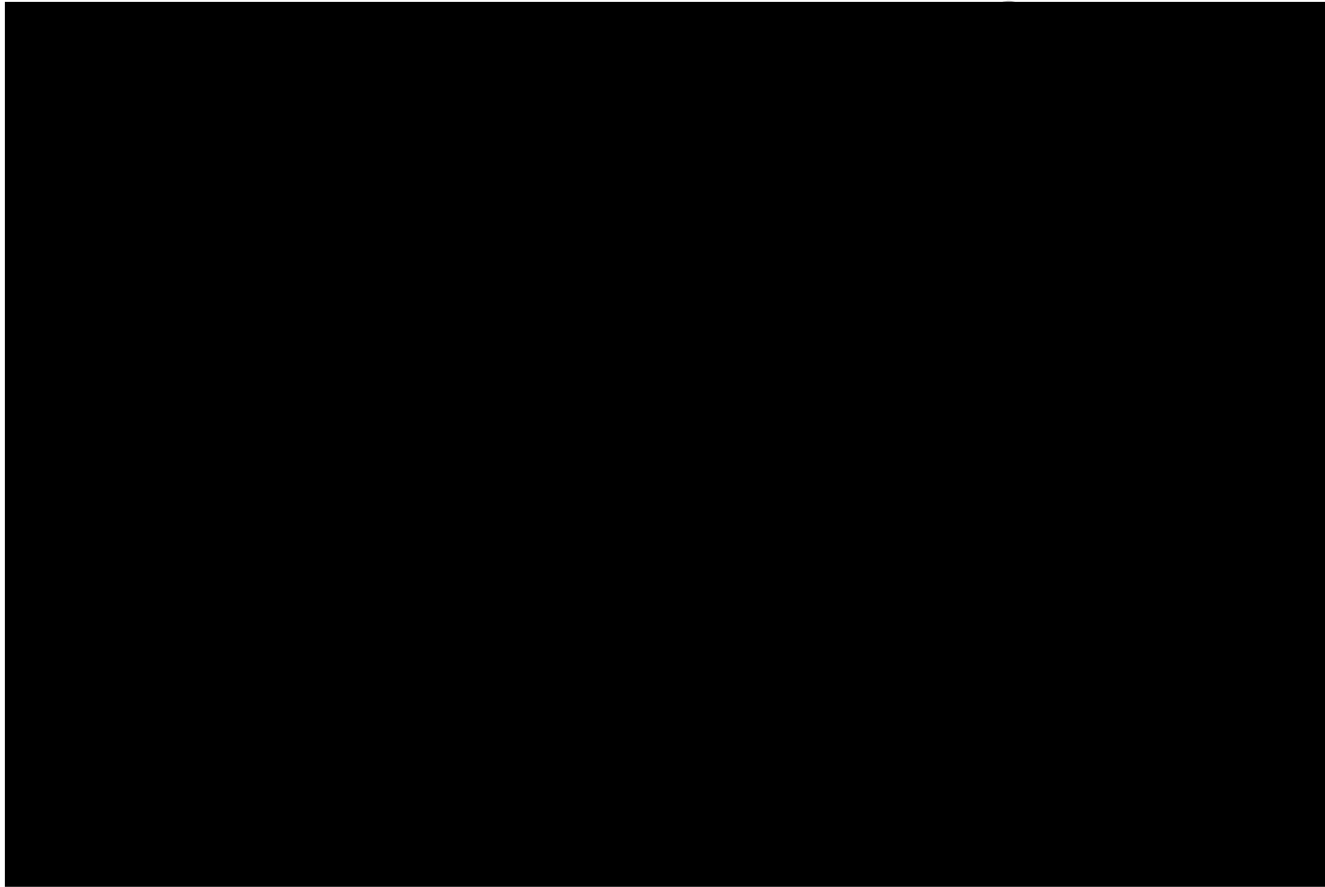
Low Reactivity - Methane (2D Confinement and Low Congestion)



Low Reactivity - Methane (2D Confinement and High Congestion)

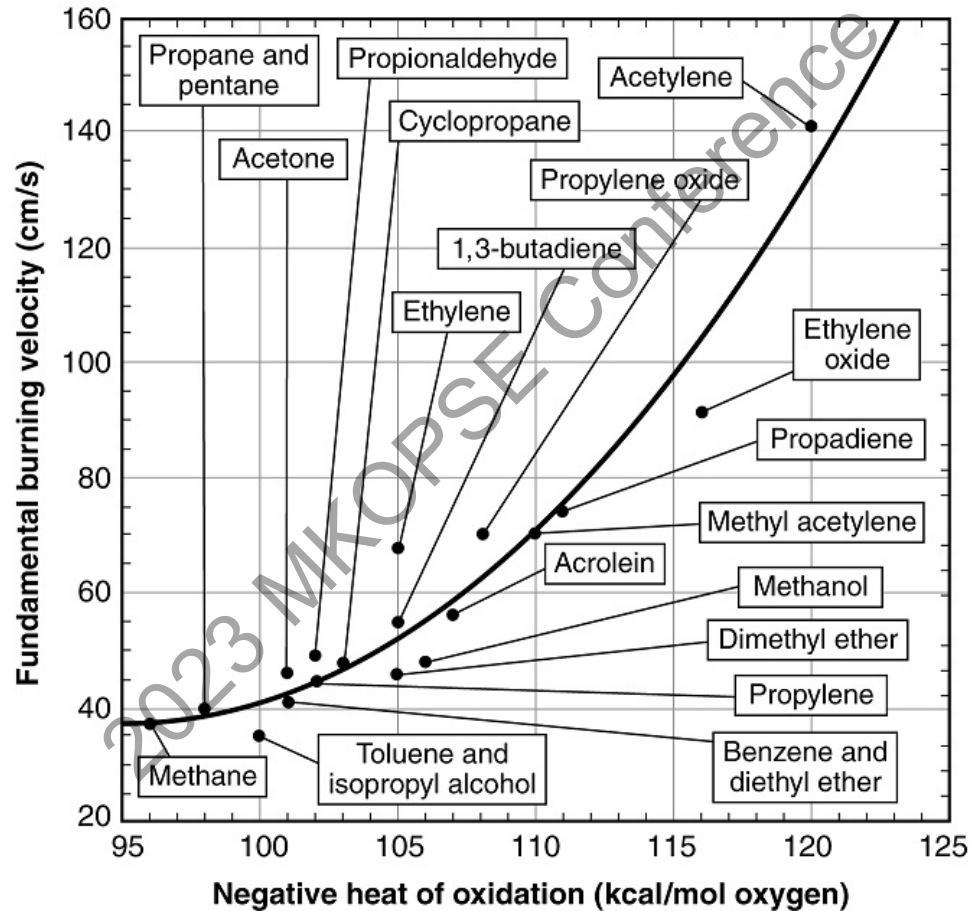


Detonation Example



Laminar Burning Velocities

Hydrogen
 $S_u = 286 \text{ cm/s}$



Minimum AutoIgnition Temperature (MAIT)

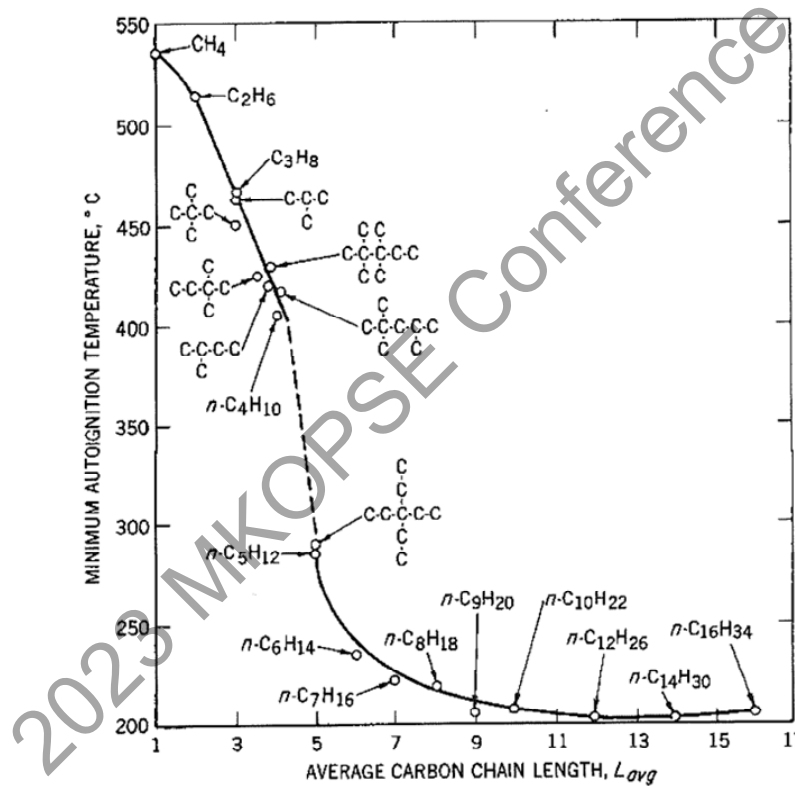
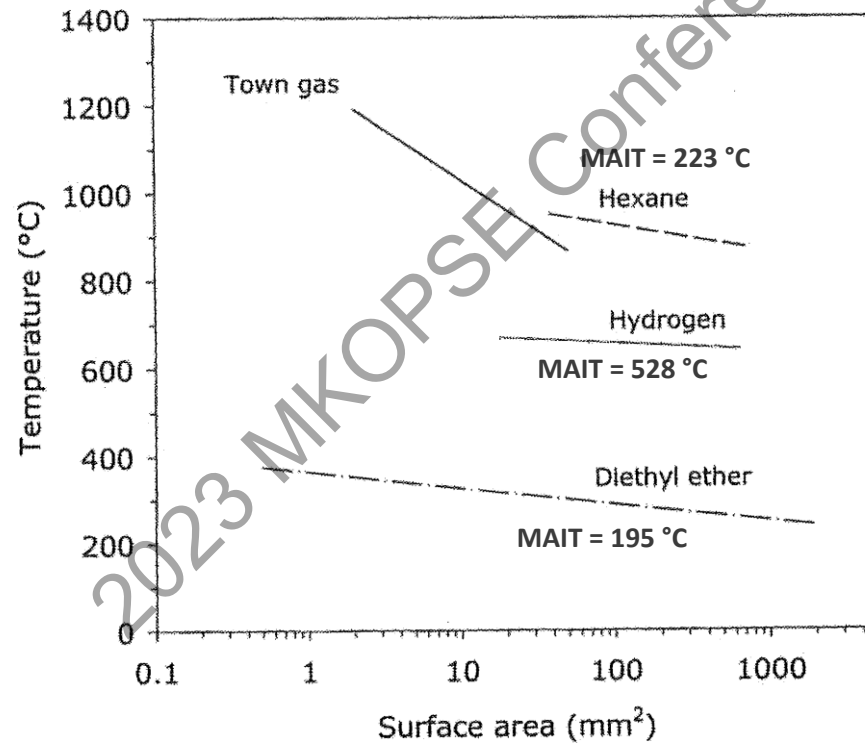


Figure 1.3. AIT as a function of chain length (Zabetakis, 1965).

Hot Surface Ignition Temperatures



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Thank You
Any Questions

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October 13, 2023

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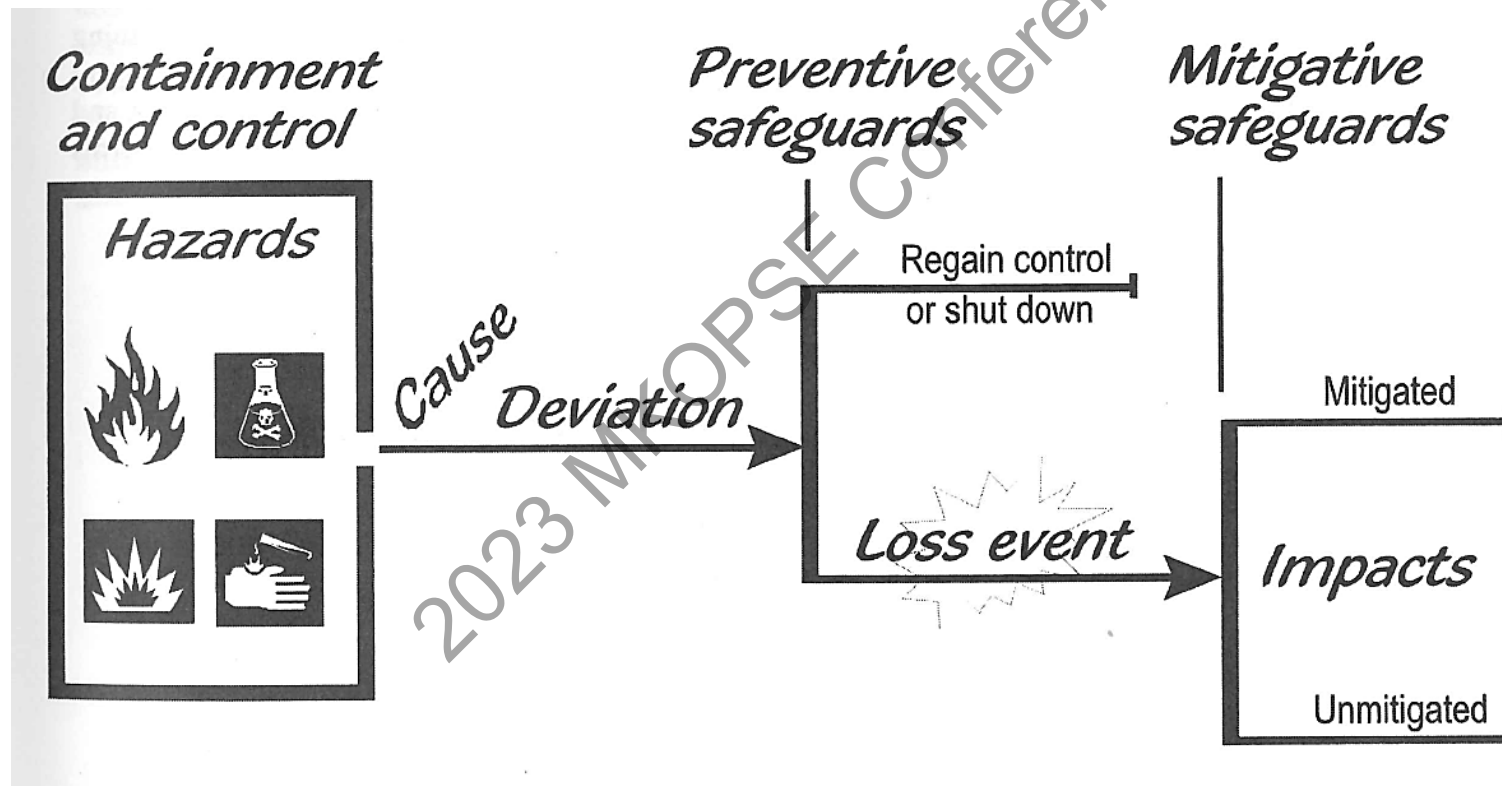
EXPLOSION RISK MITIGATION

Minimizing Risk

- Risk = Likelihood x Consequence

	Consequence				
Likelihood	Insignificant	Minor	Moderate	Major	Severe
Almost Certain	Low	Medium	High	Extreme	Extreme
Likely	Low	Medium	Medium	High	Extreme
Possible	Low	Low	Medium	High	High
Unlikely	Low	Low	Low	Medium	High
Rare	Low	Low	Low	Medium	Medium

Safeguards



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EXPLOSION PREVENTION / PROTECTION

NFPA Standards - Explosion Protection of Equipment

- Ignition Control
- Oxidant Concentration Reduction
- Fuel Concentration Reduction
- Chemical Suppression
- Isolation
 - Active
 - Passive
- Pressure Containment
- Explosion Venting

NFPA 69

Standard on Explosion Prevention Systems

NFPA 68

Standard on Explosion Protection by Deflagration Venting

Deflagration vs. Detonation

- Definitions (NFPA):
 - Deflagration: “Propagation of a combustion zone at a velocity that is less than the speed of sound in the unreacted medium”
 - Detonation: “Propagation of a combustion zone at a velocity greater than the speed of sound in the unreacted medium.”
- Explosion protection standards (NFPA 68 / 69) are not applicable to mitigation of detonations.
- NFPA 68 and NFPA 69 can still be used to prevent the occurrence of a deflagration and/or detonation.

NFPA 68

1.3.1 This standard does not apply to detonations, bulk auto-ignition of gases, or unconfined deflagrations, such as open-air or vapor cloud explosions.

NFPA 69

1.3.2 This standard shall not apply to the following conditions:

- (1) Devices or systems designed to protect against detonations

NFPA 69 Explosion Prevention Methods

- Prevention of deflagration ignition via:
 - **Chapter 7** – Deflagration Prevention by Oxidant Concentration Reduction
 - **Chapter 8** -- Deflagration Prevention by Combustible Concentration Reduction
 - **Chapter 9** – Predeflagration Detection and Control of Ignition Sources
- Prevention of deflagration propagation via:
 - **Chapter 11** – Deflagration Control by Active Isolation
 - **Chapter 12** – Deflagration Control by Passive Isolation
- Prevention of vessel rupture via:
 - **Chapter 10** – Deflagration Control by Suppression
 - **Chapter 13** – Deflagration Control by Pressure Containment
 - **Chapter 14** – Passive Explosion Suppression Using Expanded Mesh or Polymer Foam

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PRESSURE CONTAINMENT

Strengthening System

- Chapter 13 of NFPA 69 provides requirements for strengthening the system (pressure containment).
- NFPA 69 is not applicable if deflagration transitions to a detonation.
- Enclosure would need to be designed and constructed in accordance with the *ASME Boiler and Pressure Vessel Code*, or similar codes.
- The vent system would also be subjected to overpressure and would need to be considered.

NFPA 69: Standard on Explosion Prevention Systems, 2019 Edition - Chapter 13 Deflagration Control by Pressure Containment

13.1 Application.

13.1.1

The technique for deflagration pressure containment shall be permitted to be considered for specifying the design pressure of a vessel and its appurtenances so they are capable of withstanding the maximum pressures resulting from an internal deflagration.

13.2 Design Limitations.

13.2.1 *

Deflagration pressure containment techniques shall not be applied to systems for the purpose of containing a detonation.

13.3 Design Bases.

13.3.1

Enclosures protected by design for deflagration pressure containment shall be designed and constructed according to the *ASME Boiler and Pressure Vessel Code*, or similar codes, where the maximum allowable working pressure, herein designated as P_{MAWP} , shall be determined by calculation.

13.3.8

Auxiliary equipment such as vent systems, manways, fittings, and other openings into the enclosure, which could also experience deflagration pressures, shall be designed to ensure integrity of the total system and shall be inspected periodically.

Detonation Containment

- NFPA 68 / 69 standards do not apply.
- NFPA 67 applies, but is only a guideline at this time.
- Pipe must be strong enough and properly supported to withstand a detonation.
- All components must be able to withstand peak detonation overpressure.
- Additional engineering analysis is required to properly design such a system.

NFPA 67

Guide on Explosion Protection for Gaseous Mixtures in Pipe Systems

Chapter 7 Detonation Containment

7.1* General. The philosophy of the detonation containment method is to design a sufficiently strong vessel that is able to withstand maximum explosion pressure. Donat (1978) introduced two distinctions in designing pressure-resistant equipment: explosion pressure-resistant equipment and pressure shock-resistant equipment. Explosion pressure-resistant equipment applies to a pressure vessel, which must be capable of withstanding at least the maximum explosion pressure for a long time period. All elements of the process units are designed as a pressure vessel, that is, for a maximum permissible working pressure equal to the maximum explosion pressure. However, this approach is conservative and results in an expensive design.

Detonations in Pipes

- Normal deflagration pressures are in the < 10 barg range
- Detonations in straight open pipe can result in peak overpressures 15-20 barg
 - Higher overpressures possible at elbows and fittings (due to pressure wave reflections) and during a Deflagration-to-Detonation transition (DDT).



NFPA 68

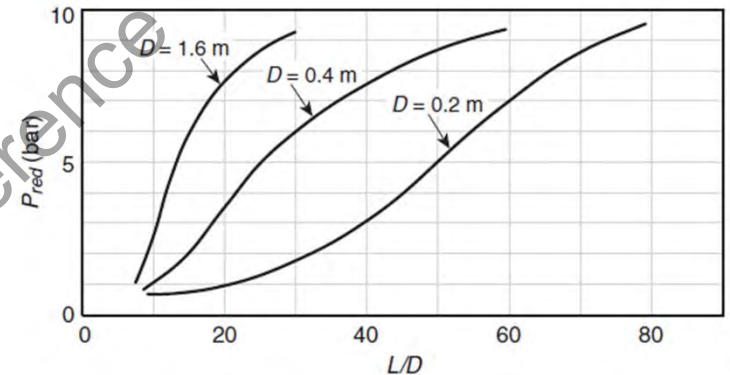


FIGURE 9.2.10.2.1.1 Maximum Pressure Developed During Deflagration of Propane/Air Mixtures Flowing at 2 m/s or Less in a Smooth, Straight Pipe Closed at One End.

NFPA 67

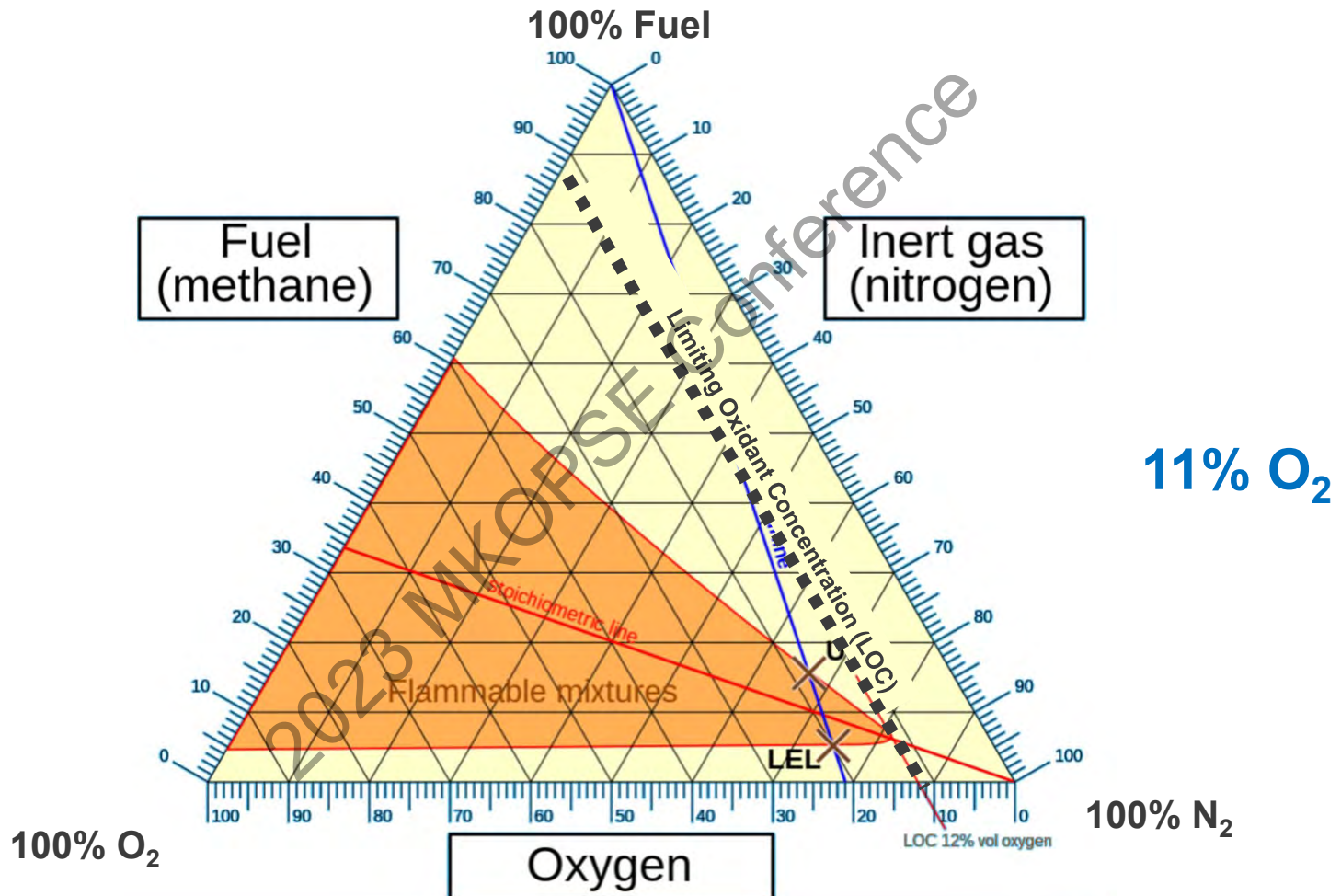
Table 7.3.1 Chapman and Jouguet Pressure and Velocity Values

Property	Hydrogen	Ethylene	Propane	Methane
CJ pressure (bar)	15.8	18.6	18.6	17.4
CJ velocity (m/s)	1968	1822	1804	1802

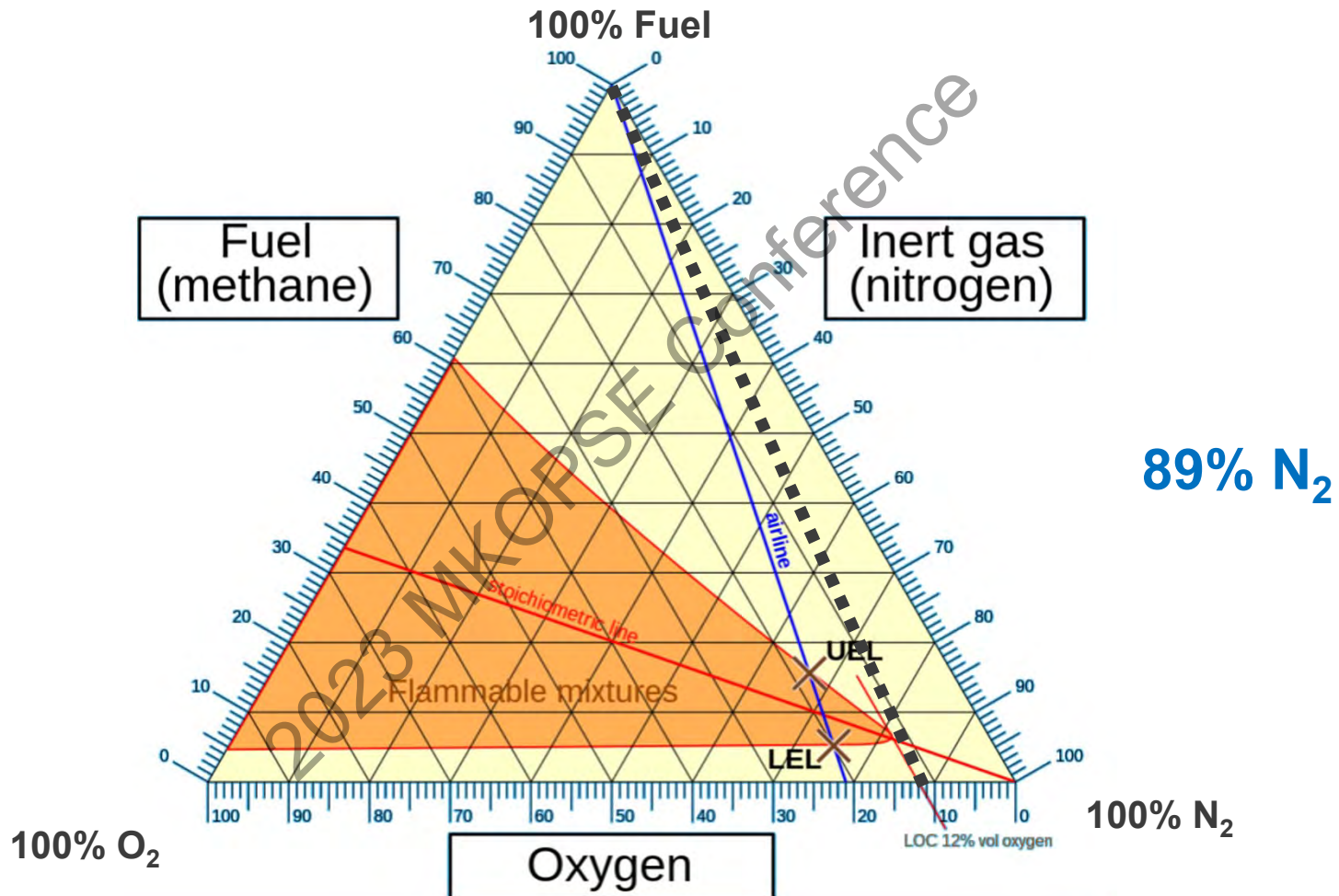
INERTING

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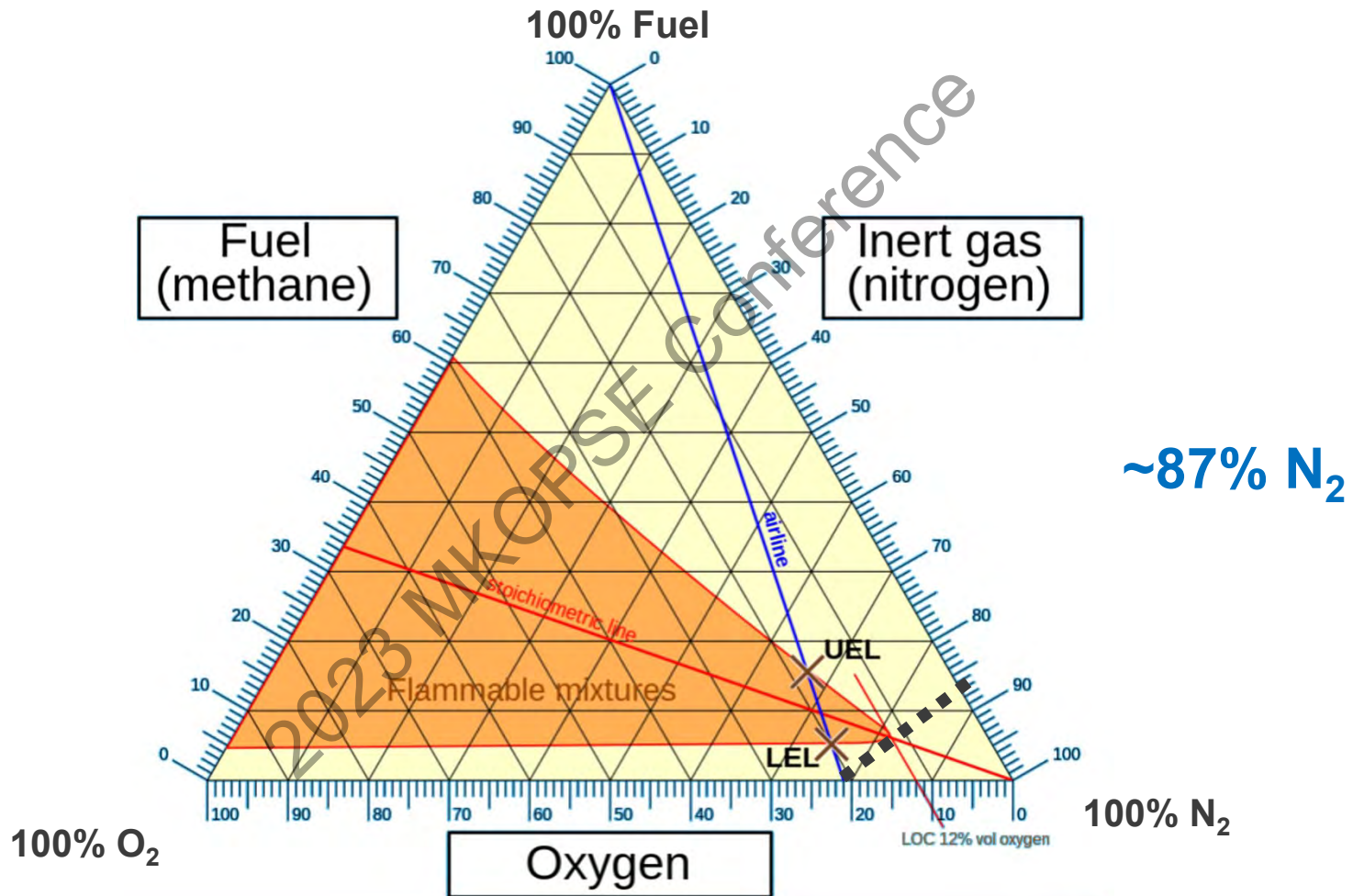
Inerting - Limiting Oxygen Concentration (LOC)



Inerting – N₂ Added to the Air



Inerting – N₂ Added to the Fuel



Inerting Requirements – NFPA 69

7.7.2.5* One of the following requirements shall be met where the oxygen concentration is continuously monitored and controlled with safety interlocks:

- (1) Where the LOC is greater than or equal to 5 percent, a safety margin of at least 2 volume percent below the worst credible case LOC shall be maintained.
- (2) Where the LOC is less than 5 percent, the equipment shall be operated at no more than 60 percent of the LOC.

7.7.2.8* Where the oxygen concentration is not continuously monitored and controlled with safety interlocks, one of the following requirements shall be met:

- (1) Where the LOC is greater than or equal to 7.5 percent, a safety margin of at least 4.5 volume percent below the worst credible case LOC shall be maintained.
- (2) Where the LOC is less than 7.5 percent, the oxygen concentration shall be designed to operate at no more than 40 percent of the LOC.

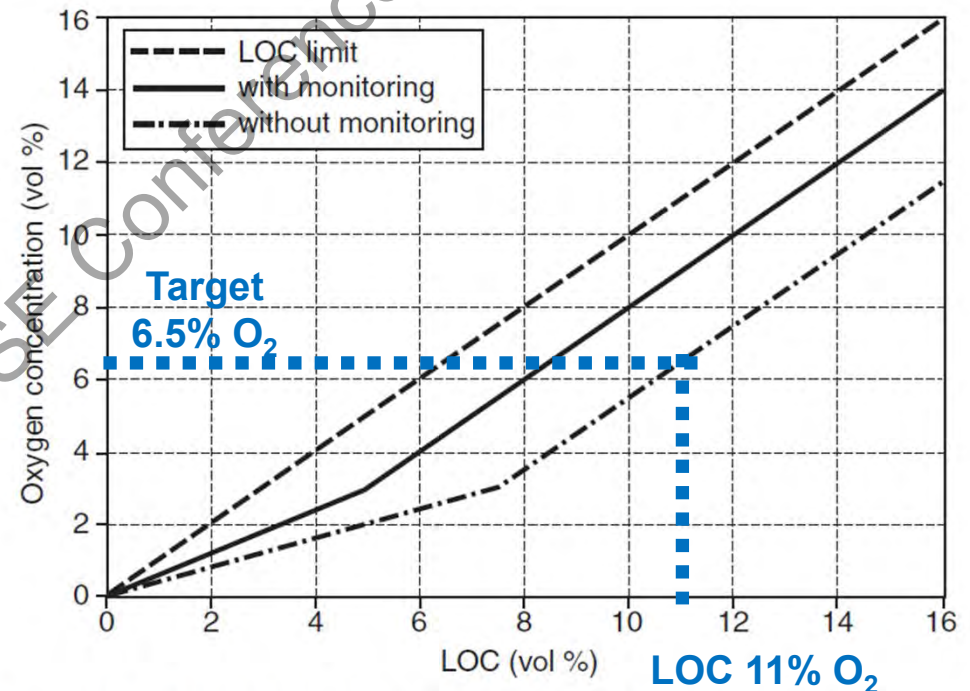


FIGURE A.7.7.2.8 Oxidant Control Limits as a Function of LOC.

Inerting Using Different Gases

Diluent	CO ₂	N ₂	Ar	He
Cp (J/K-mol) ⁽¹⁾	<u>37.3</u>	<u>29.2</u>	<u>20.8</u>	<u>20.8</u>
Methane LOC ⁽²⁾	14.6%	12.1%	9.8%	N/A
Methane LOC ⁽³⁾	13.1%	11.1%	N/A	N/A
CO LOC ⁽³⁾	5.1%	5.1%	N/A	N/A
H ₂ LOC ⁽³⁾	4.6%	4.6%	N/A	N/A

(1) NIST Webbook (<https://webbook.nist.gov/>) – Fluid properties at 1 atm and 20°C

(2) Irvin Glassman "Combustion" 3rd Ed, Academic Press (1996), Pg. 165

(3) NFPA 69 (2019), Appendix C

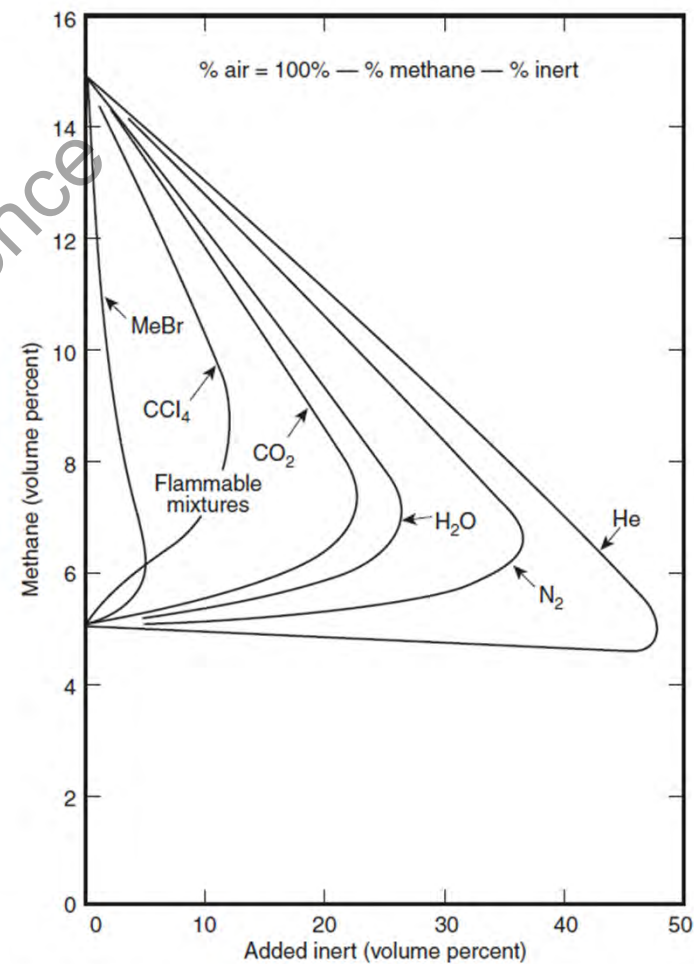


FIGURE B.3 Limits of Flammability of Methane-Inert Gas-Air Mixtures at 25°C (77°F) and Atmospheric Pressure.

DILUTION

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Air Dilution

- Chapter 8 of NFPA 69 provides requirements for use of air dilution (combustible concentration reduction).
- NFPA 69 requires that fuel concentration be maintained:
 - < 25% LFL, or
 - < 60% LFL when concentration is continuously monitored and controlled.

NFPA 69: Standard on Explosion Prevention Systems, 2019 Edition - Chapter 8 Deflagration Prevention by Combustible Concentration Reduction

8.1 * Application.

The technique for combustible concentration reduction shall be permitted to be considered where a mixture of a combustible material and an oxidant is confined to an enclosure and where the concentration of the combustible can be maintained below the lower flammable limit (LFL).

8.3.1 * Combustible Concentration Limit.

The combustible concentration shall be maintained at or below 25 percent of the LFL for all foreseeable variations in operating conditions and material loadings, unless the following conditions apply:

- (1) Where continuously monitored and controlled with safety interlocks, the combustible concentration shall be permitted to be maintained at or below 60 percent of the LFL.

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EXPLOSION SUPPRESSION

Explosion Protection

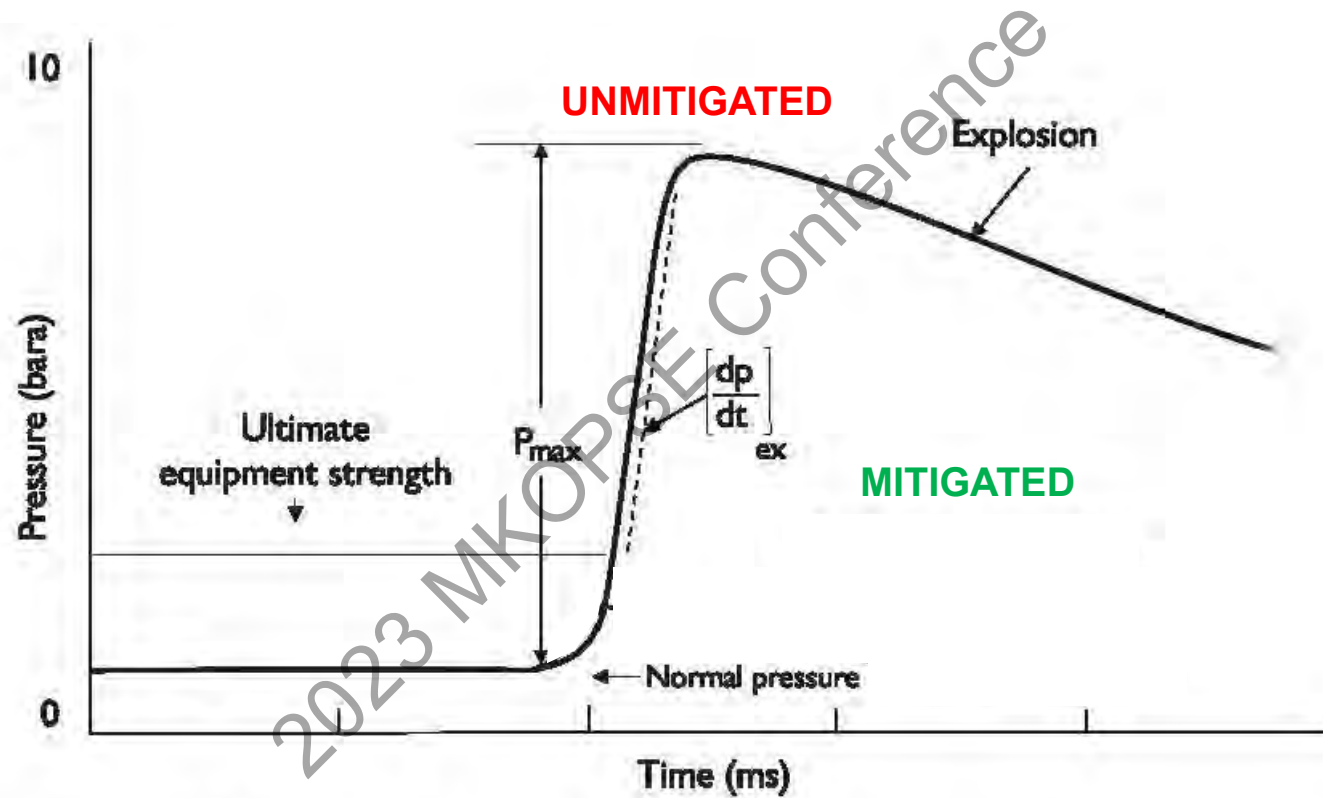


Figure 1: Pressure time histories of protected and unprotected explosions.

Deflagration Suppression for Combustible Dust

- Detection of explosion
 - Pressure rise
 - Spark/flame detection
- Suppression
 - Fast injection of chemical suppressants
- Can typically minimize explosion overpressure to a few psi
- Often used when explosion venting is not feasible
- Typically more expensive than venting

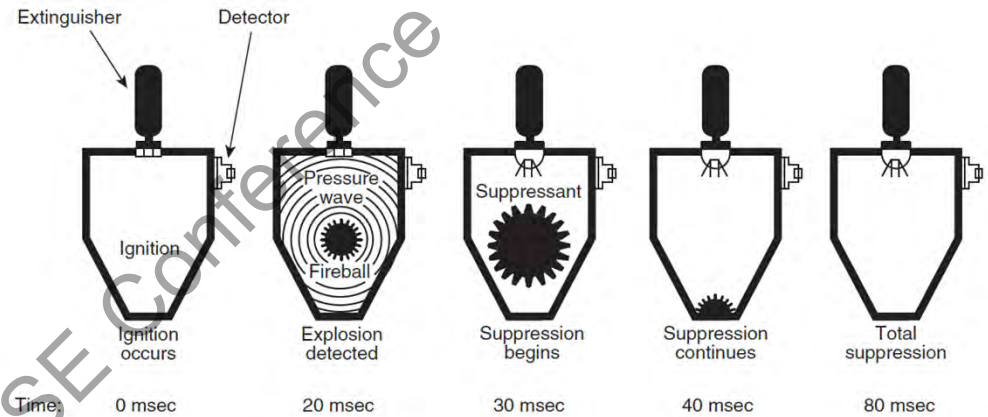
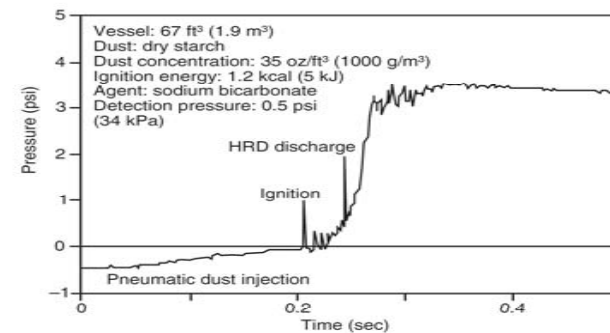


FIGURE B.5.1(a) Deflagration Suppression Sequence of Starch in a 35 ft³ (1 m³) Vessel.



Note: Pressures are gauge pressures.

FIGURE B.5.1(b) Pressure Versus Time in a Suppressed Deflagration.

Deflagration Suppression – Slow Motion

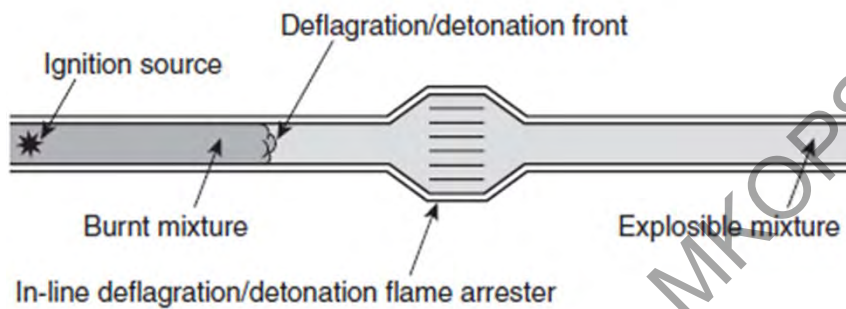


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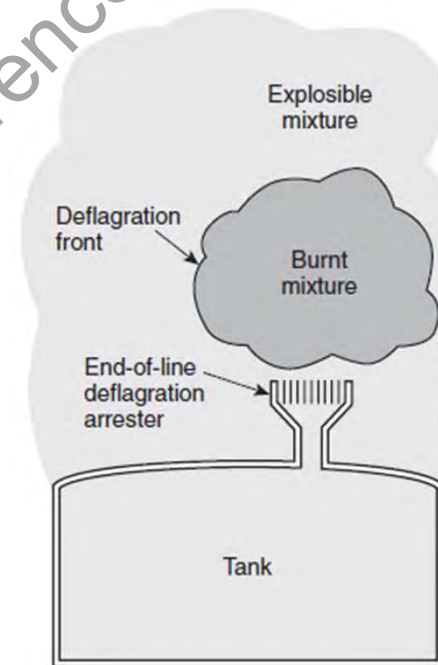
EXPLOSION ISOLATION

Types of flame arresters

- NFPA 69



In-line Flame arrester



End-of-line Flame arrester

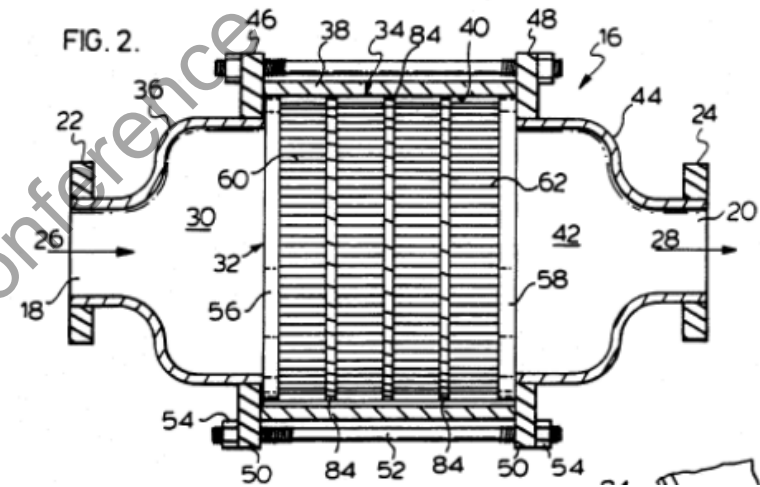
How do flame arresters work?

- **Quenching**

- Flame arresters function by removing heat from a passing flame such that the temperature of the burning gases drops below the temperature required to sustain combustion, quenching the flame.

- Whether a flame can be quenched is dependent on:

- The fuel / flame properties
- The specific geometry of the flame path.
- The physical properties of the arrester.
- The flame speed approaching the flame arrester.

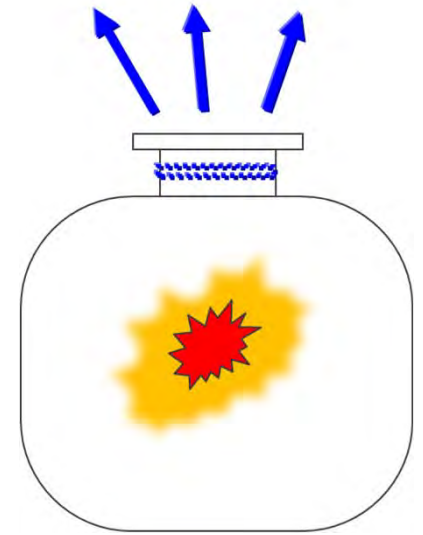


US Patent: US5415233A

Active Explosion Isolation



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EXPLOSION MITIGATION VIA DEFLAGRATION VENTING

Deflagration (Explosion) Venting – NFPA 68

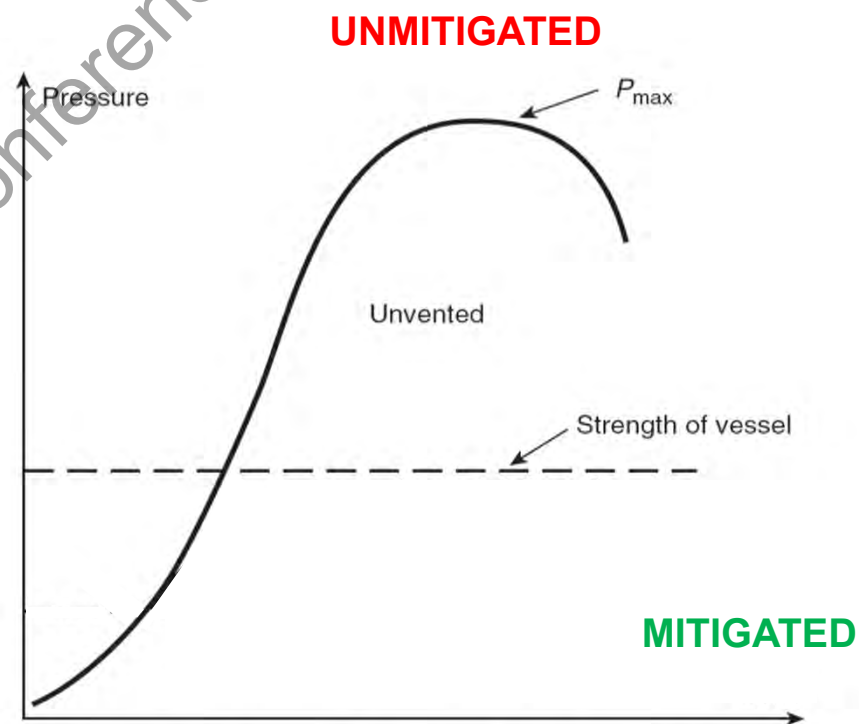
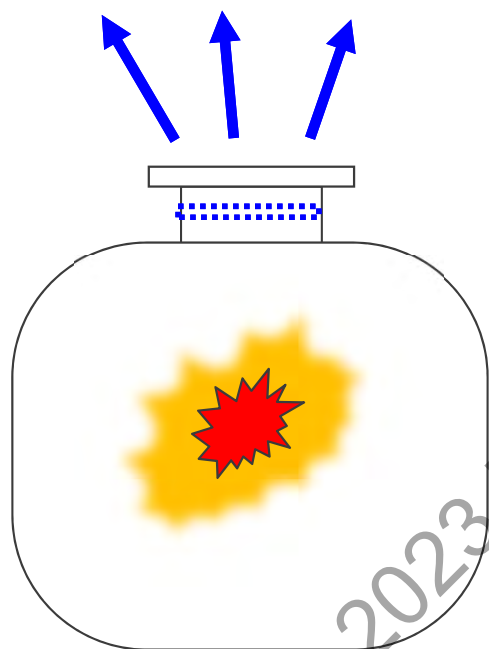


FIGURE B.4.1 Pressure–Time Graph of a Vented Deflagration.

Deflagration (Explosion) Venting – NFPA 68

- NFPA 68 provides equations for determining required explosion vent areas
- Vent reduces maximum overpressure
- Typically lower cost than explosion suppression systems
- Must vent to safe outdoor area
- Flame Arresting and Particulate Retention (Flameless) vents can be used indoors

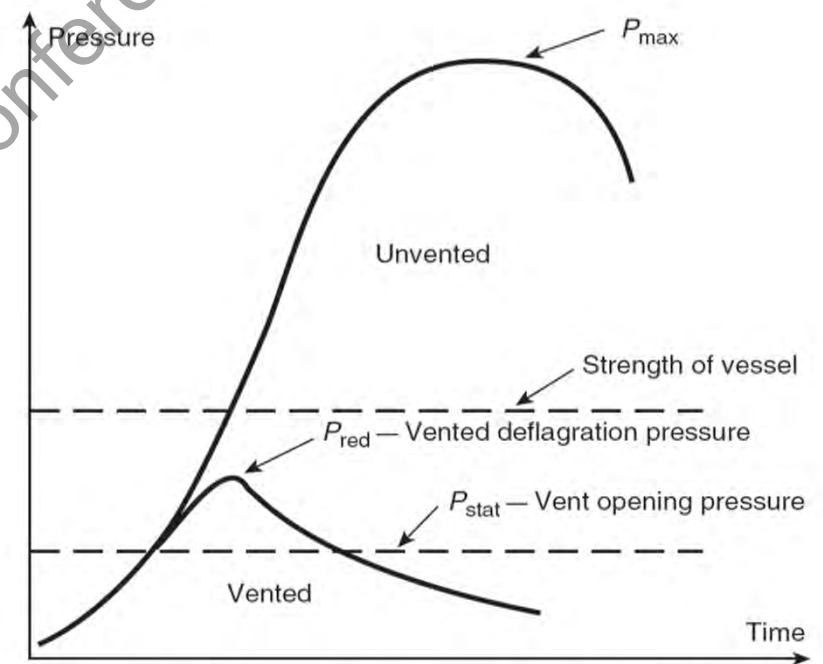


FIGURE B.4.1 Pressure–Time Graph of a Vented Deflagration.



Take a
Break

Hierarchy of Hazard Control

Elimination

Substitution

Engineering Controls

Administrative Controls

Personal Protective Equipment (PPE)

Preventive Safeguards

- Explosion prevention
- Instrumented protective system designed to bring system to safe state
- Operator response

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Mitigative Safeguards

- Explosion protection via deflagration venting
- Secondary Containment
- Explosion blast barricades and blast-resistant construction
- Fire/release detection and warning systems
- Deluge, foam and vapor mitigation systems
- Fire resistant supports and structures
- PPE
- Emergency response and planning

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CONTROL OF IGNITION SOURCES

Ignition Source Control

NFPA 69: Standard on Explosion Prevention Systems,
2019 Edition - Chapter 9 Predeflagration Detection and
Control of Ignition Sources

9.1 * Application.

Systems used for the predeflagration detection and control of certain specific ignition sources shall be permitted to be used to reduce the probability of the occurrence of deflagrations in systems that handle combustible particulate solids.

9.1.1

Systems used for the predeflagration detection and control of ignition sources shall be permitted to be used in conjunction with other explosion prevention or explosion protection measures, such as deflagration suppression or deflagration venting, for those systems posing a dust explosion hazard.

Metrics for Flames

- Laminar Burning Velocity
 - The laminar burning velocity is the speed of the flame front relative to the position of the unburned gas
- Maximum Experimental Safe Gap (MESG)
 - The MESG is the maximum gap between two parallel flat surfaces that prevents flame propagation across that gap under certain experimental conditions
 - The MESG is relied upon in the National Electric Code (NEC) to, in part, define flammable gases and vapors into four groups (A, B, C, D)
- Critical/Quenching Diameter
 - The quenching diameter is the maximum diameter of a round hole that would quench a slow moving flame



Detonation Pressures

- Reflected shocks at closed ends can result in peak pressures up to $2.5P_{CJ}$. (Chapman and Jouguet detonation pressure)
 - Elbows can also result in reflected pressure waves.
- A DDT can produce peak pressures up to $4.5P_{CJ}$.

facilities. When the detonation reaches a closed end, it will reflect as a shock wave that propagates away from the closed end. The peak pressure of the reflected shock wave [62] is about $2.5P_{CJ}$ and the pressure decays as the wave moves away from the reflecting surface. The reflected shock wave will induce flex-

It has been known for some time [73, 74] that DDT can produce pressures in excess of the CJ or reflected CJ pressure. White [73] reports observations of reflected pressures in stoichiometric H_2 -air initially at 300 K and 1 atm. During flame acceleration in a 3.5×3.5 in. (89 × 89 mm) tube 32 ft (9.75 m) long, a peak pressure of 170 atm was recorded. This is 4.5 times the usual reflected CJ pressure and is probably due to the overdriven detonation produced during the transition process. As discussed previously, reflected

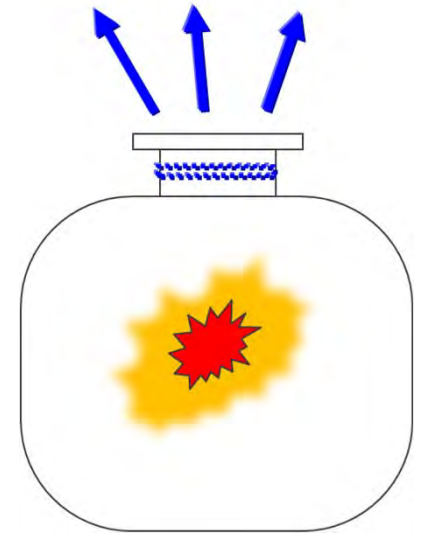


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EXPLOSION MITIGATION VIA DEFLAGRATION VENTING

Deflagration (Explosion) Venting – NFPA 68

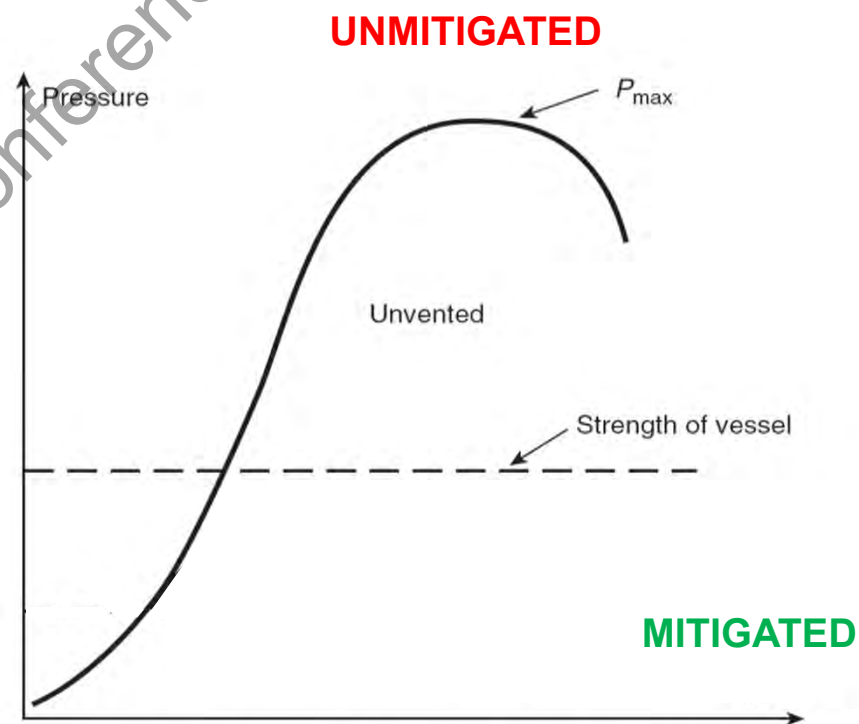
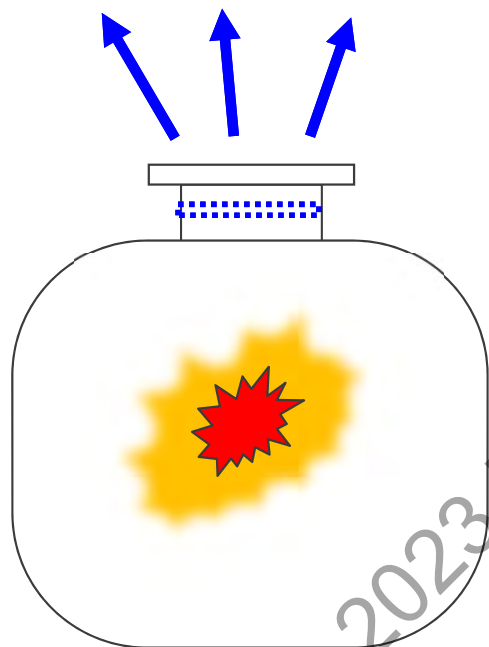


FIGURE B.4.1 Pressure–Time Graph of a Vented Deflagration.

Deflagration (Explosion) Venting – NFPA 68

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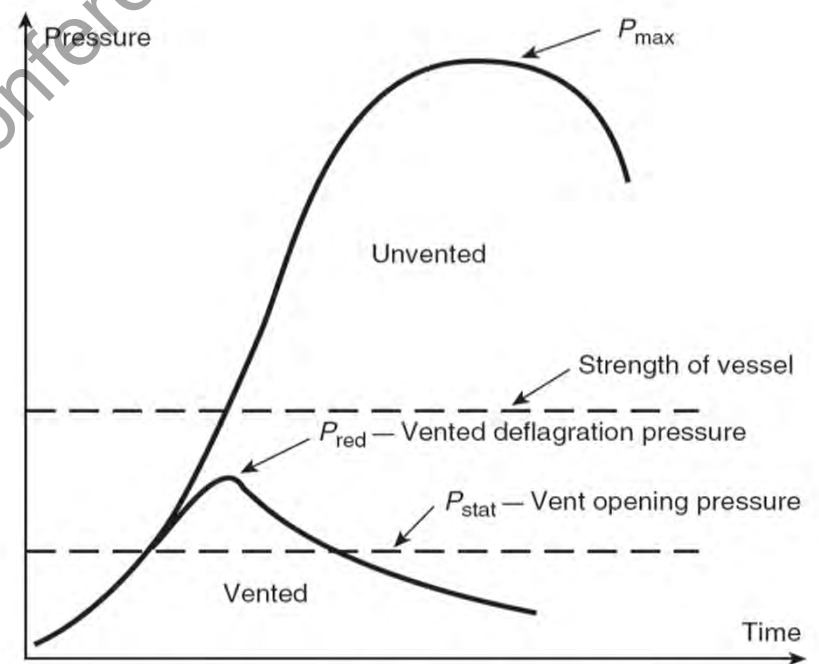


FIGURE B.4.1 Pressure–Time Graph of a Vented Deflagration.

Vented Deflagrations – NFPA 68 - Gas Mixtures

NFPA 68: Standard on Explosion Protection by Deflagration Venting, 2023 Edition - Chapter 7 Venting Deflagrations of Gas Mixtures and Mists



▼ Chapter 6 Fundamentals of Venting of Deflagrations

- 6.1 Basic Concepts.
- 6.2 Mixtures.
- 6.3 Enclosure Design and Support.
- 6.4 Enclosure Length-to-Diameter Ratio and Vent Variables.
- 6.5 Vent Closure Operation.
- 6.6 Consequences of a Deflagration.
- 6.7 Effects of Vent Inertia.
- 6.8 Fireball Dimensions.
- 6.9 Effects of Vent Discharge Ducts.
- 6.10 Venting with Flame Arresting and Particulate Retention.

▼ Chapter 7 Venting Deflagrations of Gas Mixtures and Mists

- 7.1 Introduction.
- 7.2 Venting by Means of Low Inertia Vent Closures.
- 7.3 Partial Volume Effects.
- 7.4 Effects of Panel Inertia.
- 7.5 Effects of Vent Ducts.
- 7.6 Deflagration Venting of Enclosures Interconnected with Pipelines.

NFPA 68 – 7.2 Low Inertia Vent Closures

7.2.1 Low Inertia Vent Closure Equations for Low P_{red} .

When $P_{red} \leq 0.5$ bar-g, the minimum required vent area, A_{v0} , shall be determined by Equation 7.2.1a and Equation 7.2.1b:

$$A_{v0} = \frac{A_s C}{\sqrt{P_{red}}} \quad [7.2.1a]$$

$$P_{red} < 0.5 \text{ barg}$$

$$C = \frac{S_u \rho_u \lambda}{2G_u C_d} \left[\left(\frac{P_{max} + 1}{P_0 + 1} \right)^{1/\gamma_0} - 1 \right] (P_0 + 1)^{1/2} \quad [7.2.1b]$$

7.2.2 Low Inertia Vent Closure Equations for High P_{red} .

When $P_{red} > 0.5$ bar-g, the minimum required vent area, A_{v0} , shall be determined from Equation 7.2.2a and Equation 7.2.2b:

$$A_{v0} = A_s \frac{1 - \left(\frac{P_{red} + 1}{P_{max} + 1} \right)^{1/\gamma_b}}{\left(\frac{P_{red} + 1}{P_{max} + 1} \right)^{1/\gamma_b} - \delta} \frac{S_u \rho_u \lambda}{G_u C_d} \quad [7.2.2a]$$

$$P_{red} > 0.5 \text{ barg}$$

$$\delta = \frac{\left(\frac{P_{stat} + 1}{P_0 + 1} \right)^{1/\gamma_b} - 1}{\left(\frac{P_{max} + 1}{P_0 + 1} \right)^{1/\gamma_b} - 1} \quad [7.2.2b]$$

NFPA 68 – 7.2.6 Turbulent Flame Enhancement Factor, λ

$$\lambda_0 = \varphi_1 \varphi_2$$

φ_1

Enhancement due to flame-generated turbulence

φ_2

Enhancement due to vent-generated turbulence

$$\varphi_1 = \begin{cases} 1, & \text{if } Re_f < 4000 \\ \left(\frac{Re_f}{4000}\right)^\theta, & \text{if } Re_f \geq 4000 \end{cases}$$

$$Re_f = \frac{\rho_u S_u (D_{he} / 2)}{\mu_u}$$

$$\varphi_2 = \max \left\{ 1, \beta_1 \left(\frac{Re_v}{10^6} \right)^{\left(\frac{\beta_2}{S_u}\right)^{0.5}} \right\}$$

$$Re_v = \frac{\rho_u u_v (D_v / 2)}{\mu_u}$$

$$u_v = \min \left\{ \sqrt{\frac{2 \times 10^5 P_{red}}{\rho_u}}, a_v \right\}$$

NFPA 68 – 7.2.6.2 Obstacles

7.2.6.2

The total external surface area, A_{obs} , of the following equipment and internal structures that can be in the enclosure shall be estimated:

- (1) Piping, tubing, and conduit with diameters greater than $\frac{1}{2}$ in.
- (2) Structural columns, beams, and joists
- (3) Stairways and railings
- (4) Equipment with a characteristic dimension in the range of 2 in. to 20 in. (5.1 cm to 51 cm)

7.2.6.3

When $A_{obs} < 0.2A_S$, λ_1 shall be equal to λ_0 as determined in 7.2.6.1.

7.2.6.4

When $A_{obs} > 0.2A_S$, λ_1 shall be determined as follows:

$$\lambda_1 = \lambda_0 \exp\left(\sqrt{\frac{A_{obs}}{A_S} - 0.2}\right)$$

NFPA 68 – 7.2.6.5 Length to Diameter Ratio (L/D)

7.2.6.5

The L/D of the enclosure shall be determined according to Section 6.4.

7.2.6.6

For L/D values less than 2.5, λ shall be set equal to λ_1 .

7.2.6.7

For L/D values from 2.5 to 5 and for P_{red} no higher than 2 bar-g, λ shall be calculated as follows:

$$\lambda = \lambda_1 \left[1 + \left(\frac{L/D}{2.5} - 1 \right)^2 \right]$$

NFPA 68 – 7.3 Partial Volume Effects

7.3 Partial Volume Effects.

7.3.1

When a documented hazard analysis demonstrates that there is insufficient gas in the enclosure to form a stoichiometric gas-air mixture occupying the entire enclosure volume, the vent area, A_{v0} , calculated from Equation 7.2.1a or Equation 7.2.2a, as appropriate, shall be permitted to be reduced as described in 7.3.3.

7.3.2 *

A partial volume fill fraction, X_r , shall be calculated as shown in Equation 7.3.2:

$$X_r = \frac{V_{gas}}{(V_{enc} - V_{solid})} x_{st} \quad [7.3.2]$$

where:

V_{gas} = maximum volume of gas that can be mixed with air in the enclosure

V_{enc} = enclosure volume

V_{solid} = volume of solid objects

x_{st} = stoichiometric volume concentration of gas

7.3.3

If $X_r < 1$, the minimum required vent area, A_{v1} , shall be calculated from the following equation:

$$A_{v1} = A_{v0} X_r^{-1/3} \cdot \sqrt{\frac{X_r - \Pi}{1 - \Pi}} \quad [7.3.3]$$

where:

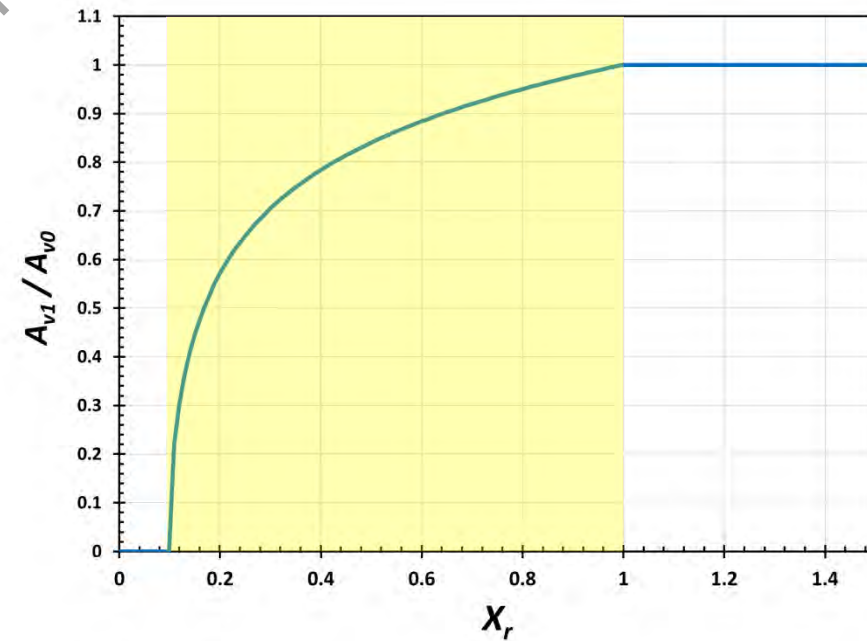
A_{v1} = vent area for partial volume deflagration

A_{v0} = vent area for full volume deflagration as determined from Equation 7.2.1a or 7.2.2a

X_r = fill fraction $> \Pi$

$\Pi = P_{red}/P_{max}$

$P_{red} = 0.5 \text{ barg}$
 $P_{max} = 5 \text{ barg}$
 $\Pi = 0.1$



NFPA 68 – 7.4 Effect of Panel Inertia

7.4 Effects of Panel Inertia.

7.4.1 *

When the mass of the vent panel $\leq 40 \text{ kg/m}^2$, Equation 7.4.2 shall be used to determine whether an incremental increase in vent area is needed, and Equation 7.4.3 shall be used to determine the value of that increase.

7.4.2

The vent area determined in Section 7.3 shall be adjusted for vent mass when the vent mass exceeds M_T as calculated in Equation 7.4.2:

$$M_T = \left[\frac{P_{red}^{0.2} \cdot n^{0.3} \cdot V}{(S_u \cdot \lambda)^{0.5}} \right]^{1.67} \quad [7.4.2]$$

where:

M_T = threshold mass (kg/m^2)

P_{red} = the maximum pressure developed in a vented enclosure during a vented deflagration (bar-g)

n = number of panels

V = enclosure volume ($>1 \text{ m}^3$)

7.4.3

For $M > M_T$, the required vent area, A_{v2} , shall be calculated as follows:

$$A_{v2} = A_{v1} \cdot F_{SH} \left[1 + \frac{(0.05) \cdot M^{0.6} \cdot (S_u \cdot \lambda)^{0.5}}{n^{0.3} \cdot V \cdot P_{red}^{0.2}} \right] \quad [7.4.3]$$

where:

A_{v2} = vent area for panel inertia (m^2)

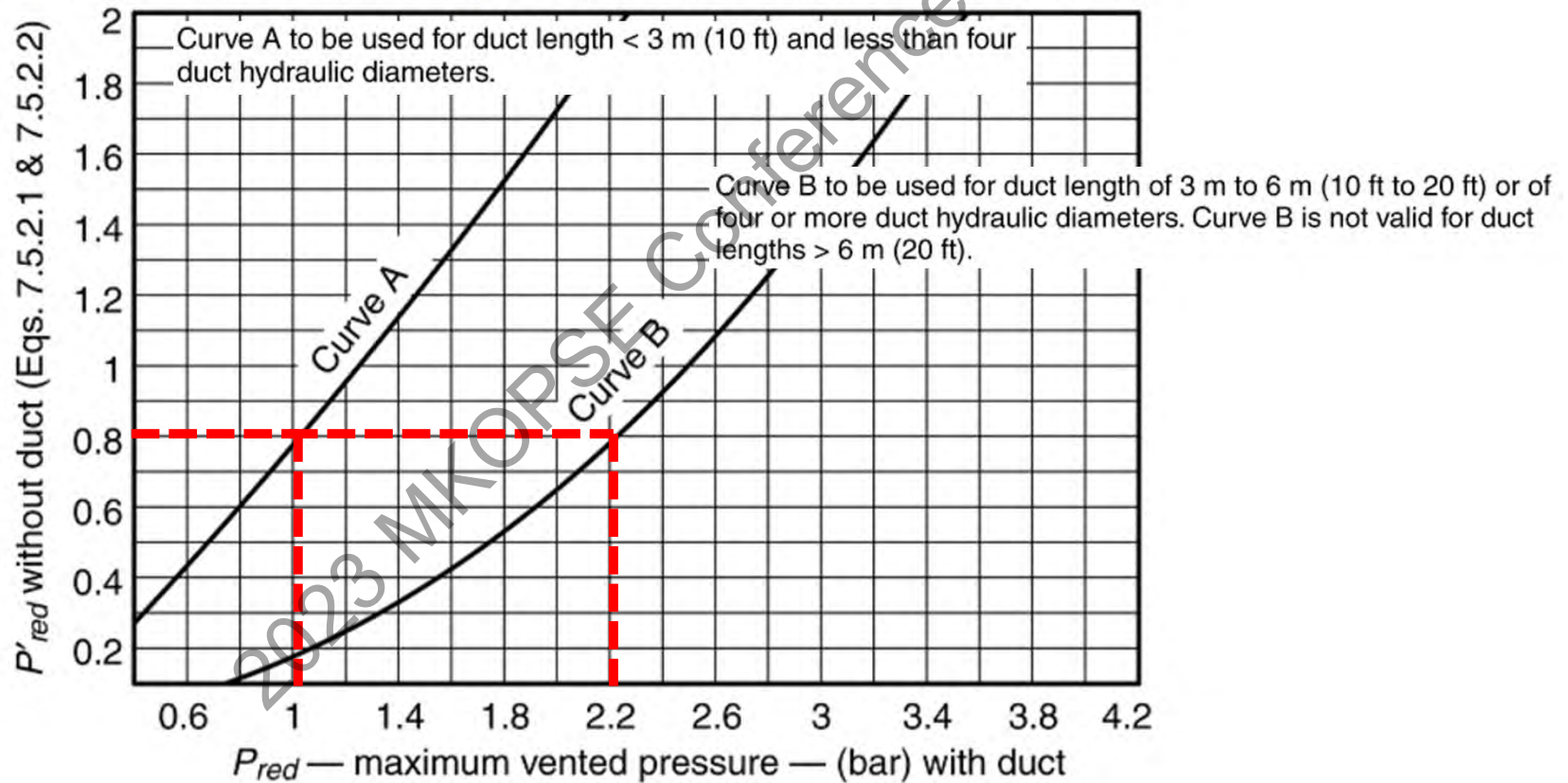
M = mass of vent panel (kg/m^2)

A_{v1} = vent area determined in Section 7.3 (m^2)

$F_{SH} = 1$ for translating panels or 1.1 for hinged panels

NFPA 68 – 7.5 Effect of Vent Ducts

Figure 7.5.2 Maximum Pressure Developed During Venting of Gas, with and Without Vent Ducts.



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FIREBALL SIZE

Flameless Explosion Vents



Dust Explosion Venting
without REMBE® Q-Rohr®



with REMBE® Q-Rohr®

Explosion Venting Examples



Explosion Venting Examples



Empirical Correlations for Fireball Size

- NFPA 68 *Standard on Explosion Protection by Deflagration Venting*
- British Standard BS EN 14994 *Gas Explosion Venting Protective System*

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Vented Deflagration Fireball Dimensions: NFPA 68 (2018)

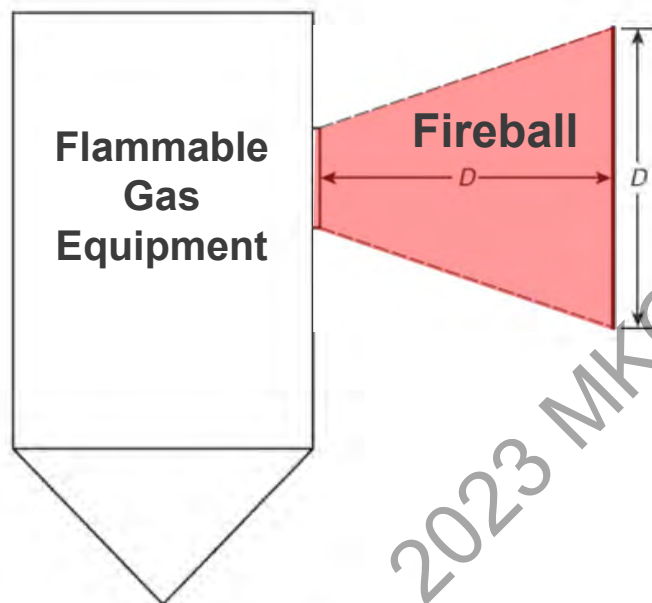


FIGURE 8.9.2.2 Fireball Dimensions.

**Maximum Flammable Gas
Fireball Travel Distance:**

$$D = 3.1 \cdot \left(\frac{V}{n} \right)^{0.402}$$

where:

D = axial distance (front-centerline) from vent (m)

V = volume of vented enclosure (m^3)

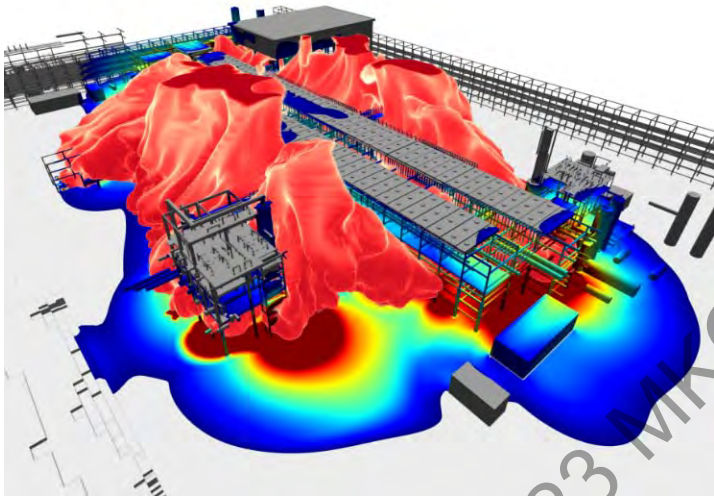
n = number of evenly distributed vents

EN 14494 uses $D=5 V^{1/3}$

Empirical Equation Limitations

- Based on a number of limited experiments
- Depend on only:
 - Enclosure volume
 - Number of vents
 - Metal dust (yes/no)
- Do not take into account:
 - Fuel reactivity (S_u)
 - Vent activation pressure (P_{stat})
 - Maximum vented explosion overpressure (P_{red})
 - Vent geometry
 - Fuel concentration

FLACS / DUSTEX CFD Models



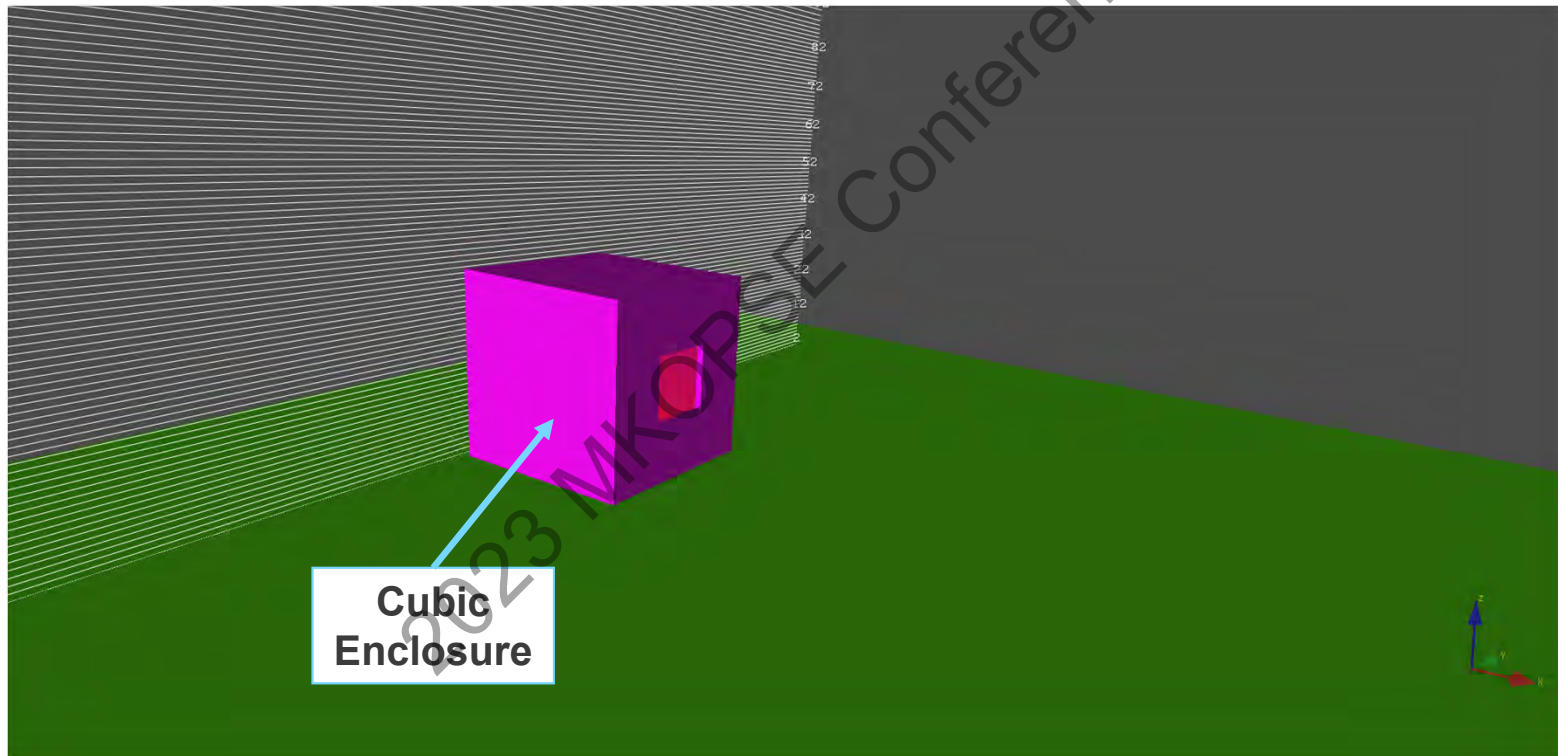
- FLACS is a Computational Fluid Dynamics (CFD) software developed by Gexcon to model vapor dispersion and gas explosion events
- DUSTEX is a FLACS module developed to model combustible dust deflagrations and explosions



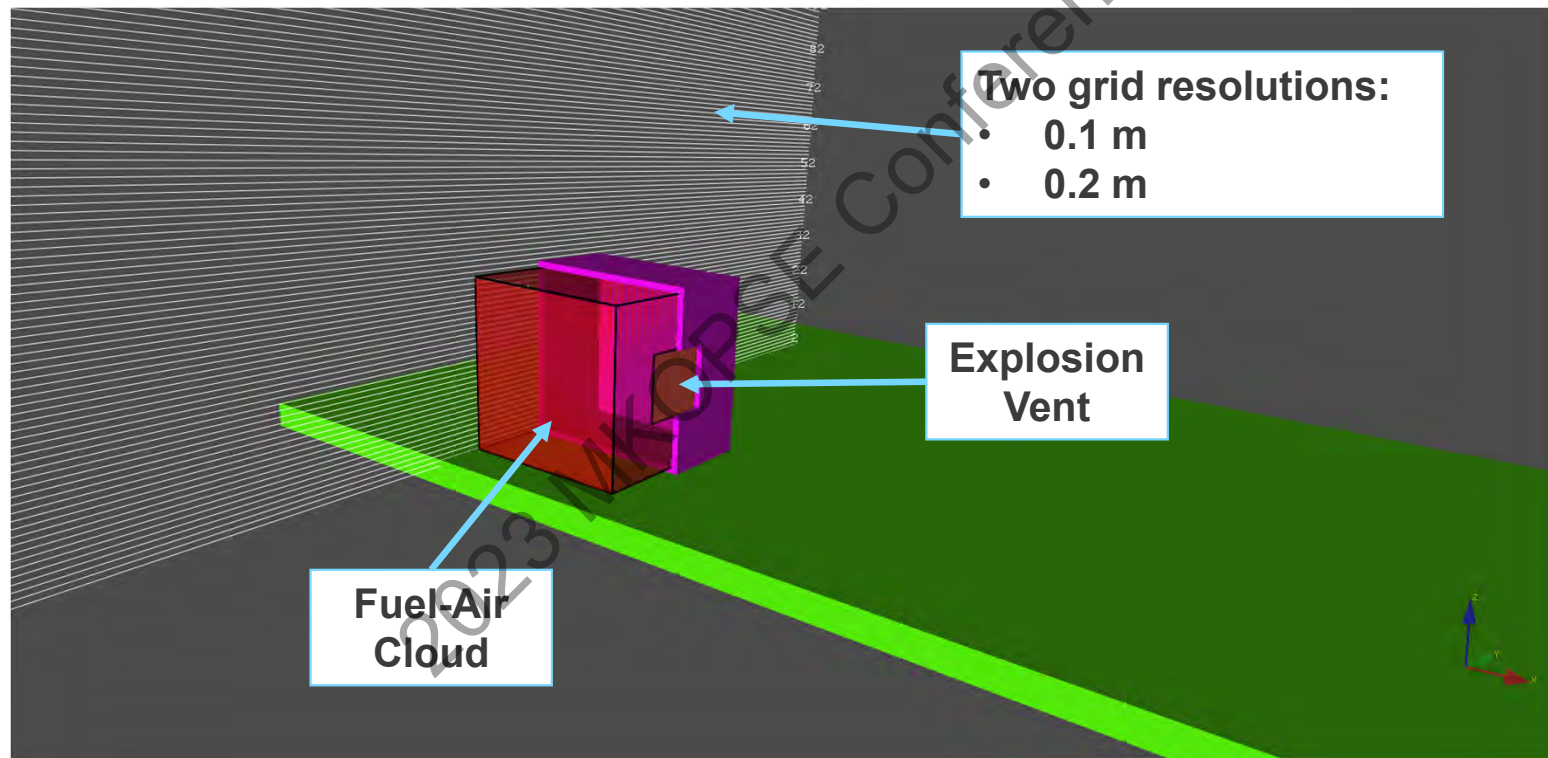
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GEXCON

CFD Modeling of Explosion Venting - Geometry



CFD Modeling of Explosion Venting - Geometry



Scenario Matrix

Fuel	Methane	Propane	Ethylene
Concentration	Phi = 1.0	Phi = 0.7 Phi = 1.0 Phi = 1.4	Phi = 1.0
Fuel ¹ S_u	38 cm/s	45 cm/s	74 cm/s
Enclosure Volume	4 – 1,000 m ³	4 – 1,000 m ³	4 – 1,000 m ³
Vent Size	0.2 – 16 m ²	0.2 – 16 m ²	0.2 – 16 m ²
Vent Activation Pressure	0.1 barg	0.1 – 0.2 barg	0.1 barg
# of scenarios	7	24	7

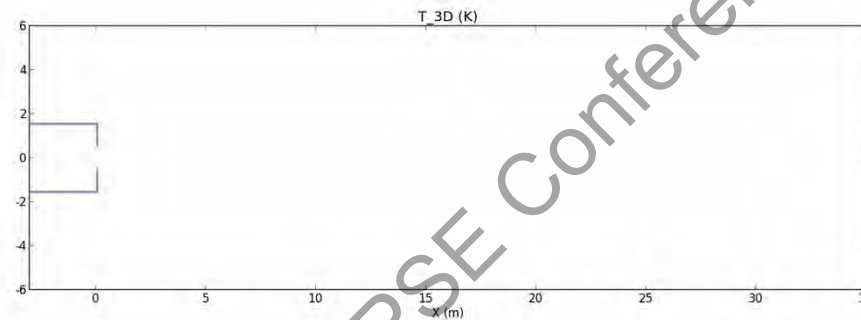
[¹] Default values in FLACS libraries

Propane Explosion Venting Example

Propane
Phi = 1
3m x 3m x 3m

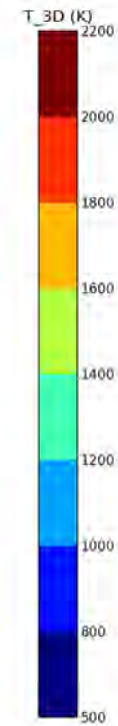
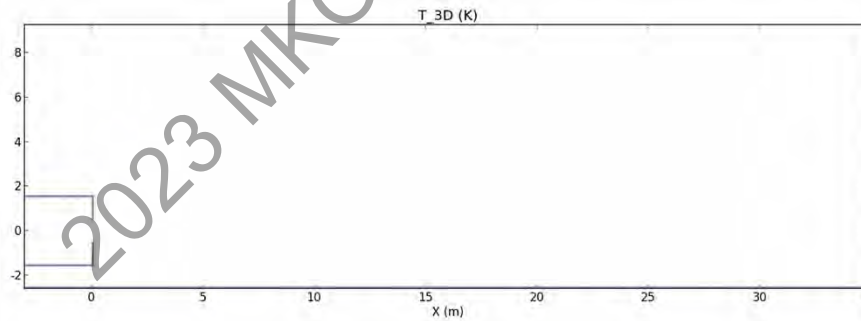
Top
View

Run: 680117
Var: T_3D
Time: 0.00 s (0)
Plane: XY, Z=0.05m



Side
View

Run: 680117
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.05m



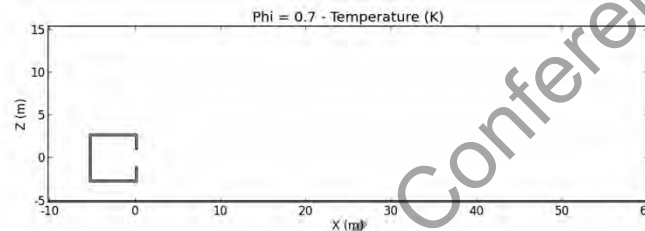
Temperature
Contours
500 K – 2200 K

Propane – Effect of Equivalence Ratio

Propane
5.2m x 5.2m x 5.2m

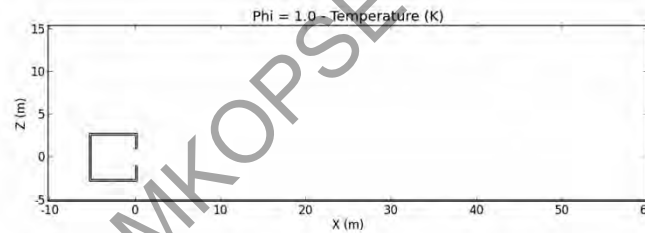
Phi = 0.7

Run: 680121
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



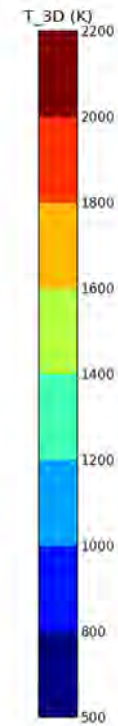
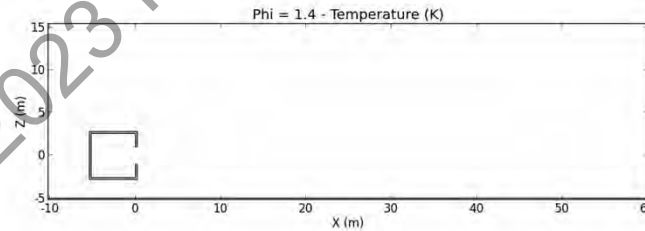
Phi = 1.0

Run: 680120
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



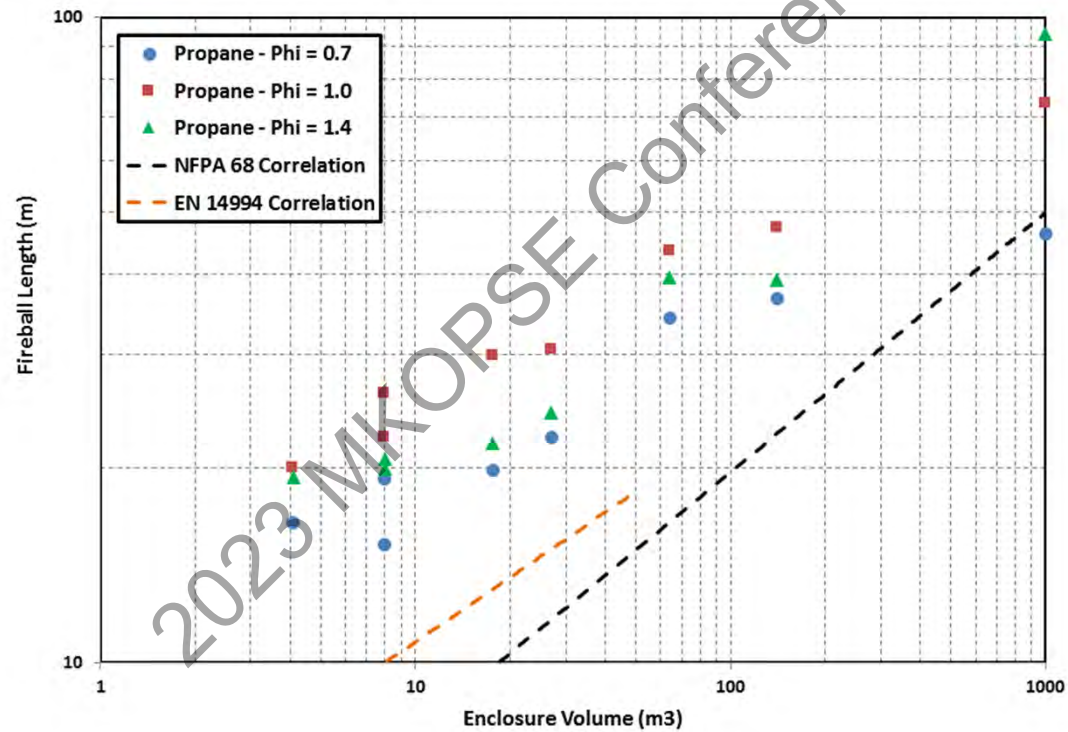
Phi = 1.4

Run: 680122
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



Temperature
Contours
500 K – 2200 K

Gas Explosion Venting Fireball – CFD Results

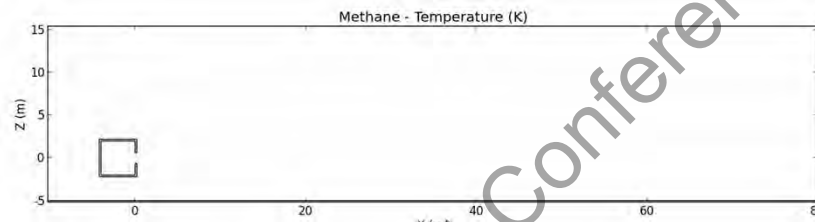


Effect of Fuel Type – Small Volume

Phi = 1.0
4m x 4m x 4m

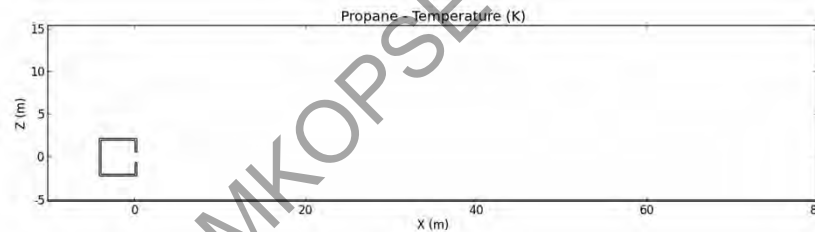
Methane

Run: 680144
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



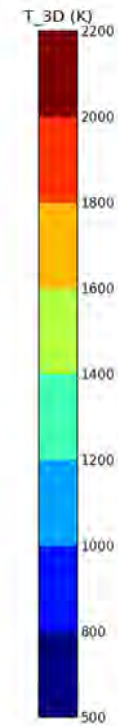
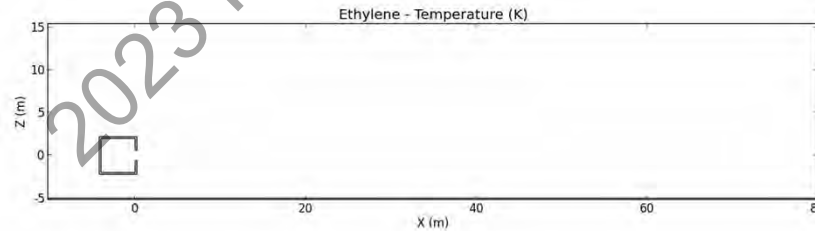
Propane

Run: 680141
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



Ethylene

Run: 680145
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



Temperature
Contours
500 K – 2200 K

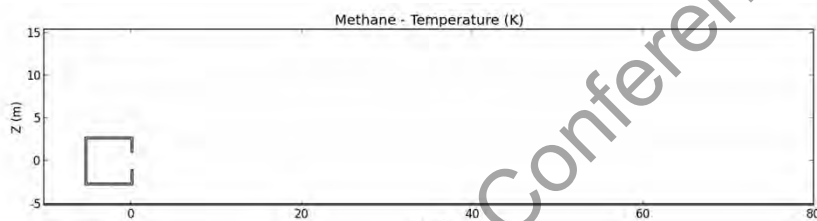
Effect of Fuel Type – Large Volume

$\Phi = 1.0$

5.2m x 5.2m x 5.2m

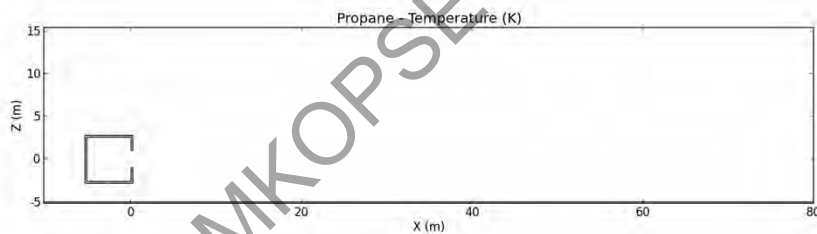
Methane

Run: 680129
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



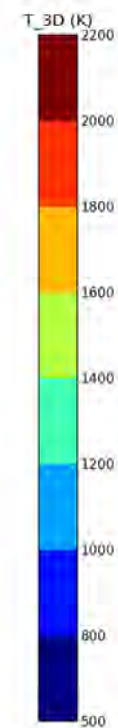
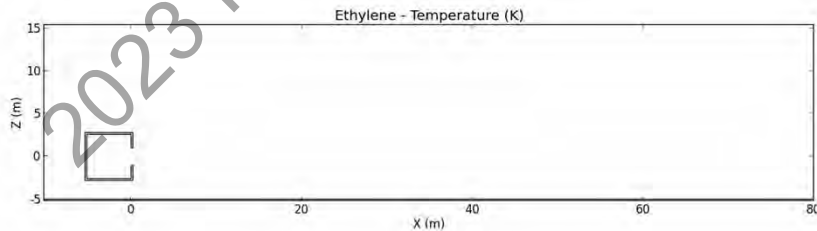
Propane

Run: 680120
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



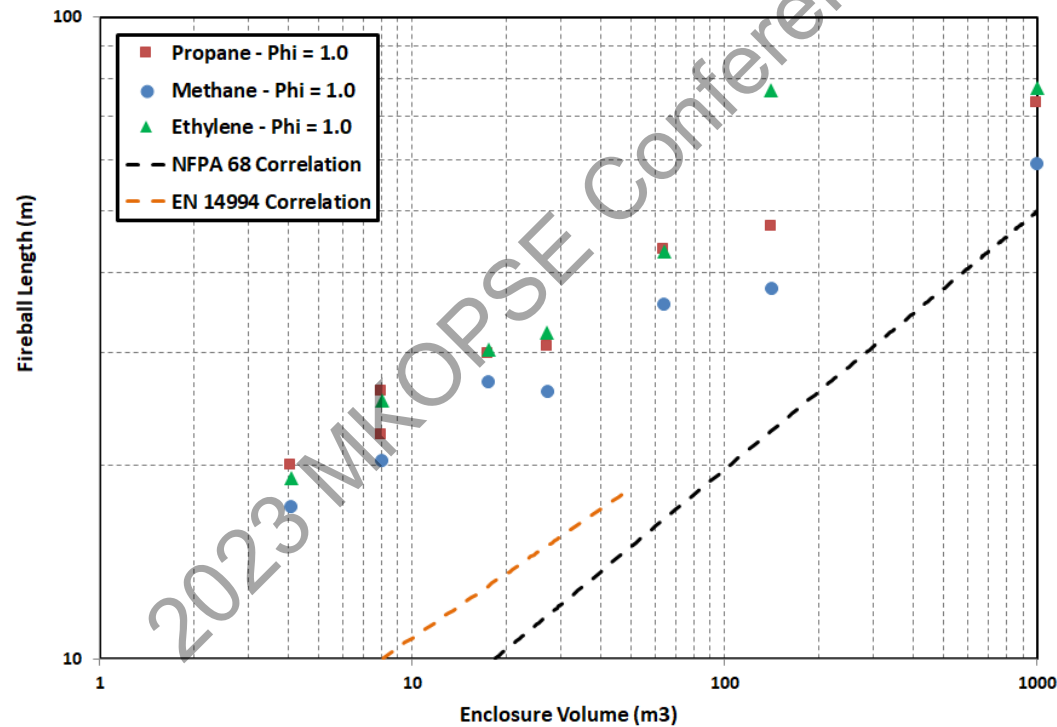
Ethylene

Run: 680135
Var: T_3D
Time: 0.00 s (0)
Plane: XZ, Y=0.1m



Temperature
Contours
500 K – 2200 K

Gas Explosion Venting Fireball – CFD Results



Conclusions – Flammable Gas

- Stoichiometric, or near-stoichiometric, conditions pose a worst-case scenario for explosion venting fireball lengths.
- Relatively-poor agreement was obtained between gas deflagration venting simulation fireball length data and the empirical correlations.
 - Sizes calculated using the FLACS CFD model are up to a factor 2 to 3 larger than the estimates obtained using the standard correlations.
- A dependency of the fireball size on flammable gas species has been identified with propane and ethylene leading to larger fireballs.
 - Further analysis is required to determine the relative role of the expansion ratio and flame speed on the fireball dimensions

Explosion Venting Examples





Risk Assessment: **How to avoid slipping, tripping, and falling over the numbers**

Will Sharpe

2023 MKOPSC

kentplc.com

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Frank Hart


- Mathematical Modeller (DNV) since 2019
- Previously
 - Risk consultant (Risktec Solutions)
 - Software engineer (Tessella, now CapGemini)
 - Research associate (School of Physics, University of Bath)



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Model improvements and validation for buried CO₂ pipeline ruptures

2023 MKOPSE Conference

Introduction

- Dense phase pipeline transport
- Necessary for reducing CO₂ emissions during energy transition
- Especially for buried pipelines, modelling these is not easy
- Various attempts to better assess potential hazards

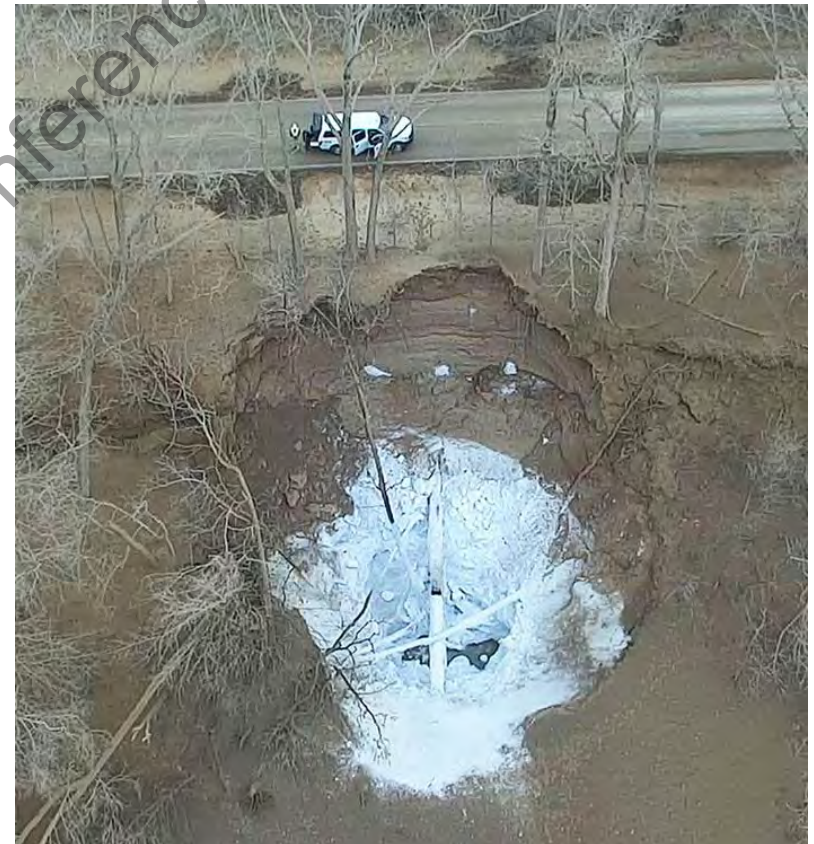
6" buried CO₂ pipeline rupture at DNV Spadeadam



Introduction

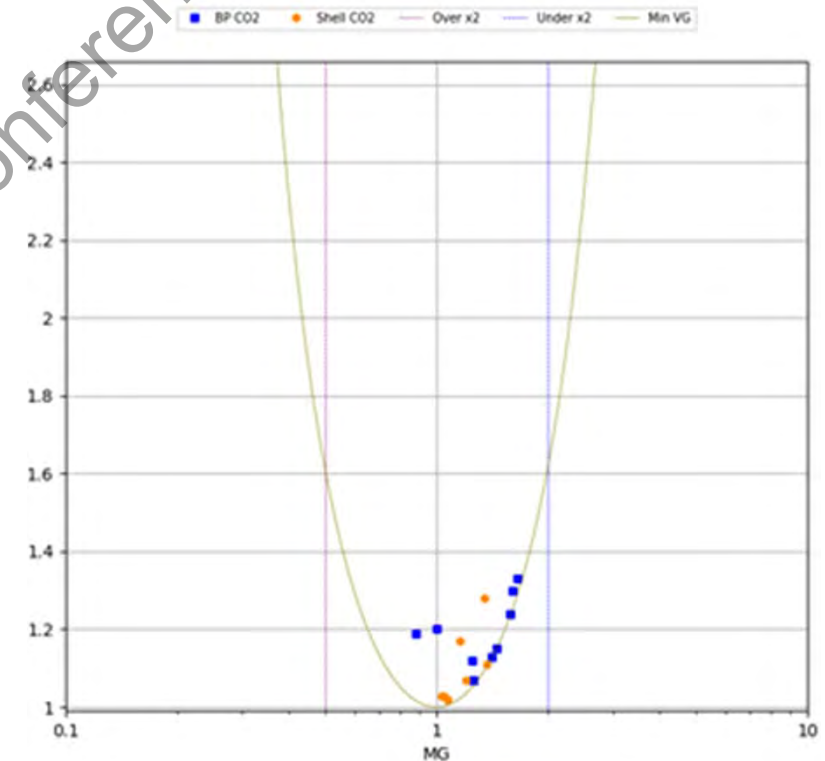
- The hazards of CO₂ pipeline transport are registering with the public and politicians
- Some high profile failures
- Current hazard zones demonstrably inadequate

Crater from a 24" pipeline rupture near Satartia in 2020



Modelling and Phast 8.71 CO₂ Validation

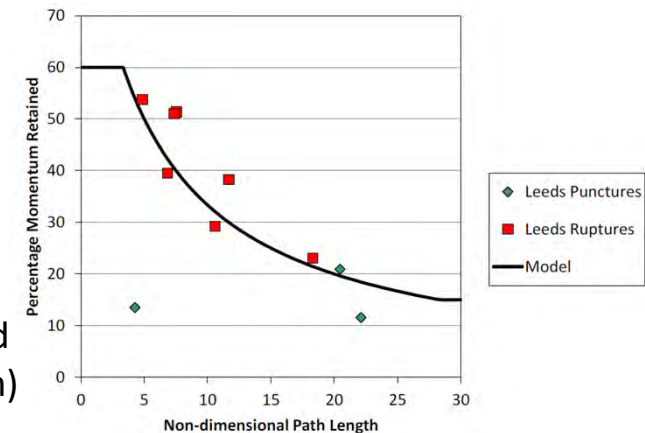
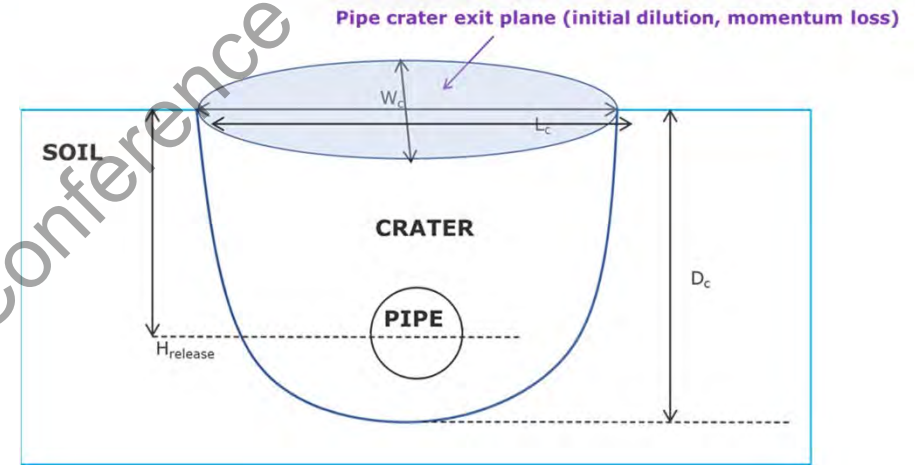
- Use the widely-used Phast UDM dispersion model
- Existing validation for small-medium scale above ground releases
- Specific to buried pipelines...
 - 'Crater' model
 - Thermodynamic model extension - solid phase CO₂



Validation against CO2PIPETRANS dispersion experiments

Crater modelling

- Crater dimensions
- Post-expansion source has additional air entrainment and reduced velocity
- Based on a small number of idealised CFD simulations
- Velocity appears too high for standard jet-based dispersion models

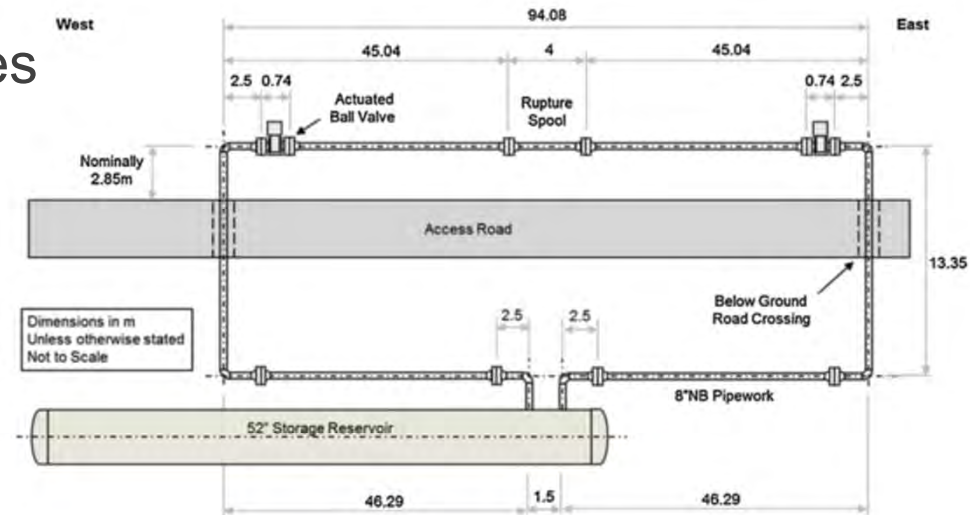


Crater model schematic (top), and correlation for momentum against 'path length' (bottom)

COSHER experiments

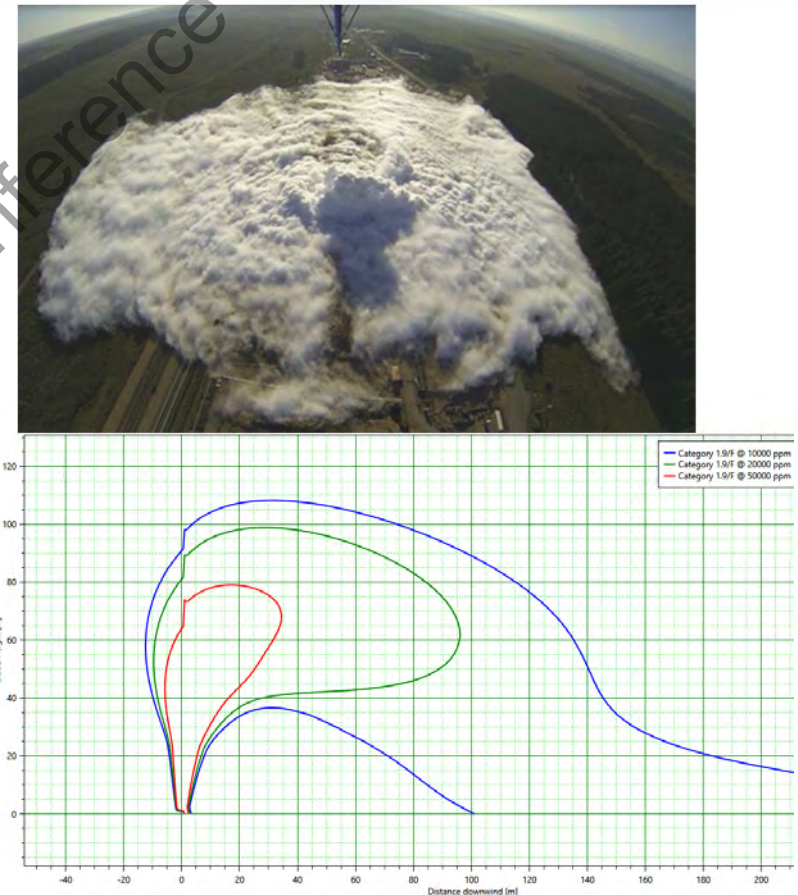
- Carried out at DNV Spadeadam test site in the UK
- Two punctures from buried 6" CO₂ pipelines (1.9/F and 4.7/D weather)
- Complex release geometry – requires some simplifying assumptions for source term
- Limited publicly available data

COSHER experiments – equipment layout



COSHER Validation (v8.71)

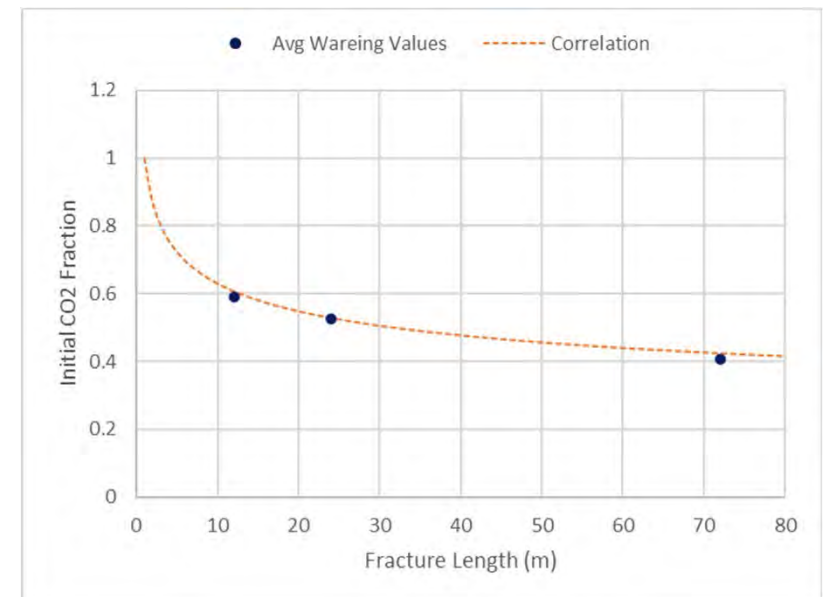
- Visible comparison of experiment vs prediction sufficient to show issues
- Experiment shows...
 - No evidence of an elevated plume
 - 'Pancake' shaped cloud around the release
- Primary cause was velocity out of the crater



COSHER 2 (low windspeed) release at 120s

Improved crater model

- Simplified model derived – flow area defined by crater width
- Implies generally larger areas and much reduced velocities (esp. for small L_f)
- Air entrainment correlation based on full set of CFD simulations
- Full bore ruptures only

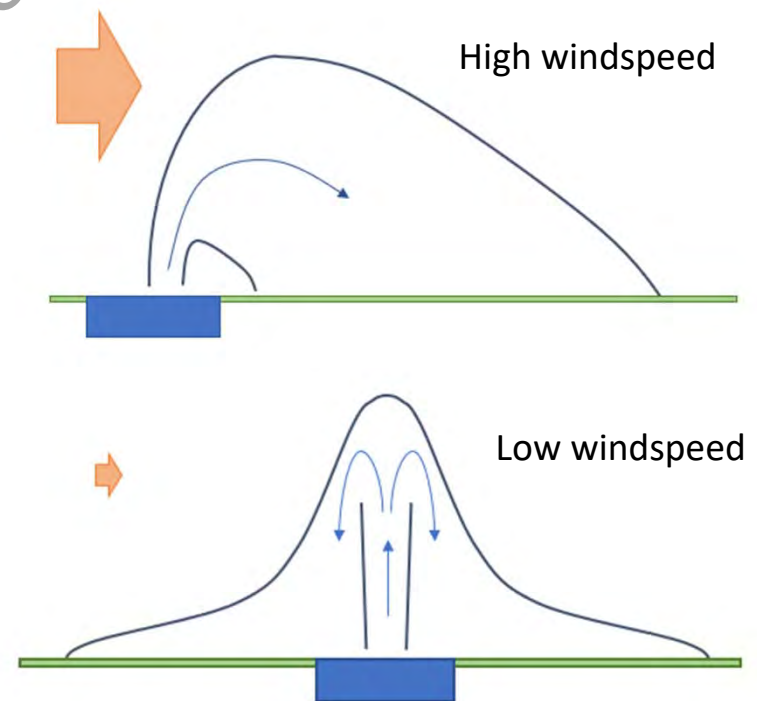


Modified Air entrainment correlation

CO₂ dispersion in contrasting wind conditions

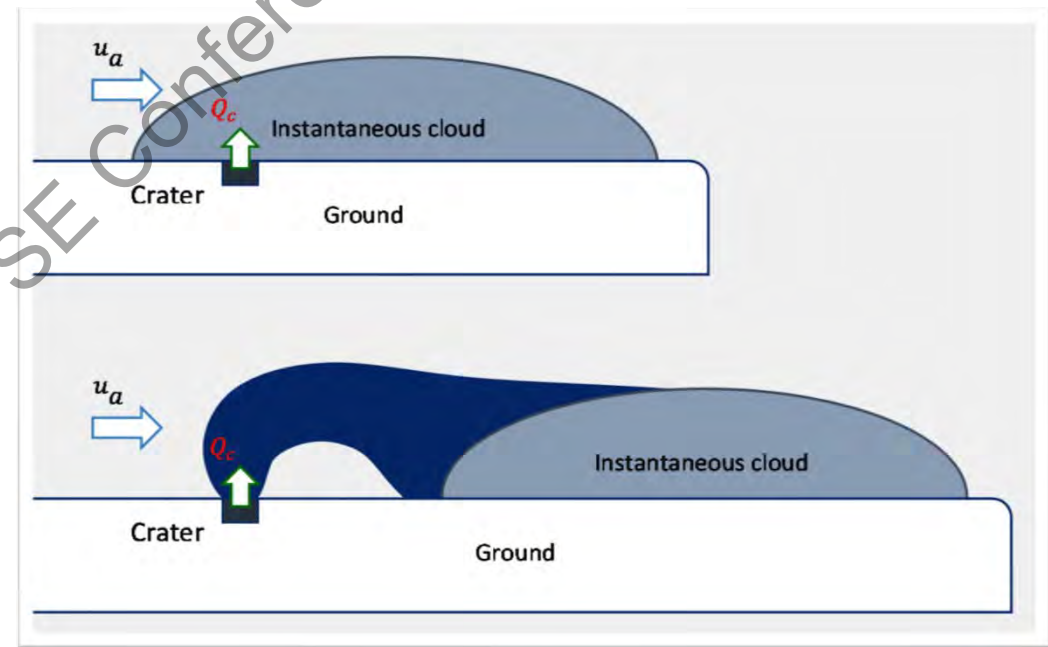
- Plume trajectory bent over by wind
- No re-entrainment, no upwind spreading
- Suitably handled by UDM

- Low impact on trajectory, results in 'fountain' behaviour
- Circular spreading at ground level
- Not well handled by standard UDM



'Gas Blanket' model

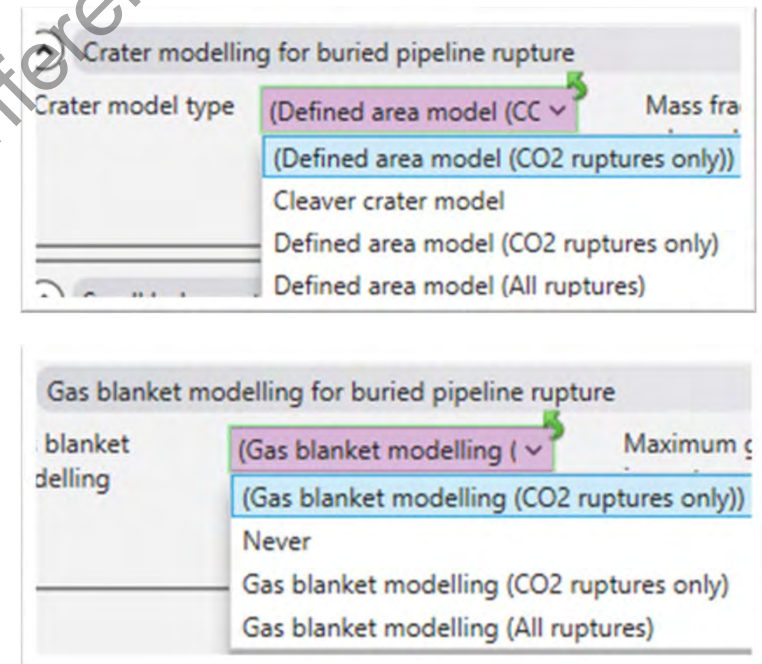
- Requires the initial jet-based plume to touch down at $> 45^\circ$ impact angle
- Represents the release as an instantaneous release
- Fed by a time-varying crater source
- Eventually the instantaneous cloud drifts and uncovers the crater
- Any remaining source treated as normal vertical jet



Gas blanket modelling

Phast v8.9

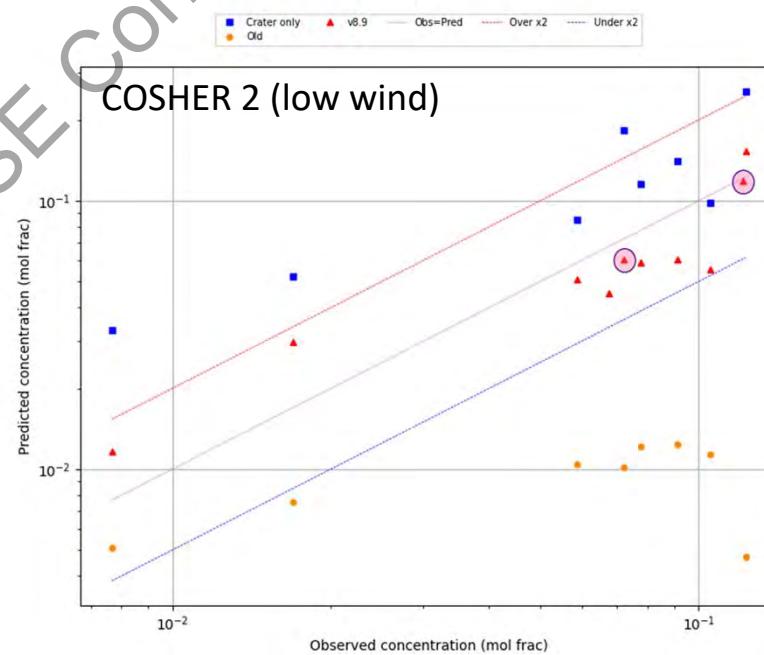
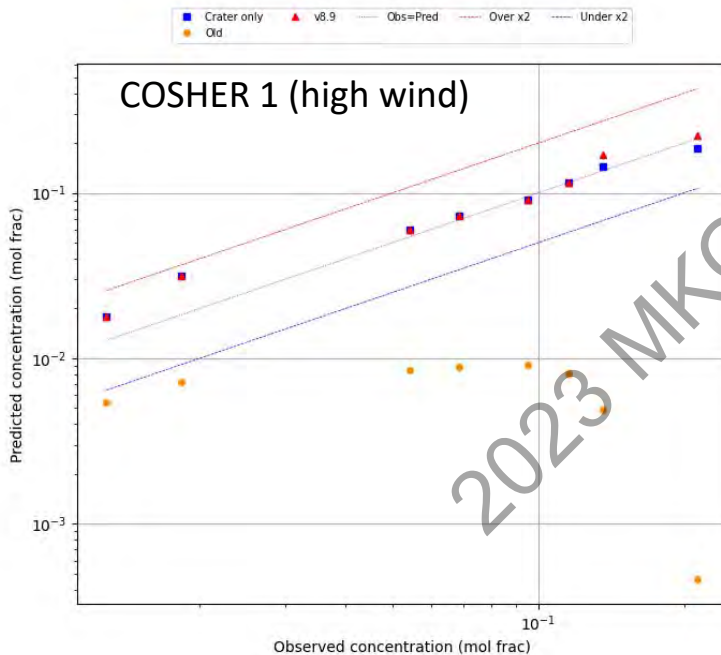
- Separate options for crater modelling and gas blanket modelling
- Options for both...
 - Original (v8.71) models
 - Improved models for pure CO₂ only (default)
 - Improved models for all materials



Phast parameters controlling improved modelling

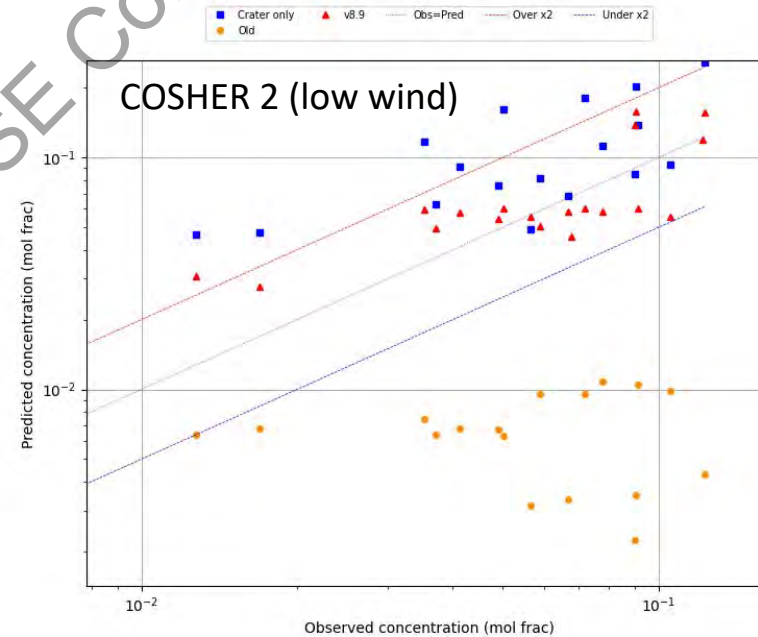
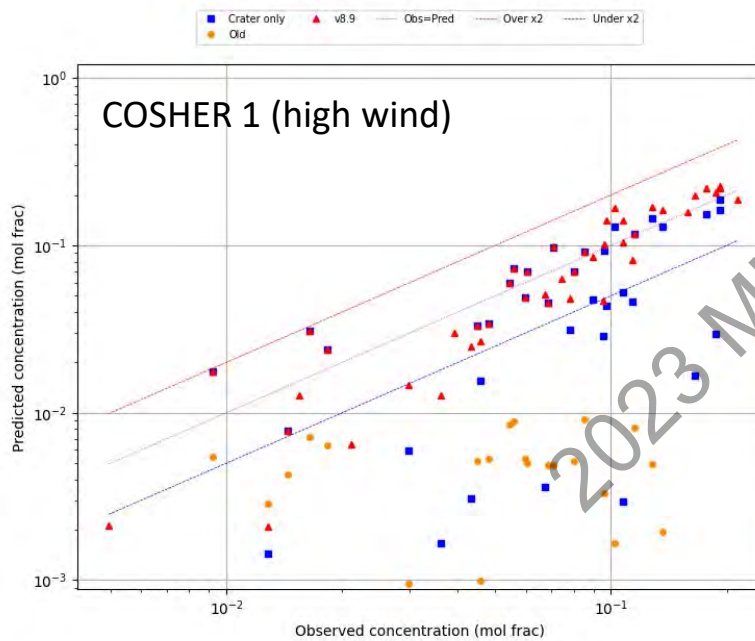
COSHER Validation – 8.9 vs .871 models

Arcwise maximum concentrations – observed vs predicted



COSHER Validation

Pointwise maximum concentrations – observed vs predicted





COSHER Validation

- Improved crater model alone.
 Vastly improved downwind ground level concentrations
- With gas blanket model (esp. for low windspeed cases):
 - Additional improvement in downwind concentrations
 - Major improvement in crosswind and upwind concentrations

	COSHER 1	COSHER 2	Overall
Phast 8.71			
MG	12.41	5.94	8.59
VG	>1000	46.41	557
Phast 8.9 (Crater only)			
MG	0.89	0.51	0.67
VG	1.06	1.94	1.43
Phast 8.9			
MG	0.86	1.09	0.98
VG	1.06	1.15	1.11

Geometric mean and variance for arcwise maximum concentrations

Further work and limitations

- Lack of available data suitable for development / validation is a critical issue
- Inability to measure the post-crater cloud makes life difficult
- Do the crater changes make sense for other materials?
- Scalability?
- What about punctures?

Proposed JIP for CO₂ Dispersion



Carbon dioxide pipeline risk assessment

Plans for a programme of CO₂ dispersion experiments and model development

Simon Gant*, Zoe Chaplin, Martin Thomson Health and Safety Executive (HSE), Buxton, UK

Dan Allason, Ann Halford, Karen Warhurst, Mike Acton, Mike Harper, Jan Stene, Gabriele Ferrara, DNV

Jo Miles, Sarah Bragg, Joel Howard, Matthew Turner, DSTL, UK

Matthew Hort, Frances Beckett, Met Office, UK

Tom Spicer, University of Arkansas, USA

Jon Lang, Ed Sullivan, National Chemical Emergency Centre, Ricardo, UK

Carbon Capture and Storage Association (CCSA), Health and Safety Technical Working Group Meeting, London, UK
31 August 2023

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Review and Validation of Phast Dispersion Model required for LNG Siting Applications in the US

2023 MKOPSE Conference

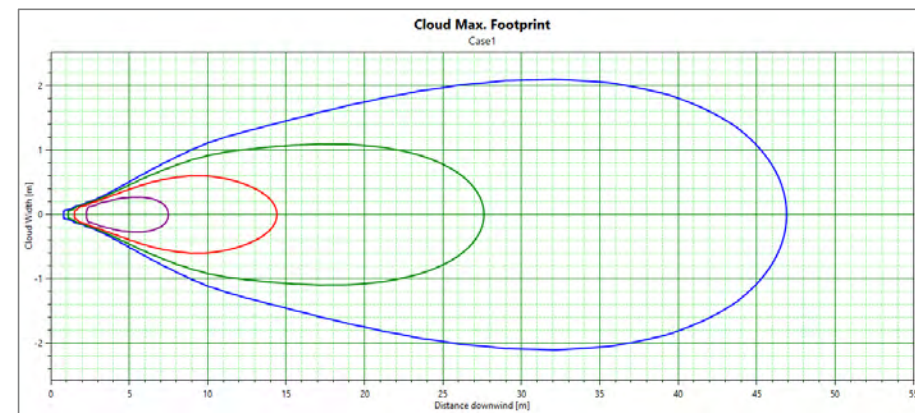
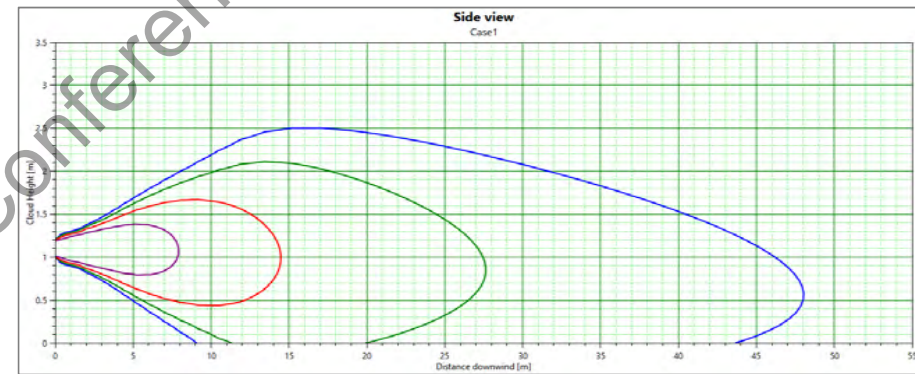


Introduction

- PHMSA require an exclusion zone around LNG facilities
 - Regulation 49 CFR 193
- This to be calculated using 'approved' models.
- Phast 6.7 was approved in 2011
- Model improvements, architectural changes, Phast 6.7 end-of-life argued for an updated approved version
- A petition was submitted to approve Phast 8.4

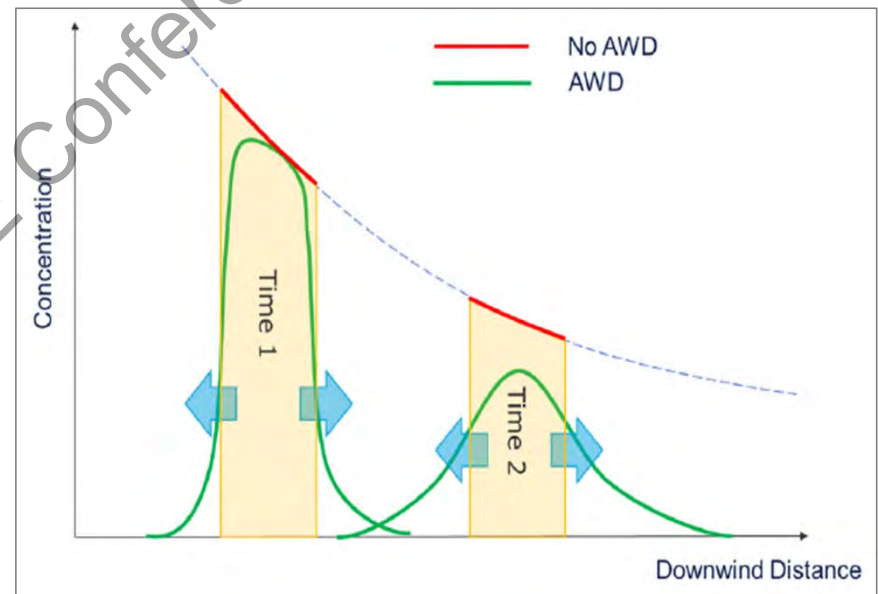
Phast - UDM

- Integral model comprising linked DAEs
- Combined jet, heavy-gas and passive models
- Imposes similarity concentration profile
- Finite duration, time-varying and instantaneous
- Droplets and rainout



Changes since v6.7

- Many changes including:
 - Pools
 - Cloud-pool linking
 - AWD
 - Instantaneous expansion
 - Improved solver

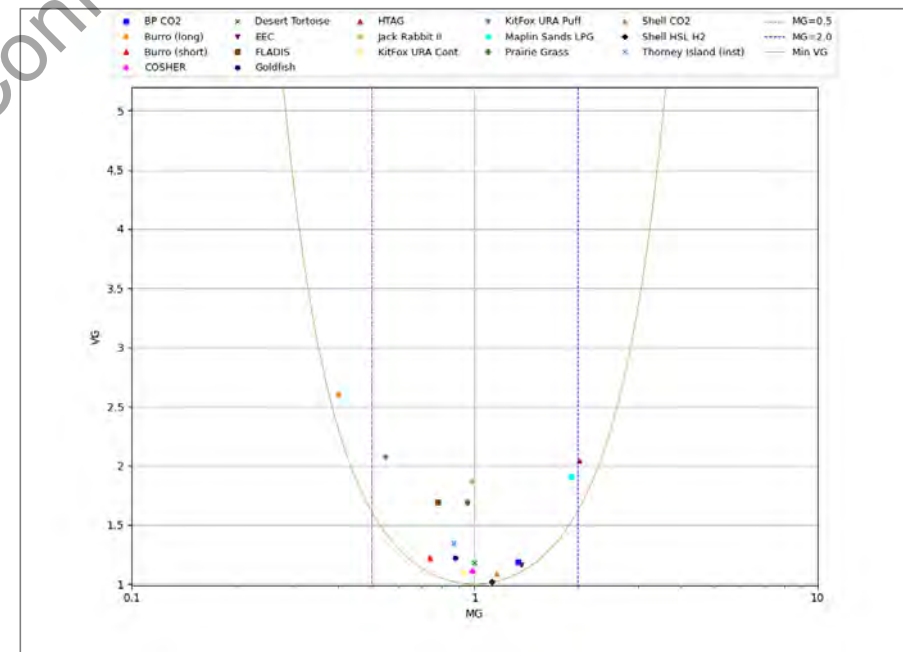




Existing validation set

- Extensive validation set with each release
- Includes most PHMSA experiments
- Generally good agreement with experiment
- All available as .psux files on request

Arc-wise concentration



PHMSA Model Evaluation Protocol

- Submission based on 2016 MEP
- Updated experimental database
- 'Change-log' report
 - Scientific Assessment
 - Verification
 - Validation
- External expert reviewer



MEP Changes (since Phast 6.7)

- Method for arc-wise concentrations
 - Maximum prediction at arc sensor locations
- Updated experimental data:
 - Full review of data set
 - Errors corrected
 - Point-wise concentrations added
 - Some post-ignition points removed
- Additional physical & statistical measures

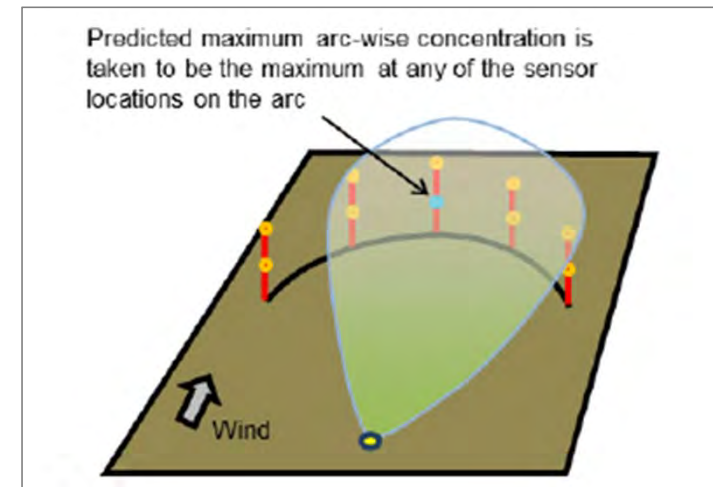


Image: 2016 MEP



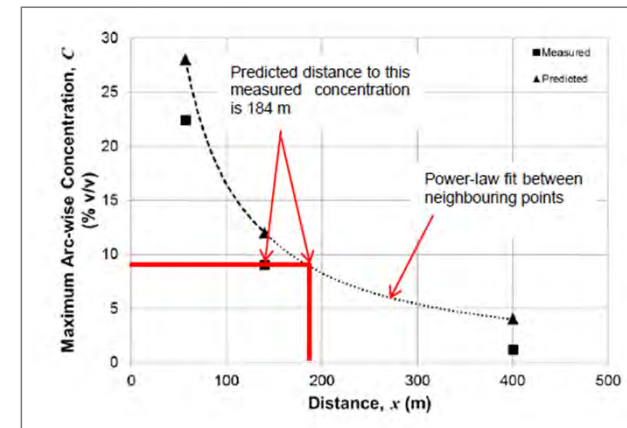
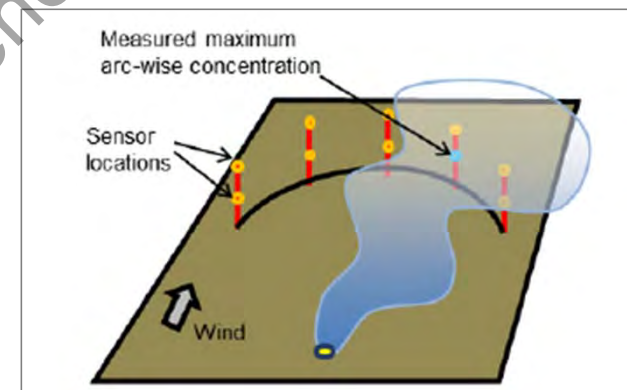
Validation Experiments

- 17 Experiments
 - No obstructions
 - 12 field experiments
 - 5 wind-tunnel
- Burro & Coyote
 - Short and long time averages
 - Each assessed separately

Experiment	Trial	Type	Material	Notes
Maplin Sands	27	Field	LNG	
	34			
	35			
Burro	3	Field	LNG	Short and long time averaged concentrations available
	7			
	8			
	9			
Coyote	3	Field	LNG	Short and long time averaged concentrations available
	5			
	6			
Thorney Island	45	Field	Freon & N ₂	
	47			
CHRC	A	Wind tunnel	CO ₂	
BA-Hamburg	DA0120	Wind tunnel	SF ₆	
	DAT223			
BA-TNO	TUV01	Wind tunnel	SF ₆	
	FLS			

Assessment Results

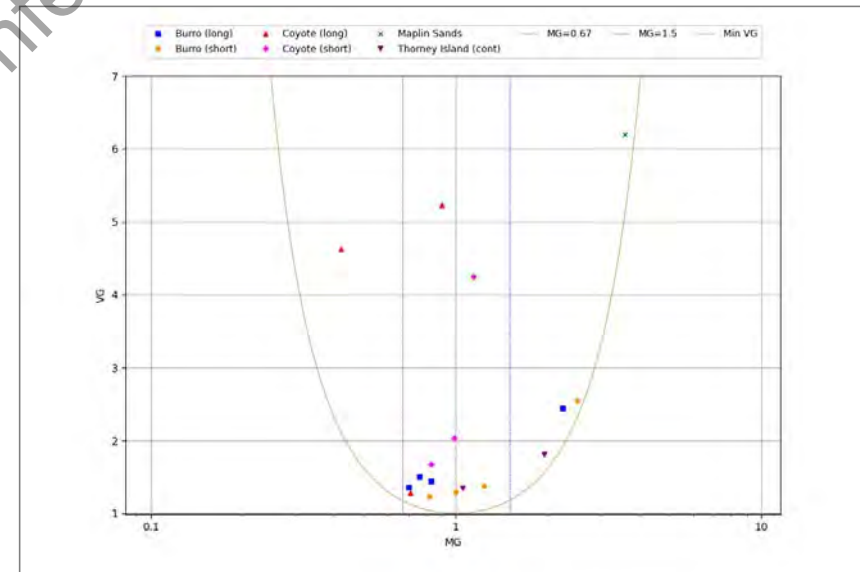
- 4 physical comparison parameters
 - Maximum arc-wise gas concentration
 - Maximum point-wise gas concentration
 - Distance to measured gas concentration
 - Width (calculated - not presented here)
- 9 statistical performance measures
 - Not all relevant for each parameter



Images: 2016 MEP

Arc-wise Concentration (Field)

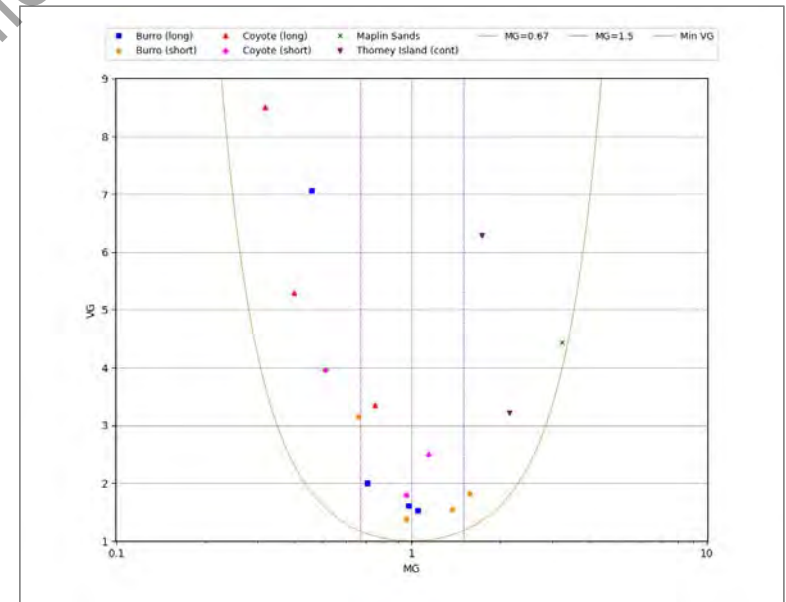
- Most within PHMSA scrutiny range
- Coyote 6 (over), TI45, BU08 (under)
- Maplin Sands high underprediction
 - Consistent feature
 - Return to this shortly



$$MG = \exp \left(\ln \left(\frac{C_m}{C_p} \right) \right) \quad VG = \exp \left(\left[\ln \left(\frac{C_m}{C_p} \right) \right]^2 \right)$$

Point-wise Concentration (Field)

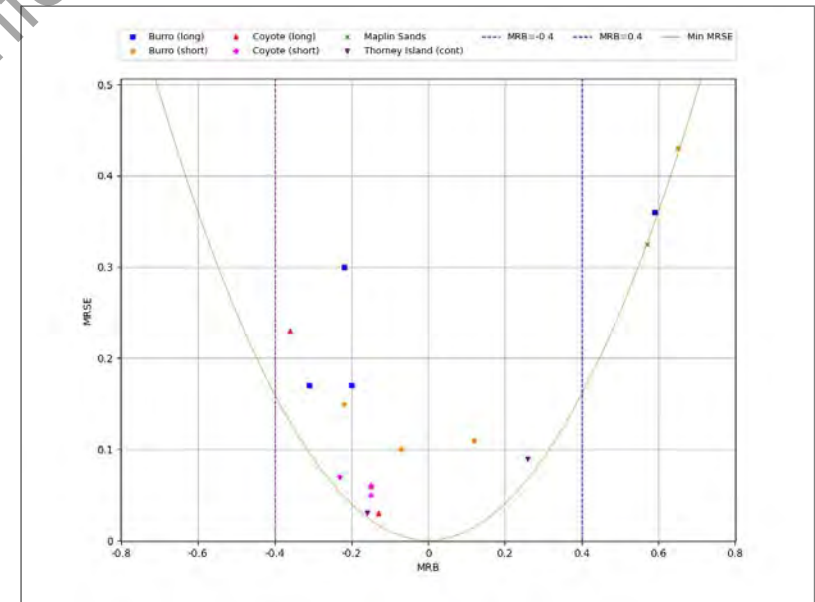
- More scatter
- Burro & Coyote (short) mainly within PHMSA scrutiny range
- Coyote (long) overprediction
- Thorney island underprediction
- Maplin Sands high underprediction



$$MG = \exp \left(\ln \left(\frac{C_m}{C_p} \right) \right) \quad VG = \exp \left(\left[\ln \left(\frac{C_m}{C_p} \right) \right]^2 \right)$$

Distance to arc-wise concentration (Field)

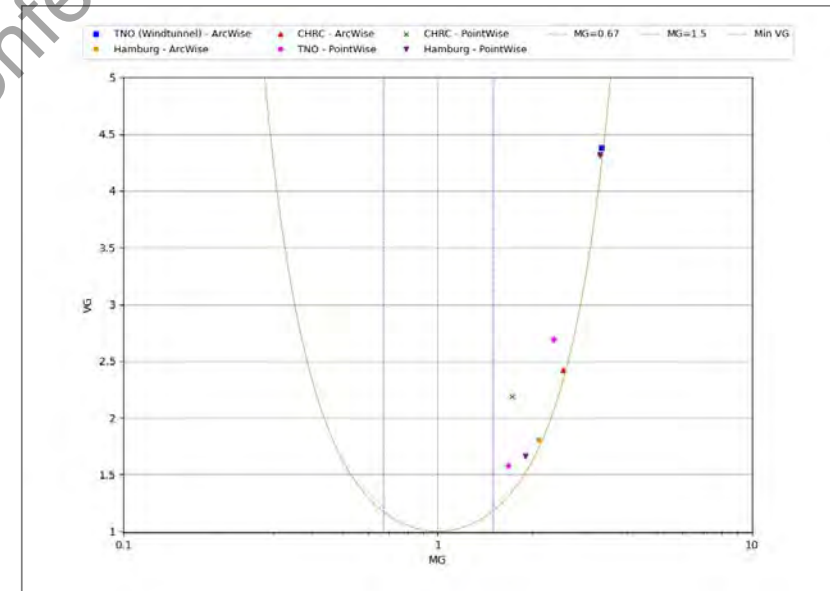
- Largely within PHMSA scrutiny range
- Slight trend to overpredict (MRB < 0)
- Burro 8 underprediction
- Maplin Sands high underprediction



$$MRB = \left\langle \frac{C_m - C_p}{\frac{1}{2}(C_p + C_m)} \right\rangle \quad MRSE = \left\langle \frac{(C_p - C_m)^2}{\frac{1}{4}(C_p + C_m)^2} \right\rangle$$

Wind-tunnel cases

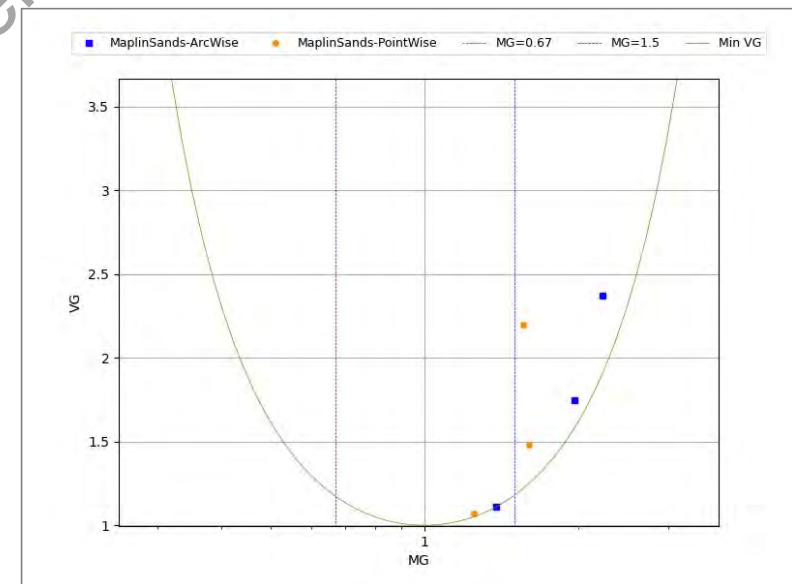
- Consistent underprediction
- Possibly due to field-scaling
 - UDM used field not wind tunnel scale
- Sensitive to roughness
 - Improved alignment with reduced SR
- Improves on Phast 6.7 results



$$MG = \exp\left(\ln\left(\frac{C_m}{C_p}\right)\right) \quad VG = \exp\left(\left[\ln\left(\frac{C_m}{C_p}\right)\right]^2\right)$$

Uncertainties

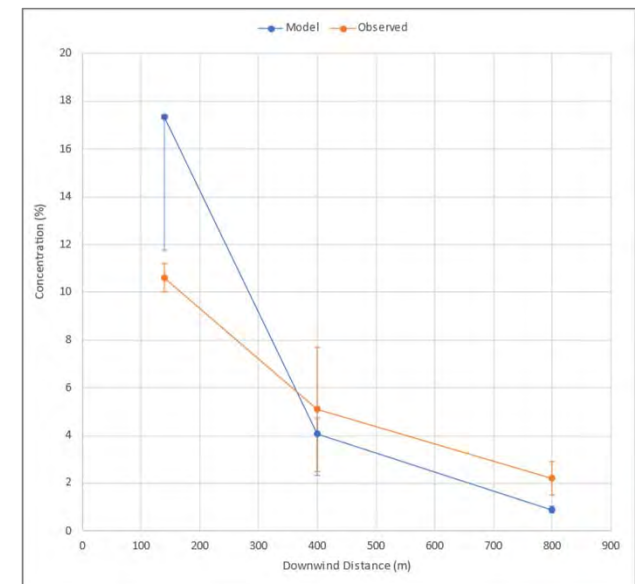
- Maplin Sands
 - Thin clouds, poor spatial resolution
 - Sensitivity - sensors at $y=0$ (5-10% change)
 - Much improved alignment
- Burro, Coyote
 - Cases with peak concentrations at arc edges
 - Terrain impact & bifurcation in Burro 8



$$MG = \exp \left(\ln \left(\frac{C_m}{C_p} \right) \right) \quad VG = \exp \left(\left[\ln \left(\frac{C_m}{C_p} \right) \right]^2 \right)$$

Sensitivities

- Sensitivity study
 - 7 cases
 - Between 1 and 8 individual parameters
- Some significant variations
 - Burro 9 (long) arc-wise shown
 - High surface roughness at lower bound
 - Different parameters at higher bound
 - Factor >2 between low/high at 400m



Summary

- PHMSA approval process outlined
 - Detailed submission due to >10 years since Phast 6.7
 - More rigorous: 2016 MEP and v12 validation database
 - Validates well, particularly for field trials
 - Uncertainties around Maplin Sands well understood
- Phast 8.4 approved April 2023
 - Identical conditions to Phast 6.7
 - Uncertainty factor of 2 for LFL distances (i.e. use $\frac{1}{2}$ LFL)
 - www.regulations.gov docket PHMSA-2021-0041



Acknowledgements

- Anay Luketa (Sandia National Laboratories)
- Thach Nguyen (PHMSA)

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October 11-13, 2023

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Title: Data-Driven Model for Multiphase Leak Detection Using Dimensional Analysis Technique

26th Process Safety International Symposium

List of Content

- 1 Self Introduction**
- 2 Introduction**
- 3 Literature review**
- 5 Objectives**
- 6 Methodology for model development**
- 7 Results and Discussion**

Conclusion
Future work
Nomenclature
References



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1 Self Introduction:

Name: Mohammad Azizur Rahman

Designation: Associate Professor
(TAMU Qatar)



Research focus:

Multiphase flow, Flow assurance, Cuttings transport, Leak Detection, Gas kick, carbon capture and storage, Geothermal energy, Ionic liquid, reservoir characterization, Statistical Analysis, Machine Learning Application in Oil and Gas Industries, and Aphron-based drilling fluid.

https://scholar.google.com/citations?hl=en&user=PYRtIBIAAAAJ&view_op=list_works&sortby=pubdate

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26th Process Safety International Symposium

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Introduction:

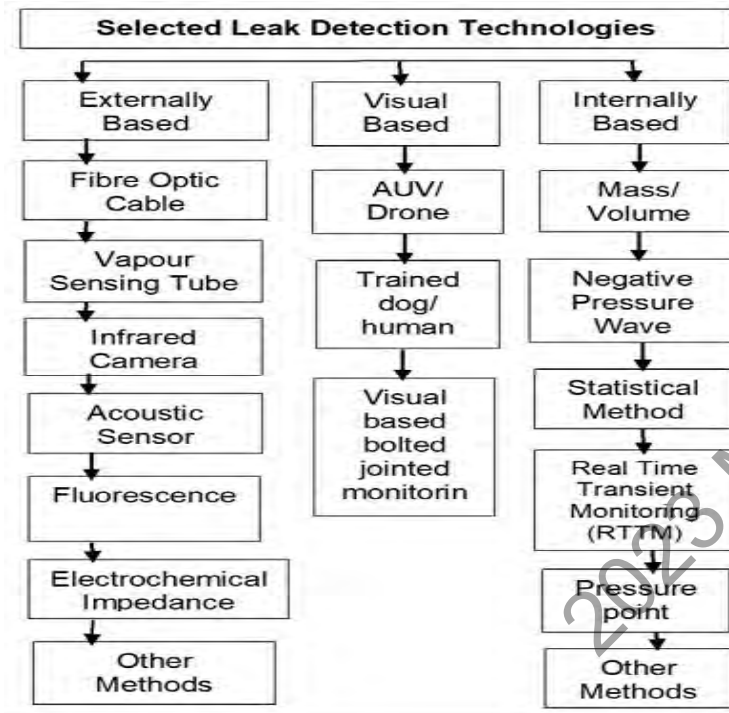
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Introduction: Why study leak detection?

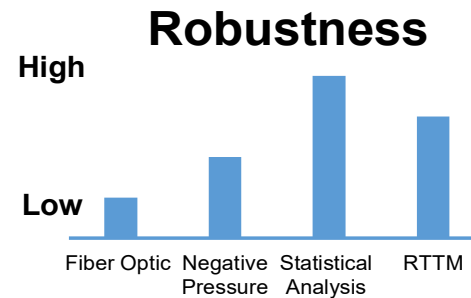
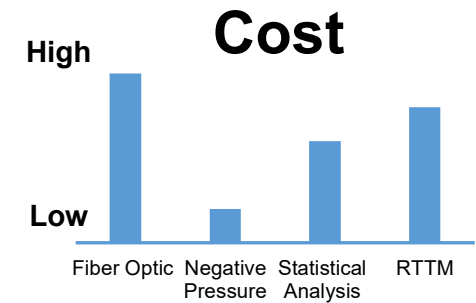
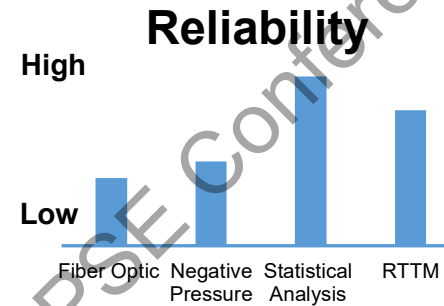
- Leaks may occur in the existing pipelines although designed with quality construction and appropriate regulations.
- Huge economic impact.
- Failure can have an adverse impact on life, the economy, the environment, and corporate reputation.



Introduction: Different types of leak detection.



(Adegboye et al., 2019; Zhang et al., 2013)



- In this study we focus on Internally based methods i.e. physics based mechanistic correlation and data-driven non-dimensional correlation.
- These methods generally have high reliability, robustness and lower cost.

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Literature review:

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List of literature for mechanistic Correlation:

Fluids used	Model used	Leak in terms of	Focus	Key remarks	Reference
Gas-liquid	Beggs and Brill's two phase correlation	Inlet and outlet total flow rate	Subsea pipelines	Higher leak size improves leak detection. Compressible liquid inhibits leak detection.	(Gajbhiye and Kam, 2008)
Gas-Oil	Beggs and Brill's two phase correlation	Change in inlet pressure, change in outlet flow rate	Deepwater operations	Outlet flowrate was more favourable as compared to inlet pressure. Longer distance, larger opening size, and compressible phase are favorable.	(Kam, 2010b)
Liquid	Probabilistic approach	Mass-imbalance	Pipeline	Able to detect leak location and leak size	(Rougier, 2005)
Water	Steady and un-steady state approach.	Pressure	Pressurized pipe system.	Higher pressure improves leak detection in a steady state as compared to an un-steady state condition.	(Ferrante et al., 2014)
Two-phase flow	Combination of numerical and analytical approach.	Pressure, Heat transfer	Wellbore	Deviated wells loses more heat to the formation as compared to the vertical wells because of higher residence time.	(Hasan et al., 1998)
Natural Gas	New mathematical model using a multi-rate test.	Flow rate and Pressure	Pipeline	Two leaks in a pipeline is detected instead of one leak.	(Rui et al., 2017)

Literature gap:

- The number of mechanistic correlations available for multiphase flow is still very limited.
- Most of the correlations (e.g. Kam 2010, Gajbhiye et al. 2008) assumes that we know leak parameters. However, in actual conditions most of the times we do not have sensors at the leak locations.
- Multiphase correlations are complex and time taking.

List of literature for Dimensional Analysis (DA):

Fluids used	Flow geometry	Key remarks	Reference
Gas-liquid	Pipe flow	A model was proposed to scale up or scale down pressure drop and liquid hold up based on DA	(Al-Sarkhi et al., 2016)
Gas-liquid	Stratified pipe flow	DA helped to scale up lab scale result to large scale facility.	(Farokhpoor et al., 2020)
Solid-liquid	Annulus pipe flow	Non-dimensional correlation for pressure drop was developed for a wide range of operating parameters and validated with independent literature data.	(Barooah et al., 2022)
Solid-liquid	Annulus pipe flow	Non-dimensional correlation was validated with literature data and used to predict volume fraction during cuttings transport.	(Khaled et al., 2021)

Key notes:

- DA has been used successfully in multiphase flow to predict and scale up lab scale data to larger scale.
- DA usually consist of simpler calculations which can be done without numerical analysis.
- Use of DA for leak detection in pipeline cannot be found in literature.

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Objective:

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Objective:

- Develop a physics-based mechanistic model for pipeline leak detection.
- Perform Dimensional Analysis to develop a non-dimensional model using the validated data points from the mechanistic model.
- Validate the non-dimensional model with independent literature data.



Methodology for model
development:

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Development of mechanistic Correlation:

Material balance equations:

$$m_{tin} = m_{tleak} + m_{tout}$$

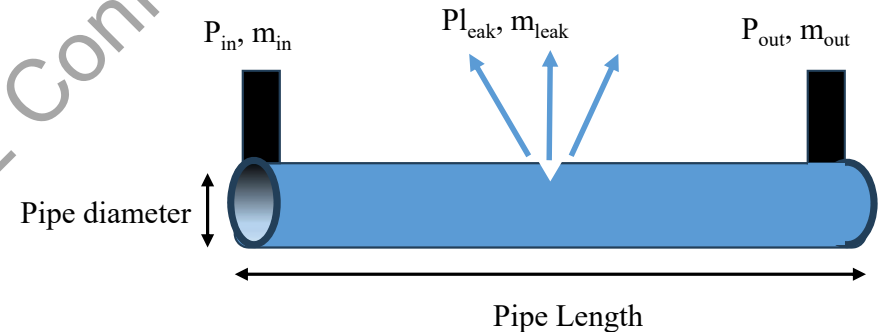
$$m_{gin} = m_{gleak} + m_{gout}$$

$$m_{Lin} = m_{Lleak} + m_{Lout}$$

$$f_{gin} = \frac{q_{gin}}{q_{tin}} = \frac{q_{gin}}{q_{gin} + q_{Lin}} = 1 - f_{Lin}$$

$$f_{gout} = \frac{q_{gout}}{q_{tout}} = \frac{q_{gout}}{q_{gout} + q_{Lout}} = 1 - f_{Lout}$$

$$f_{gout} = 1 - f_{Lout}$$



Where q is the volume flow rate, m is the mass flow rate, f is the fraction of gas, and t, g, L, in, out and $Leak$ are the subscripts for total, gas, liquid, inlet, outlet, and leak.

Development of mechanistic Correlation:

Pressure at any node is determined by:

$$P^{i+1} = P^i + \left(\frac{dP}{dx} \right) \Delta L$$

A leak which is regarded as a sink term can be described as the fluid loss due to the difference between the pressures inside and outside the pipe at the leak.

$$P_{\text{leak}} - P_{\text{sur}} = \frac{\rho_m q_{t\text{Leak}}^2}{C_d^2 \left(\frac{\pi d_{\text{Leak}}^2}{4} \right)^2}$$

Where,

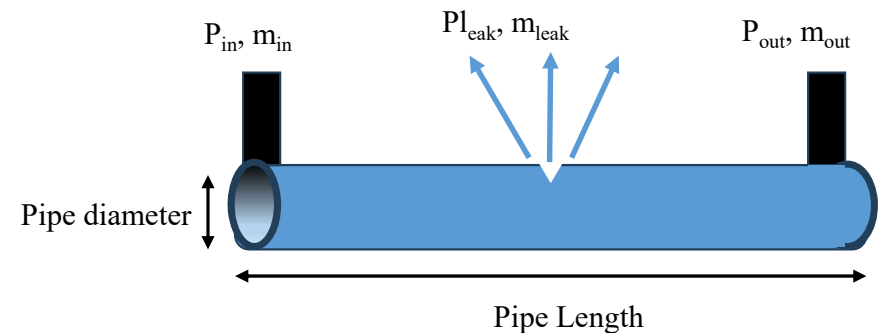
A_{Leak} = cross-sectional area of leak opening

d_{Leak} = leak equivalent diameter

ρ_m = mixture density at that point

C_d = Leak coefficient

$$\rho_m = \rho_g f_g + \rho_L f_L$$



New methodology for the leak detection correlation

Pressure drop is calculated using the Beggs and Brill model:

$$\frac{dP}{dx} = \frac{f_{tp} \rho_m (q_t/A) (q_t/A)^2}{gD}$$

Where f_{tp} is the friction factor during two-phase flow which is expressed as:

$$f_{tp} = f_n \left(\frac{f_{tp}}{f_n} \right)$$

$$\frac{f_{tp}}{f_n} = 2.2 \left(\frac{f_L}{y_L^2} \right) - 1.2 \text{ if } 1 < \left(\frac{f_L}{y_L^2} \right) < 1.2$$

Otherwise,

$$\frac{f_{tp}}{f_n} = \exp \left[\frac{\ln \left(\frac{f_L}{y_L^2} \right)}{-0.0523 + 3.182 \ln \left(\frac{f_L}{y_L^2} \right) - 0.8725 \ln \left(\frac{f_L}{y_L^2} \right)^2 + 0.01853 \ln \left(\frac{f_L}{y_L^2} \right)^4} \right]$$

Advantage:

- Most commonly used correlation for horizontal flow and circular pipe.
- Identifies the flow regime and liquid hold up, which helps to calculate the mixture velocity and density.
- Can be corrected for different inclination.
- Performs better for horizontal flow as compared to Hagedorn and Brown, Duns and Ros, Fancher and Brown, etc.
- Used in many commercial softwares such as Pipesim.

New methodology for the leak detection correlation

f_n is the fanning friction factor which is found by the Colebrook eq.

$$\frac{1}{\sqrt{f_n}} = -4 \log \left[\frac{-5.0452}{N_{re}} \log \left(\frac{7.149}{N_{re}} \right)^{0.8981} \right]$$

N_{re} is the Reynolds number, which is defined as:

$$N_{re} = \frac{\left(\frac{qt}{A}\right) \rho_m D}{\mu_L f_L + \mu_g f_g}$$

$$P_{leak} - P_{sur} = \frac{\rho_m q_{tLeak}^2}{C_d^2 \left(\frac{\pi d_{Leak}^2}{4}\right)^2}$$

μ_L and μ_g are the liquid and gas viscosities.

The liquid hold up for distributed flow is given by:

$$y = a \left(\frac{f_L^b}{N_{re}^c} \right)$$

As we have three unknowns (i.e., ρ_m , qt , d_{Leak}^2) and only two eq. (Leak eq. and Beggs and Brill correlation), therefore an iterative process is required to solve.

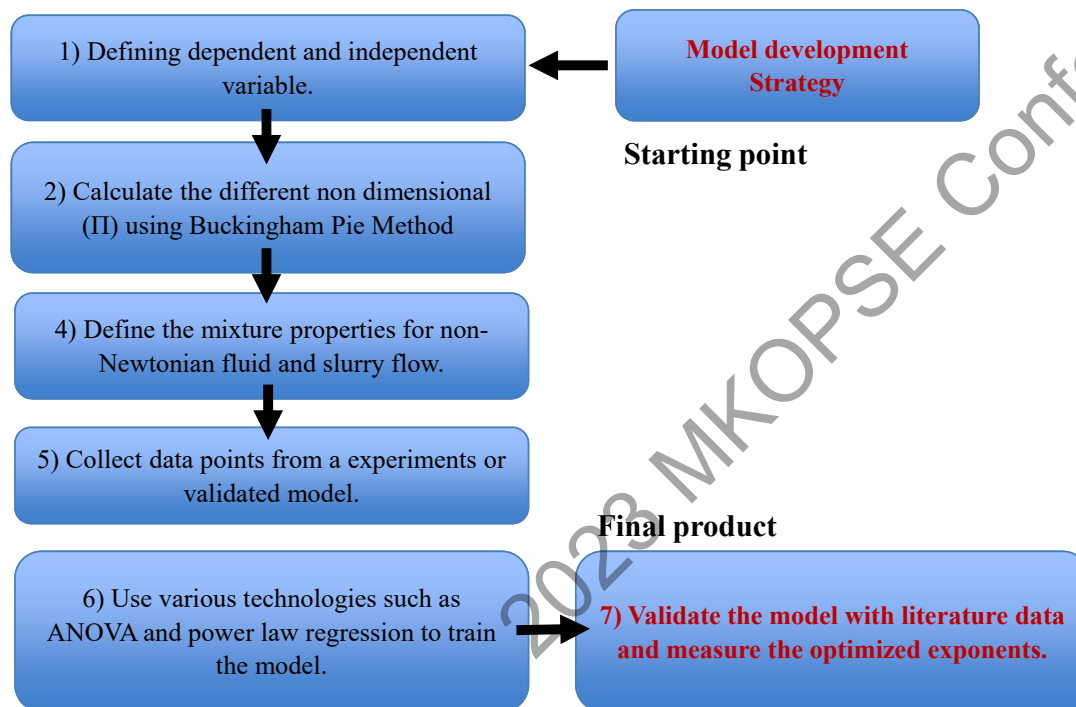
Methodology for leak detection

Steps:

- First, an initial value of total leak flow rate (q_{tleak}) is assumed, and leak pressure (P_{leak}) is calculated for different values of d_{leak} .
- Subsequently, an iterative method is employed to determine total flow rate at the pipe inlet (q_{tin}) in the upstream section, ensuring the desired value of inlet pressure P_{in} is achieved.
- Next, using another iterative method, total flow rate at the outlet q_{tout} is calculated for the downstream section while maintaining the desired constraint on outlet pressure P_{out} .
- As changing q_{tout} impacts q_{tleak} and thereby P_{leak} , the process iterates once again to find a new value of q_{tin} that maintains the desired P_{in} .
- This iterative process continues until optimized values of q_{tin} , q_{tout} , and q_{tleak} are obtained. During the entire process it needs to be ensured that the mass balance and pressure constraints are conserved.

This is be done either by developing macros in excel or in MATLAB

Methodology: Dimensional Analysis



Flowline of the model development strategy

Advantage

1. It gives us insight into what parameters could be ignored or treated approximately.
2. Upscale our correlations by testing it with a larger experimental data set which can be translated to different lab scale and field scale.
3. Develop non-dimensional flow regime map based on the non-dimensional numbers and surface operating conditions.

Methodology: Dimensional Analysis

Buckingham-Pi Theorem Methodology

Buckingham-Pi Theorem

1. Total n parameters can be grouped into n-m independent π groups expressed as: $\Pi_1 = f(\Pi_2, \Pi_3, \dots, \Pi_{n-m})$

1. n = Total number of dependent and independent variables
2. m = Minimum number dimensions required to characterize all the n parameters

Defining dependent and independent variable

Parameter	Symbol	Unit	Dimension
Mixture viscosity	(μ_m)	Kg/ms	M/LT
Mixture density difference	$\Delta\rho_m$	Kg/m ³	M/L ³
Pipe length	L	m	L
Leak diameter	d_{leak}	m	L
Pipe diameter	D	m	L
Change in total mass flow rate	Δm	Kg/s	M/T
Leak pressure	P_{leak}	Pa	M/LT ²

Defining dependent and independent variable

- **Dependent variable**
 - Leak Pressure or
 - Leak flow rate or
 - Leak location
- **Independent Variable**
 - 1) Mixture viscosity
 - 2) Mixture density difference
 - 2) Pipe length
 - 3) Leak diameter
 - 4) Pipe diameter
 - 5) Change in total mass flow rate

(Busch et. al 2019)

Methodology: Dimensional Analysis

Defining dependent and independent variable

- Set of fundamental dimensions are selected: $[M, L, T] = 3$
- Total number of parameters = $n = 7$
- Repeated parameters = $R = 3$
 - Pipe diameter
 - Change in mixture density
 - Change in mass flow rate
- By Applying Buckingham pi theorem
Non dimensionless number = $7-3=4$

Methodology: Dimensional Analysis

Calculate the different non dimensional Π terms

- $\Pi_2 = \frac{\mu_m D}{\Delta m} \frac{\rho_{inlet}}{\rho_{outlet}}$
- $\Pi_3 = \frac{L}{D}$
- $\Pi_4 = \frac{d_m}{D}$
- $\Pi_1 = \frac{P_{leak} D^5 \Delta \rho_m}{\Delta m^2}$

Input parameters	Output parameter
Pipe Diameter (m)	Leak pressure (Pa)
Leak diameter (m)	
Liquid volume fraction at inlet, cLi	
Liquid volume fraction at outlet, cLO	
Change in total inlet and outlet mass flow rate (%)	

General Form:

$$\Pi_1 = a_1 \Pi_2^{a_2} \Pi_3^{a_3} \Pi_4^{a_4}$$

The values of the different exponents have to be calculated by experimental fit or regression method.

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Results and Discussion:

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Results and Discussion: Statistical Analysis

Range of parameters for model development

Operating parameters	Range (field units)	SI units
Pipe Diameter, D (inch)	1 inch to 5 inch	0.0762 - 0.172 m
leak diameter, dm (inch)	0.2 inch to 3 inch	0.0127 - 0.0762 m
Liquid outlet fraction, cL	0.3 - 0.628	
Pipe length (feet)	2000 - 10000 feet	600 - 6500 m
Mixture viscosity	0.1126 - 0.0017 cP	1.227×10^{-4} - 1.7×10^{-6} PaS
Mixture density (kg/m ³)	295 - 560 kg/m ³	18.4162 - 34.95 lb/ft ³
Leak location (m)	91 - 460 m	91 - 460 m
Inlet total mass flow rate (kg/s)	14 - 28 kg/s	31 - 62 lb/s
Outlet total mass flow rate (kg/s)	3 - 10 kg/s	6.6 - 22

Only the inlet and outlet parameters are selected that effect the leak pressure.

$$P_{leak} - P_{sur} = \frac{\rho_m q_{tLeak}^2}{C_d^2 \left(\frac{\pi d_{Leak}^2}{4} \right)^2}$$



Results and Discussion: Statistical Analysis

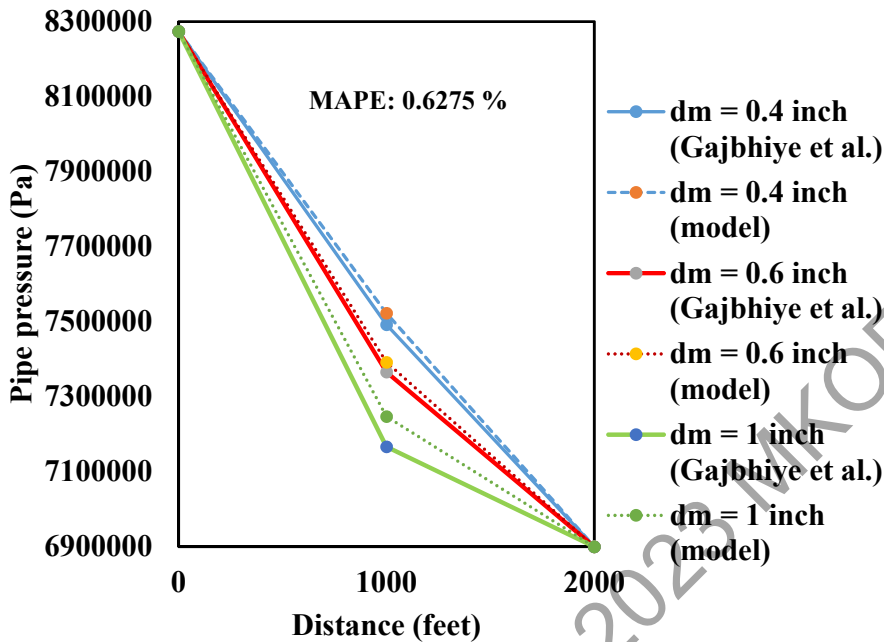
Correlation analysis

	Mixture viscosity	Mixture density (outlet)	Mixture density (inlet)	Pipe Length	Pipe Diameter, D	leak diameter	cLi	cLo	change in mass flow rate
Mixture viscosity	1								
Mixture density (outlet)	-0.312	1							
Mixture density (inlet)	4.167E-15	8.28E-15	1						
Pipe Length (feet)	0.198	0.279	0	1					
Pipe Diameter, D (inch)	0.1490	0.209	6.03E-16	-0.133	1				
leak diameter, dm (inch)	0.410	-0.184	3.81E-15	-0.366	0.572	1			
cLi	3.43E-15	8.18E-15	1	0	7.021E-17	3.15E-15	1		
cLo	-0.312	1	1.78E-15	0.279	0.209	-0.184	1.24E-15	1	
change in mass flow rate	-0.312	0.571	7.76E-16	0.474	-0.377	-0.480	6.59E-16	0.571	1

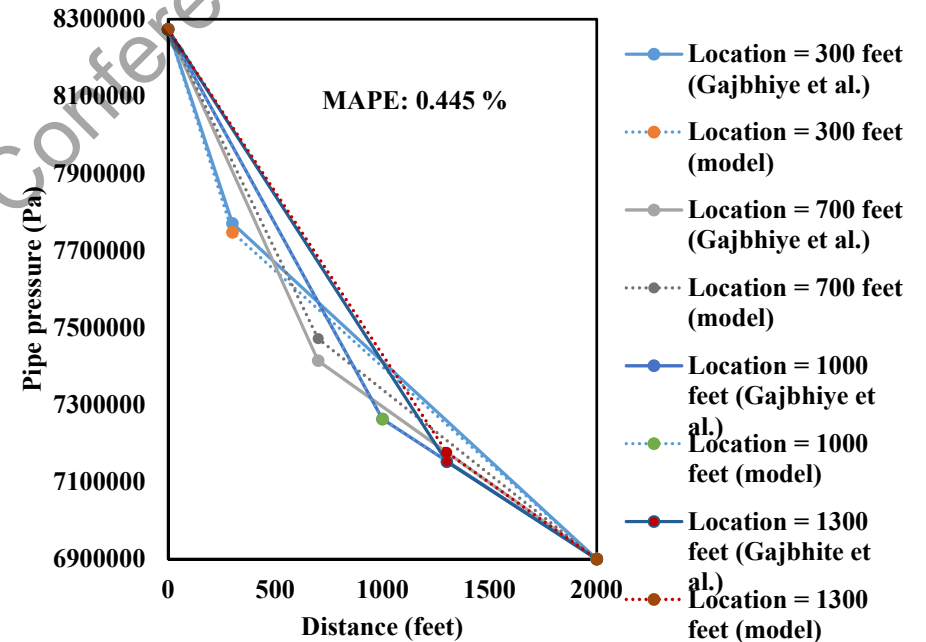
cLin and cLout is dependent on the inlet and outlet mixture density, therefore these parameters can be excluded

The ANOVA analysis shows that the input parameters are statistically significant and the correlation analysis suggest that the input parameters are statistically independent.

Results and Discussion: Validation of mechanistic model



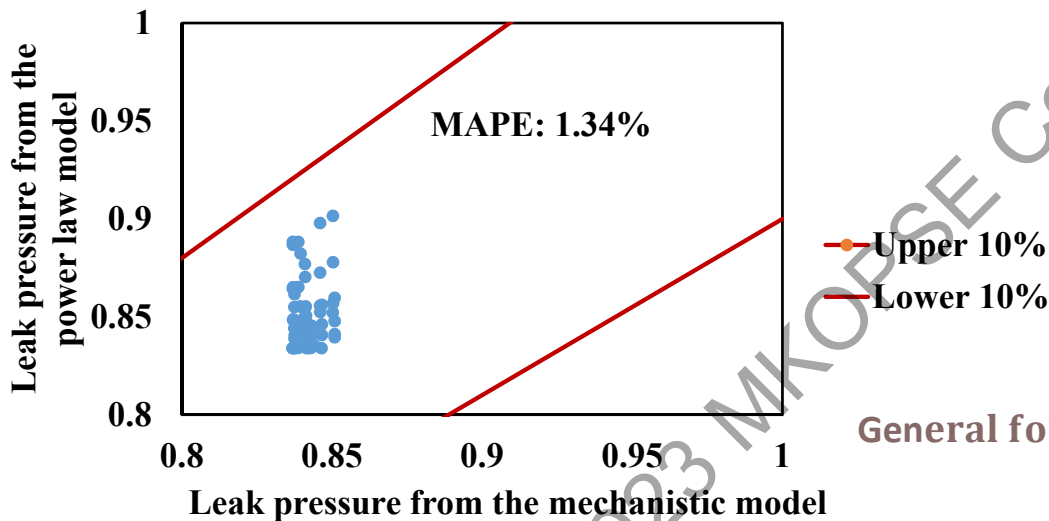
Validation for effect of pipe pressure



Validation for effect of leak location

Validation of mechanistic model for pipe pressure

Results and Discussion: Training and Optimization of non-dimensional model with mechanistic model



General form: $\Pi_1 = a \Pi_2^b \Pi_3^c \Pi_4^d$

Optimized Exponents	
a1	37.9228
a2	1.152
a3	1.732
a4	-0.354

Non-dimensional parameters	
----------------------------	--

$$\Pi_1 = \frac{P_{leak}}{P_1 - P_0}$$

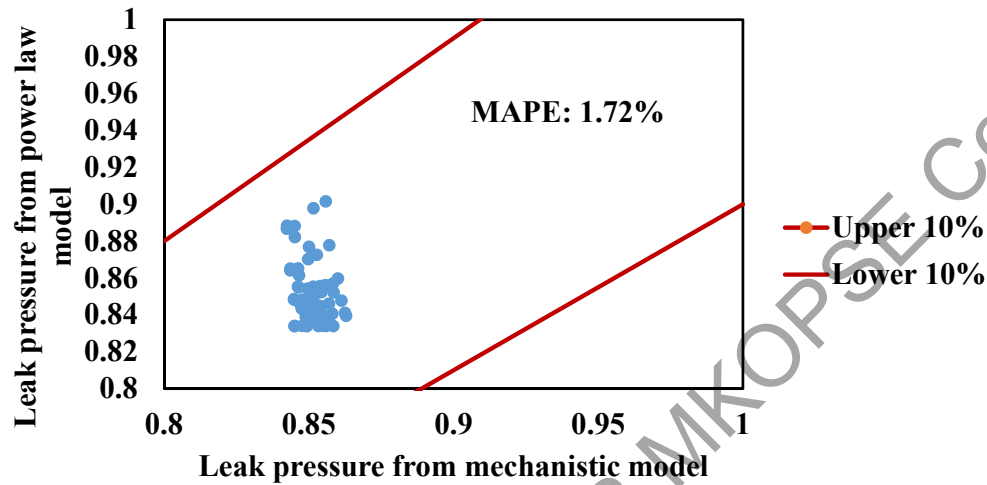
$$\Pi_2 = \frac{\mu_m D}{\Delta m} \frac{\rho_{inlet}}{\rho_{outlet}}$$

$$\Pi_3 = \frac{L}{D}$$

$$\Pi_4 = \frac{d_m}{D}$$

Model optimization is showing a good agreement with Mechanistic model with a MAPE of 1.34%.

Results and Discussion: Validation of the non-dimensional model.



Validation of leak pressure of the power law model with Gajbhiye et al. 2008

Final form of the non-dimensional correlation:

$$\frac{P_{\text{leak}}}{P_i - P_0} = 37.922 \left(\frac{\mu_m D}{m_t} \frac{\rho_{\text{inlet}}}{\rho_{\text{outlet}}} \right)^{1.152} \times \frac{L}{D}^{1.732} \times \frac{d_m}{D}^{-0.354}$$

Conclusion:

- This study Introduced an innovative mechanistic model for multiphase flow pipeline leak detection that achieved excellent predictability with a MAPE of only 0.63% through validation against independent literature data.
- A non-dimensional model was developed with impressive validation, MAPE of 1.34% and 1.72% with the mechanistic model and literature data.
- The non-dimensional model is particularly valuable for lengthy pipelines where dedicated sensors at leak locations are often lacking.
- This model offers user-friendly, real-time applicability during daily operations, in contrast to complex and time-consuming models.

Future work:

- It should be noted that the accuracy of the developed model can decrease when the range of operating parameters is too much out of the range provided in Table 3.
- Furthermore, it was identified that the accuracy of the model reduces a little when the leak location is more than 10,000 feet from the inlet section.
- Therefore, in future work, we plan to collect data points from a wide variety of experimental, modelling, and independent literature to train and validate the non-dimensional model.



Nomenclature:

m	Mass flow rate
f	Volume fraction
q	Volume flow rate
P	Pressure
dP	Pressure difference
ΔL	Length increment
ρ	Density
C_d	Leak coefficient
A	Cross-sectional area
D	Diameter
D	Pipe diameter
L	Pipe length
cL	Volume fraction of liquid
μ	Viscosity
$\Delta\rho$	Density difference between the inlet and outlet section
Δm	Change in mass flow rate between the inlet and outlet section
μ	Viscosity
Π	Non-dimensional parameter

Subscripts

t	Total
g	Gas
L	Liquid
in	Inlet
out	Outlet
$leak$	Leak
sur	Surrounding
m	Mixture

Relevant References:

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Safety and Security Impact of Emerging Technologies

How standards address the needs of owner operators

2023 MKORSE Conference

Speaker profile

- Howard Elton
 - BSChE University of Houston
 - Process Control, Automation, SIS, Instrument Systems, across a broad range of industries and process technologies (as an end user)
 - Now consulting with ProLytX as a Principal Technical Consultant for Functional Safety.





Dominant Themes in Industrial Control

- Wireless Everything
- “Levels” Are History - No More Purdue Models
- More Data from Everything – Right Now, and..
- Data Must Flow Freely In Every Direction - Everything Open And Common
- More Data From The SIS
- Ethernet Only – no proprietary networks
- Smart Everything – People??



Objectives of this Presentation

- Describe the nature of these emerging technologies
- Unpack the issues, challenges, and opportunities
- How Standards/Committees are addressing these issues

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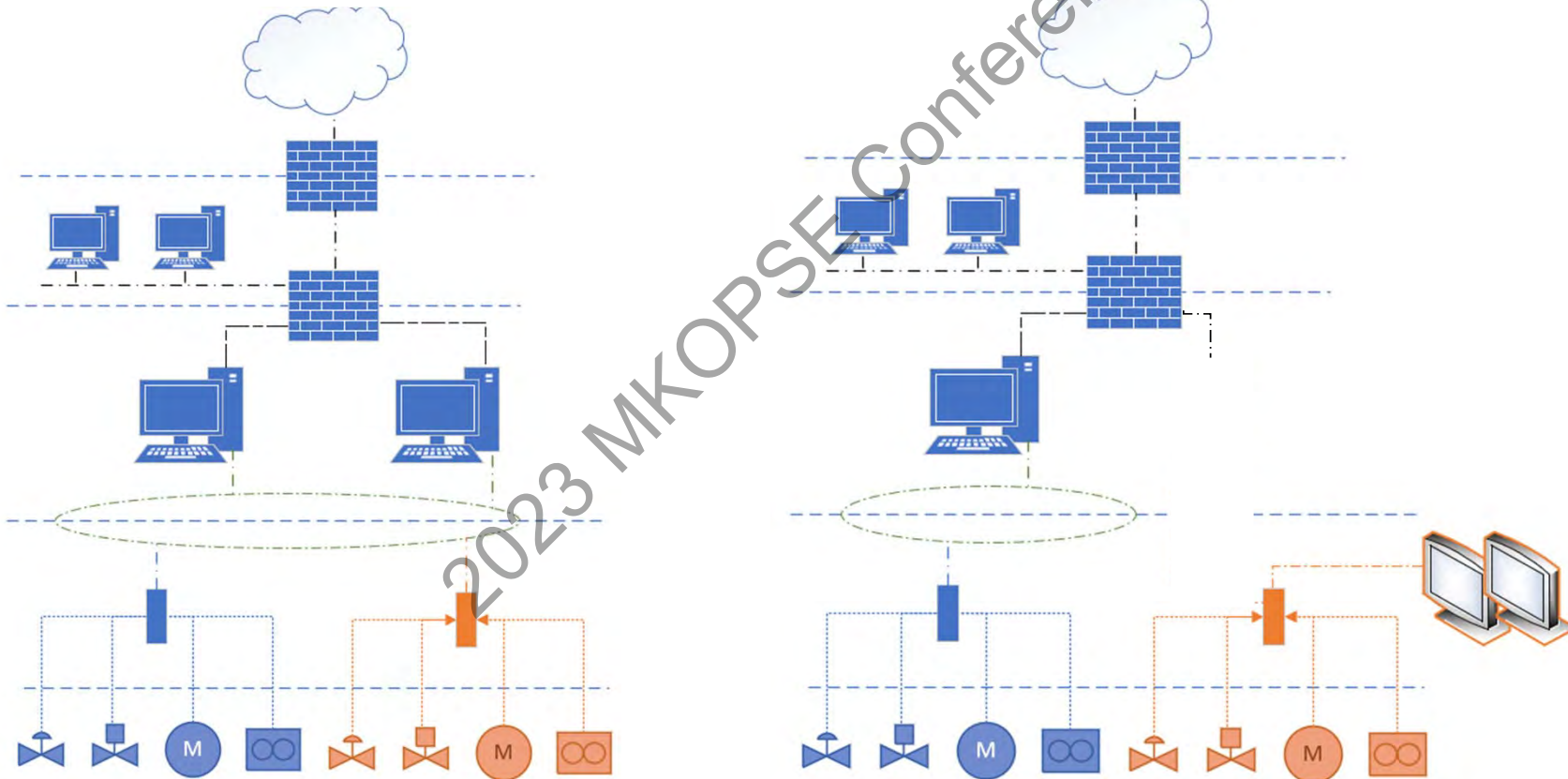
Emerging Technologies in Industrial Controls

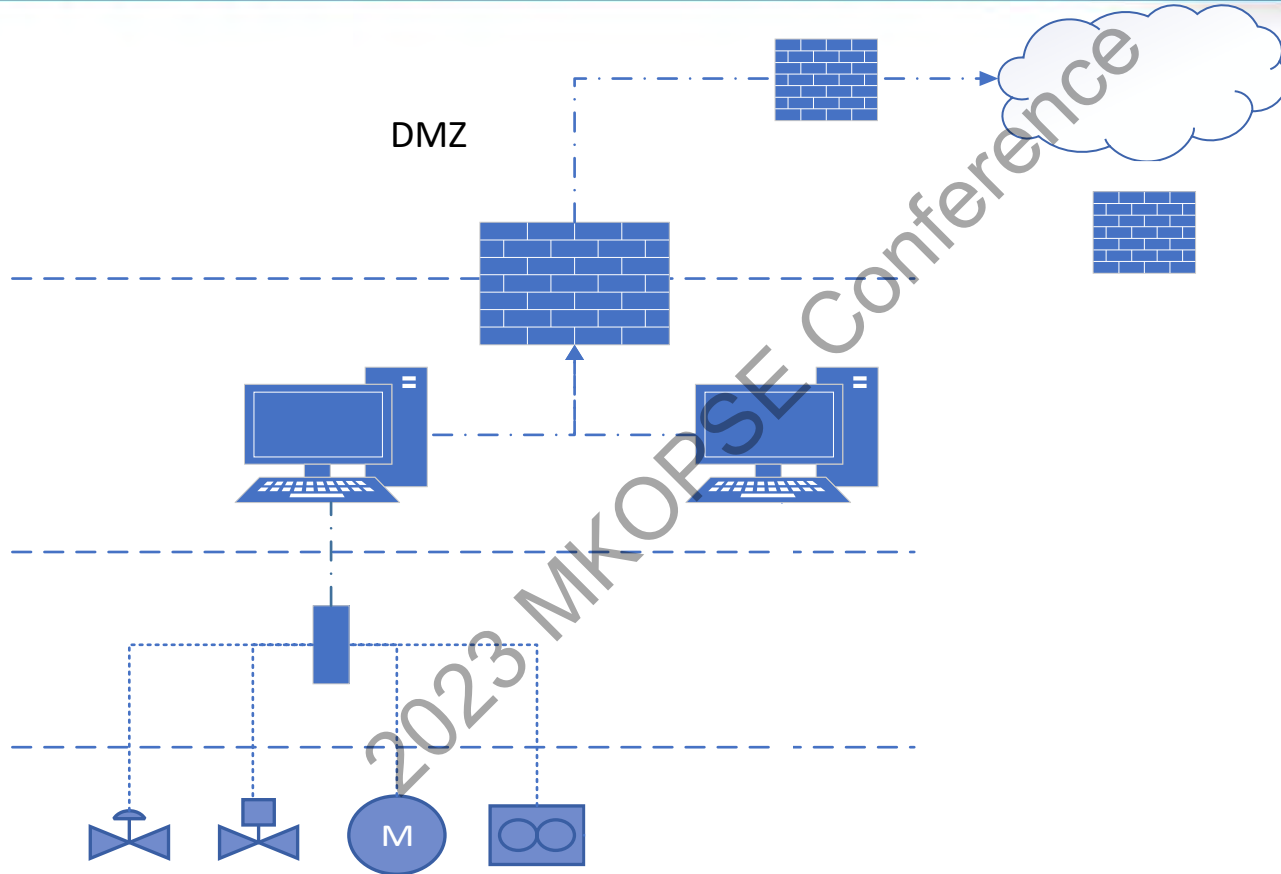


SIS Performance Management
And Data Analysis
WG10



The "Open Future" - Issues facing Owner/Operators



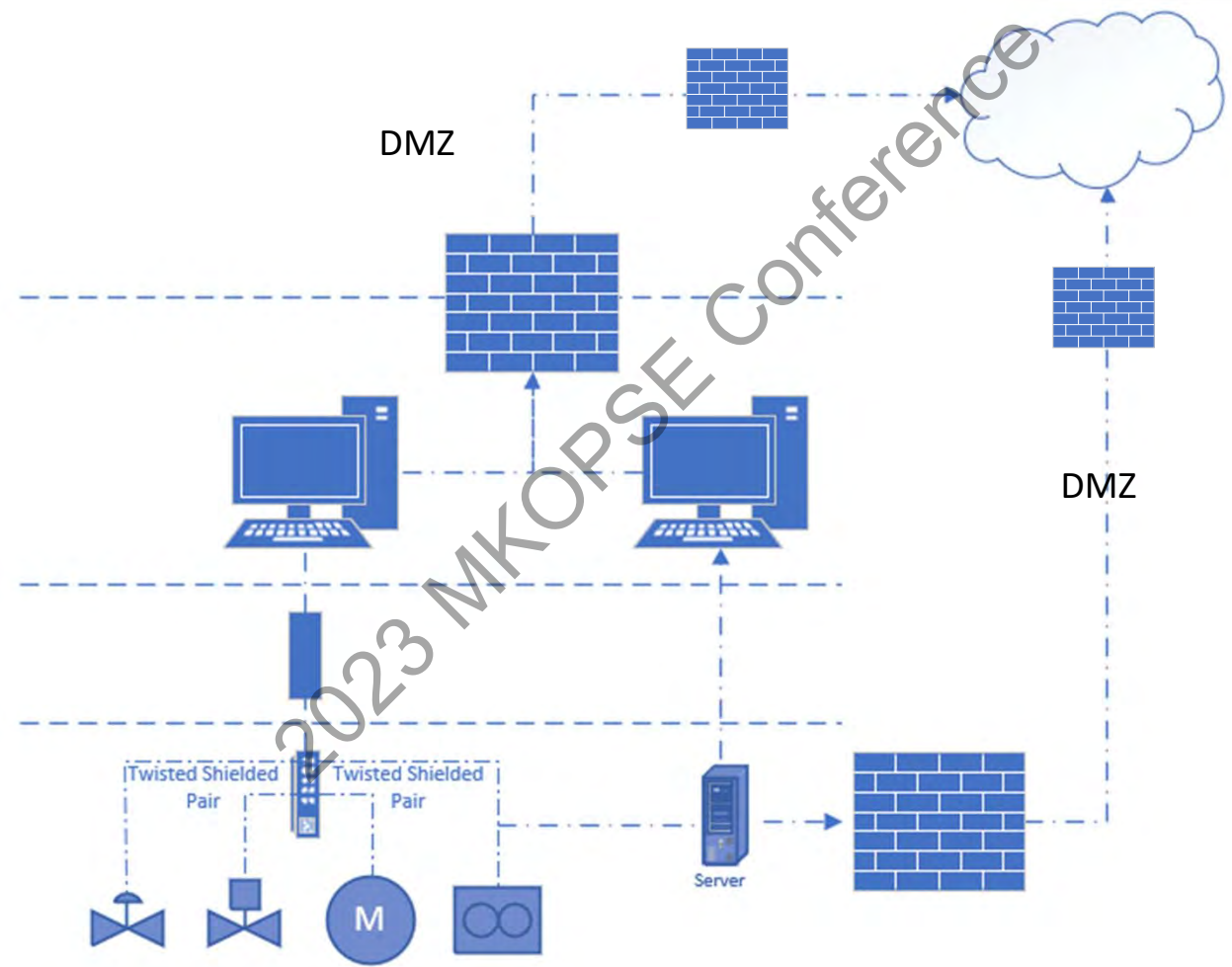


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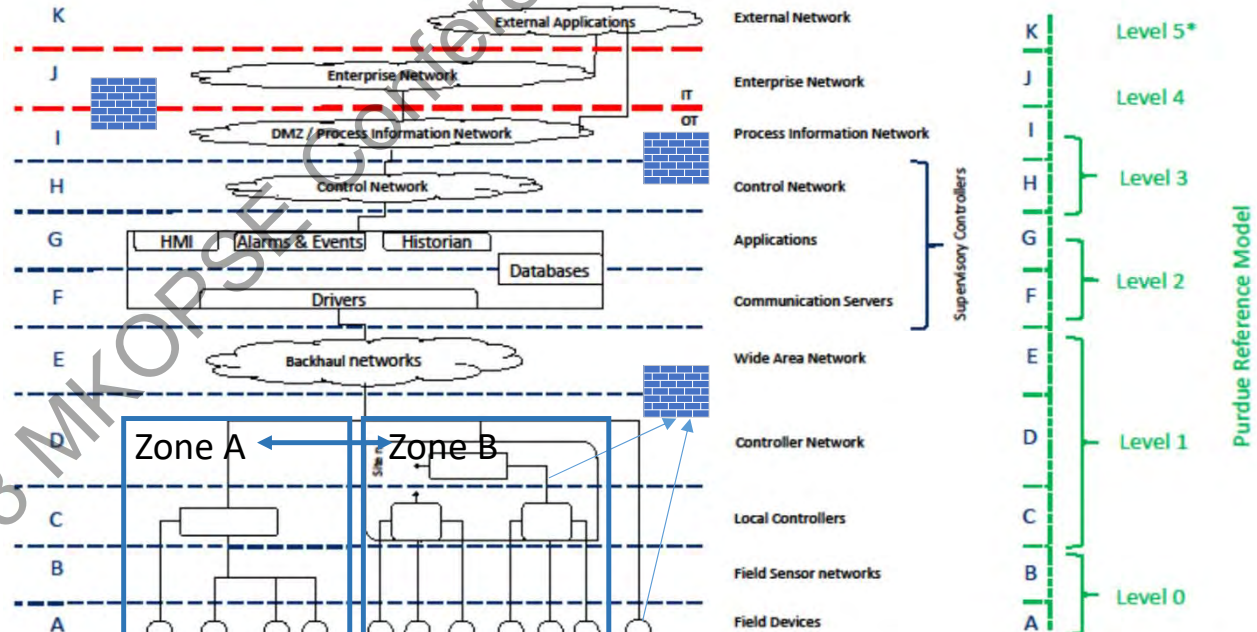
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Impact to Cybersecurity

- Purdue or not Purdue
- Functional Model is timeless and indispensable
- Cyber now lives at all levels, embedded

ISA112 SCADA System Model Architecture Diagram
 ISA112 – SCADA Systems Standards Committee – International Society of Automation (ISA) – www.isa.org/isa112/



Notes:

- Letters are used to avoid potential conflict with ISA-95 and other "Layer" models.
- Routers and Firewalls between layers as well as other system-specific servers, applications, and workstations are not shown.
- Individual architectures may vary from the above general model. For example, if only local systems are used Level E may not be required.
- Communications for any remote-hosted external applications (Cloud) with lower levels must be done using extreme care.
- The use of direct-connections for remote applications is strongly discouraged. Refer to ISA/IEC-62443 for guidance on an appropriate zone/conduit implementation.
- * We show a Purdue Level 5. The true Purdue Model only has levels 0-4 because it did not anticipate external applications.

IT = Information Technology
 OT = Operational Technology

Note: This is an interim working draft from the ISA112 SCADA Systems standards committee, as of 2022-01-26. (A previous version was posted on 2020-06-15). This diagram is still subject to change.



Impact to Programs, Policy and Organization

ISA61511
TüV – Exida
Certifications
Functional Safety
Policy

ISA62443
Cyber Policy
Training and
Certifications

ISA108
Intelligent Device
Management
Policy, Practice

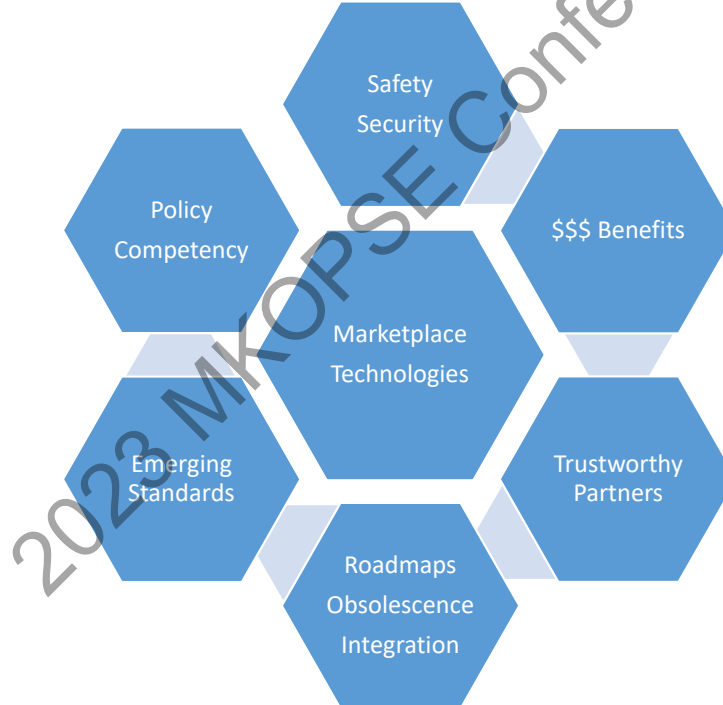
System Lifecycle Planning
Digital Transformation
Industry 4.0 Roadmap



Converging Standards

- ISA 108
- Namur and FieldComm Group/ODVA/IEEE
- OPAF
- OPC Group
- ISA84 Working Groups 9 & 10
- ISA112
- ISA62443 Cybersecurity Standards

Key Issues Presented to Owner Operators





Question and Comments



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Swiss Cheese Why the Holes Line Up?

Rajender Dahiya, CSP, MICHemE
Professional Process Safety Engineer
Energy Risk Consulting
AIG

26th Process Safety International Symposium

About Rajender

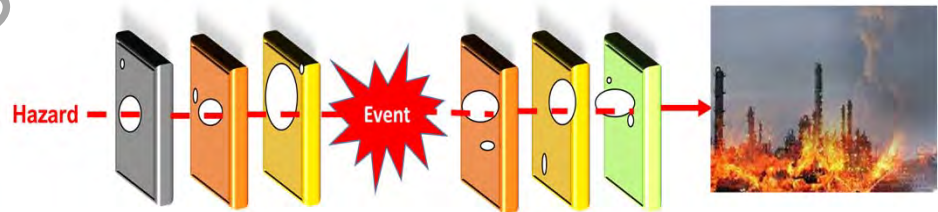
- >28 years experience in Oil, Chemicals, Insurance
- Expertise – Process safety, fire protection and risk management
- Professional Qualifications, Certifications
 - B. Sc, BE – Fire Engineering
 - Professional Process Safety Engineer (PPSE) – IChemE UK
 - Certified Safety Professional (CSP) – BCSP USA
- Membership
 - MIChemE
 - Sr. Member – AIChE
 - Professional Member – ASSP
- Presenting in national and local conferences
 - AIChE-GCPS, MKOPSC (Texas A&M) ASSP, CSSE....
- Volunteering
 - Subcommittee member – Peer Reviewer, Published 4 books recently – AIChE
 - *A yoga and meditation volunteer teacher*



Rajender Dahiya, CSP, MIChemE
Professional Process Safety Engineer
Energy Risk Consulting
AIG

Context

- We know that all incidents are preventable
- But major incidents keep occurring
- Causes and consequences are comparable
- This means...
 - there are problems, and
 - each problem has its solution
- So...It is simple
 - either we do not know the problem
 - or it is not getting fixed



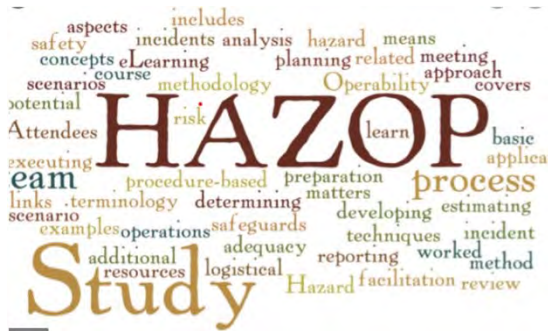


Root Causes of Incidents

Management failure to identify the hazard and manage risk	Hazard Identification and Risk Assessment (HIRA)
Management failure to maintain the integrity and availability of safety critical systems	Operating and Maintenance Programs
Management failure to learn from incidents	Learning from Incidents

What we normally do

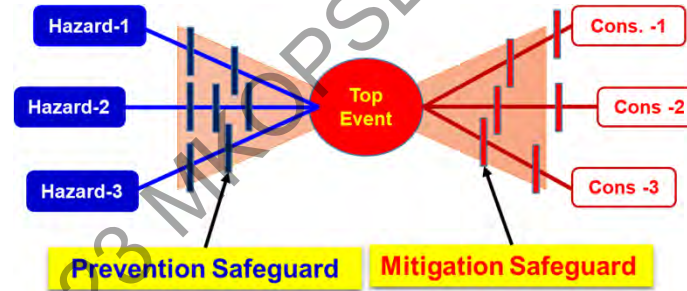
✓ HIRA done
(HAZID, PHA, LOPA.....)



Source: [CCPS - Center for Chemical Process Safety](https://www.ccps.org/)

HAZID: Hazard Identification
PHA: Process hazard analysis
HIRA: Hazard identification and risk assessment
HAZOP: Hazard & Operability Study
LOPA: Layers of Protection Analysis

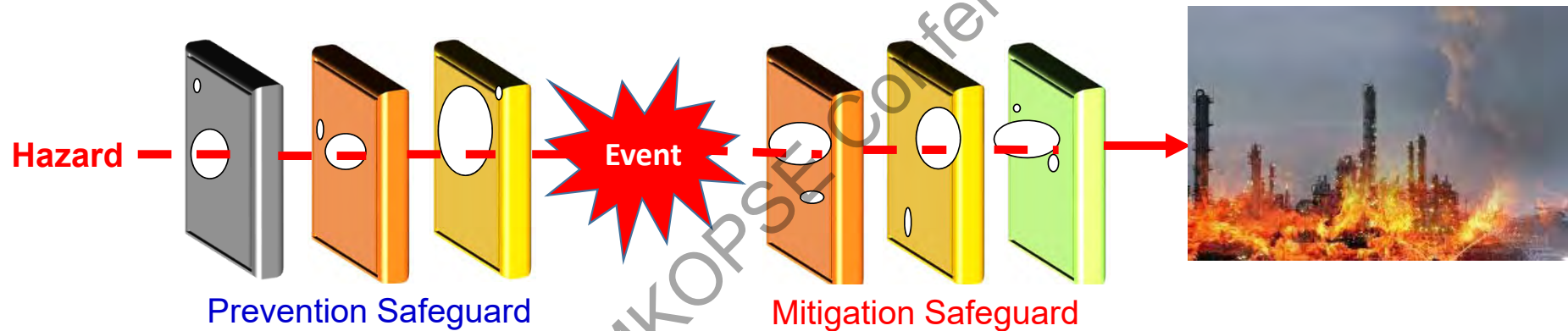
✓ multiple safeguards
installed



✓ management systems in
place

- Corporate Policies Standards
- Design Standards
- Inspection & Maintenance
- Operating Procedures
- Emergency Response
- Training Competency Culture
- KPIs Audit

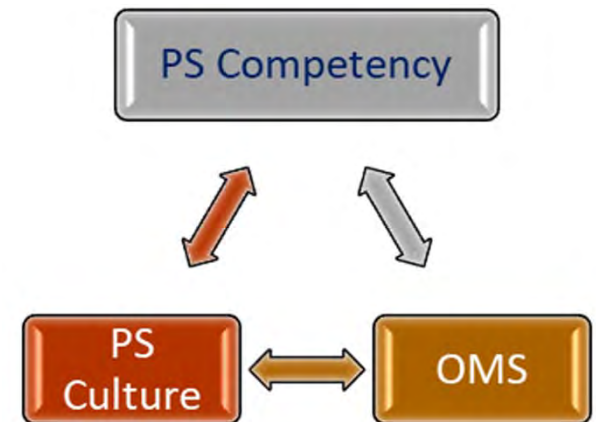
Holes Developed & Aligned – Incident



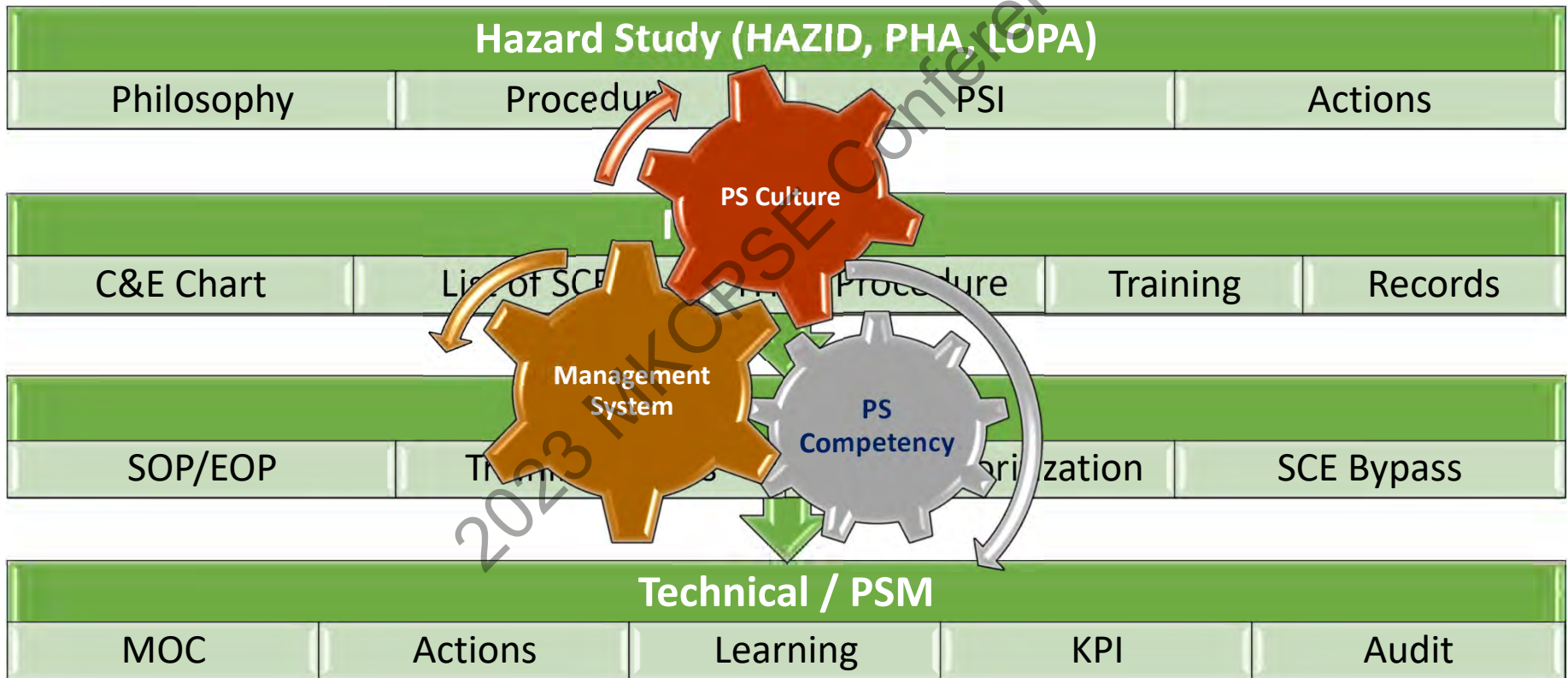
- The holes depicts MS weaknesses
- Several warning signs, weak signals, near misses, small incidents may have been neglected or not addressed adequately

Most Common Causes / Gaps

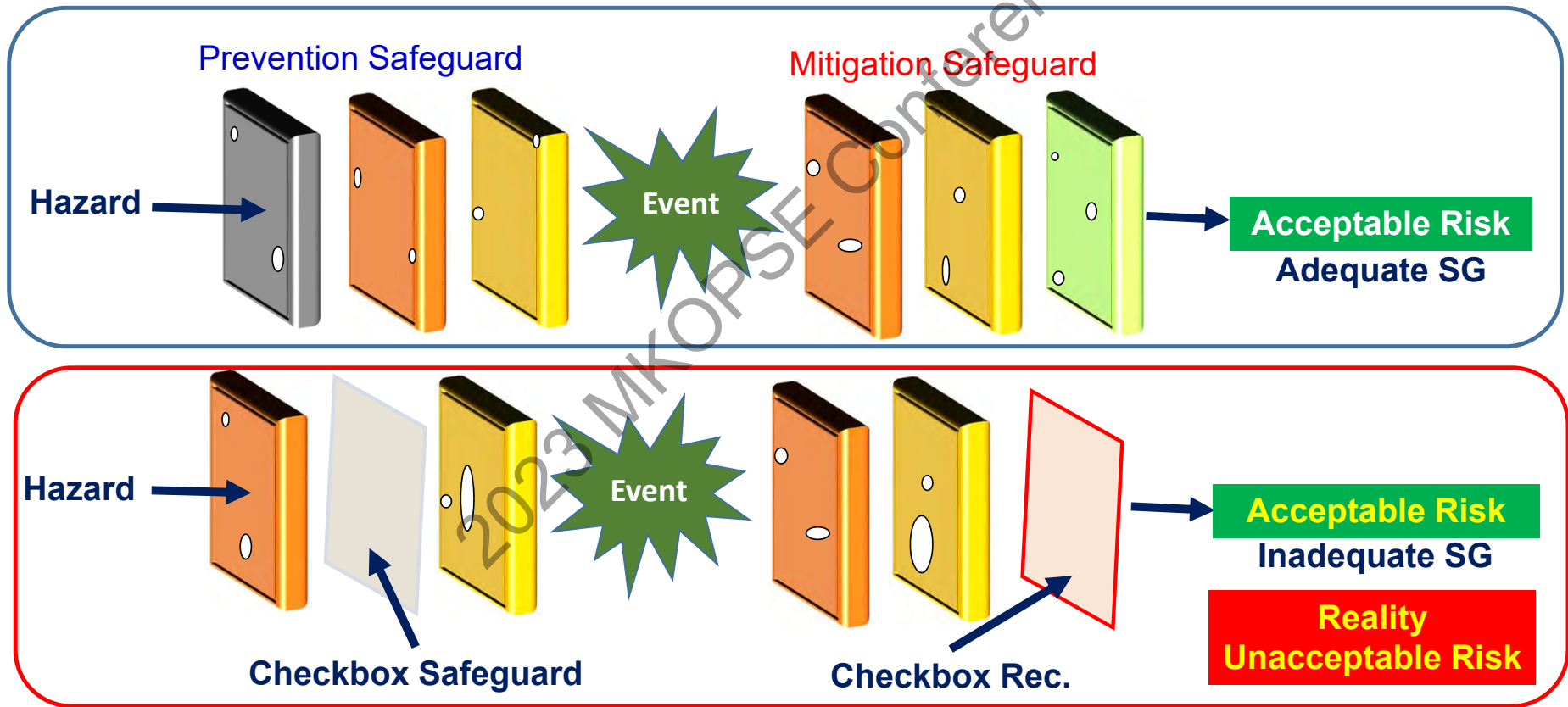
- HIRA
- Actions Management
- Inspection Testing and Preventive maintenance (ITPM)
- Operator procedures and training
- Safety system bypass
- Incident investigation and learning
- Key Performance Indicators (KPIs)
- Audit



Journey – How the Holes are Created and



HIRA Quality – Good vs. Poor

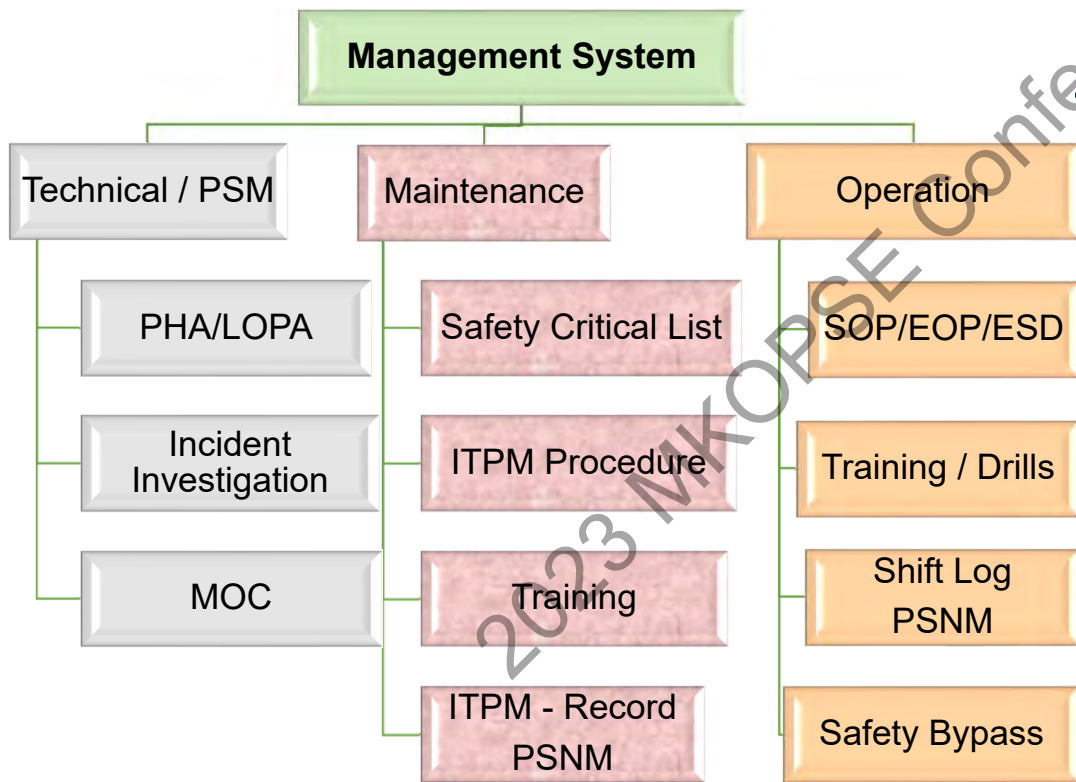


Operation Stage



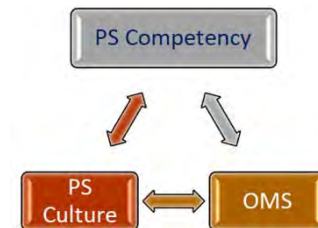
Knowingly or Unknowingly the plant is operated with UNACCEPTABLE risk

Management System Weakness - Example

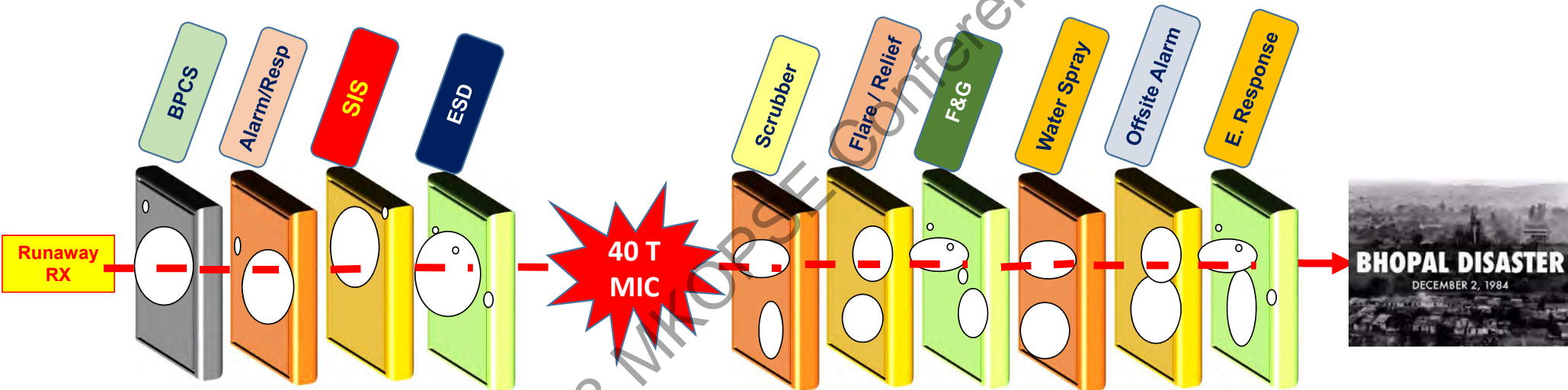


NS 001 IN SERVC P-01	HS 002 IN SERVC P-02	HS 003 IN SERVC P-03
TI 001 IN SERVC V-01	TI 002 OUT SVC V-02	TI 003 IN SERVC V-03

- Program Audit
- Key Performance Indicator



Bhopal Incident (1984) – What is Different Now?



- Several precursors, neglected
- Leaders, managers, employees, union, public, media were aware about this risk

Truth
None of these 10 Safeguards Failed

Anything different now?
Similar gaps causing an incident

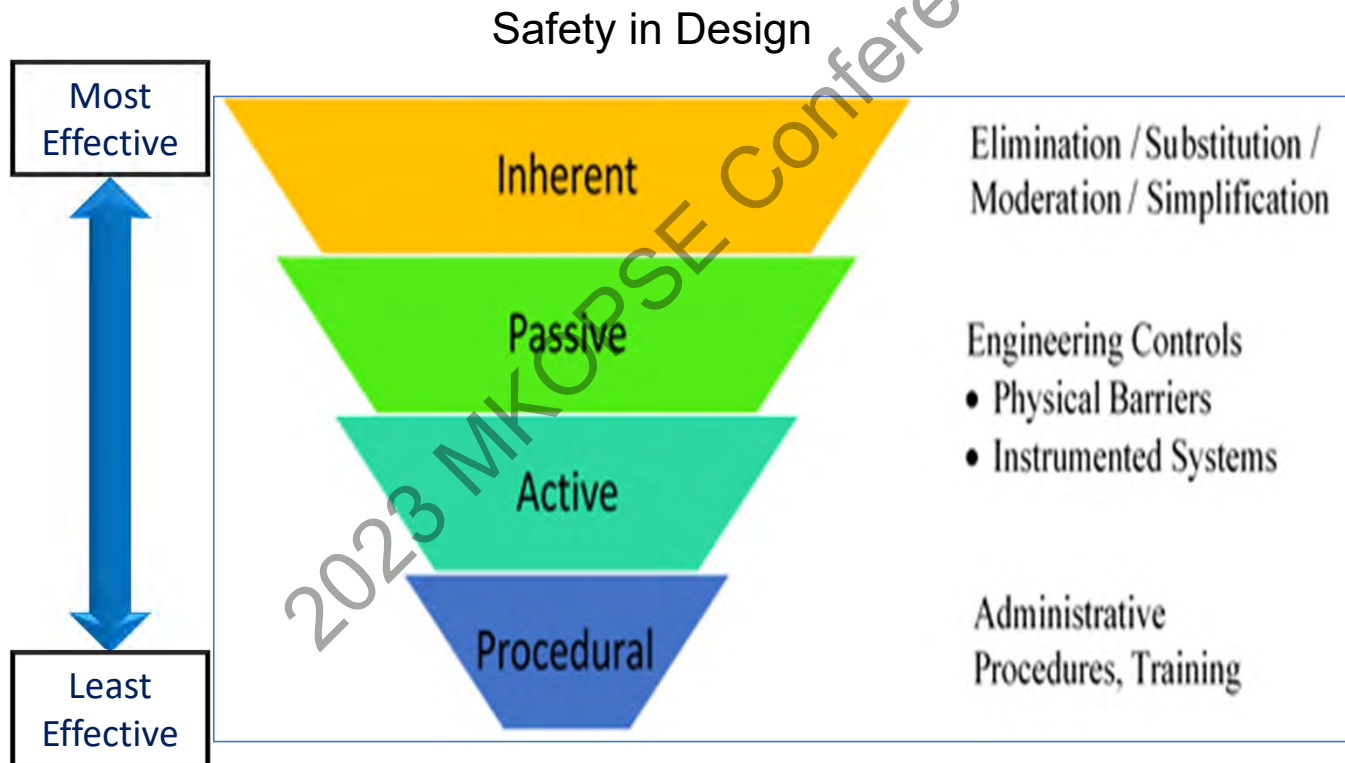


Next Step

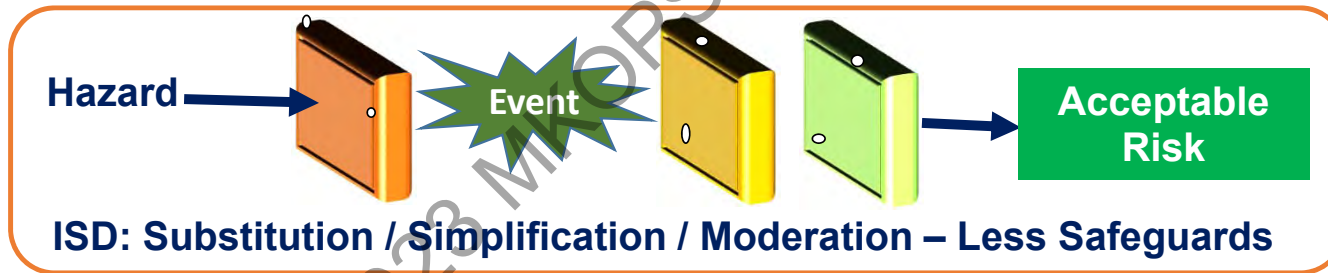
Proactive
&
Reactive

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Hierarchy of Process Risk Management (CCPS)

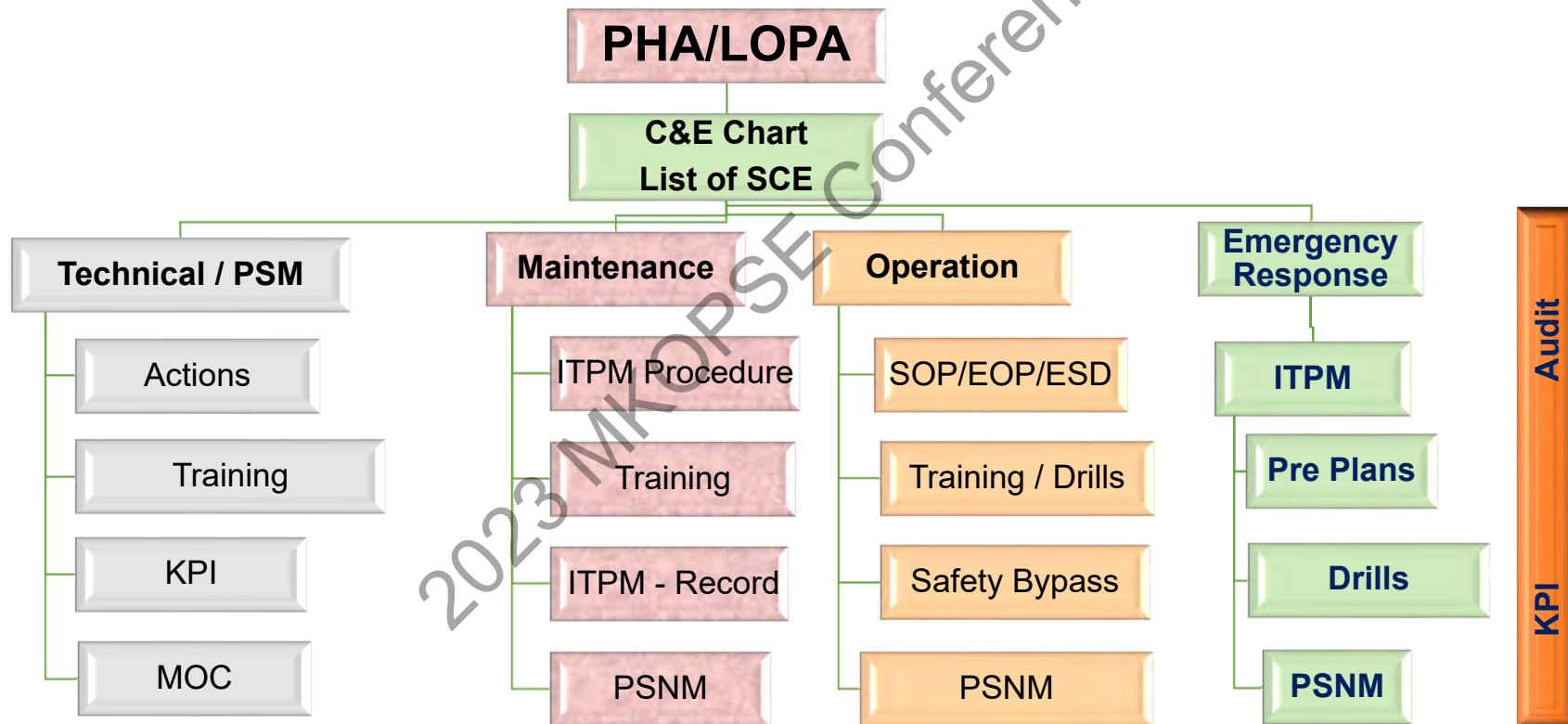


Industry Practices vs Industry Best Practices





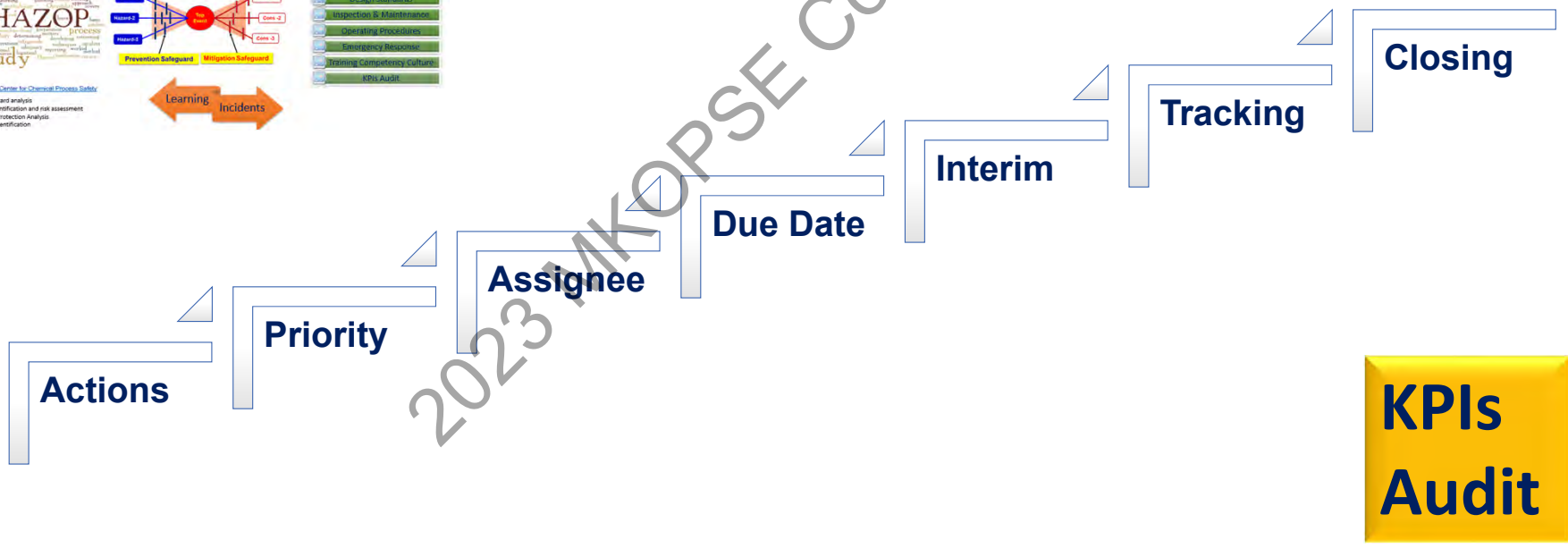
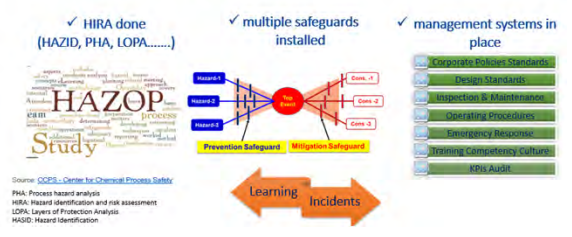
Integrity & Availability – Best Practices





Actions Management – Gaps & Best Practices

What we normally do



Learning from Incidents

- Defined / reported / KPIs
- Walk the talk, meeting

- Potential consequences
- Real root causes

- Rec. address the root causes

- Action priority, review and verification

- One pager
- Company wide



- Not defined / reported

- Actual consequences
- Not to the root cause

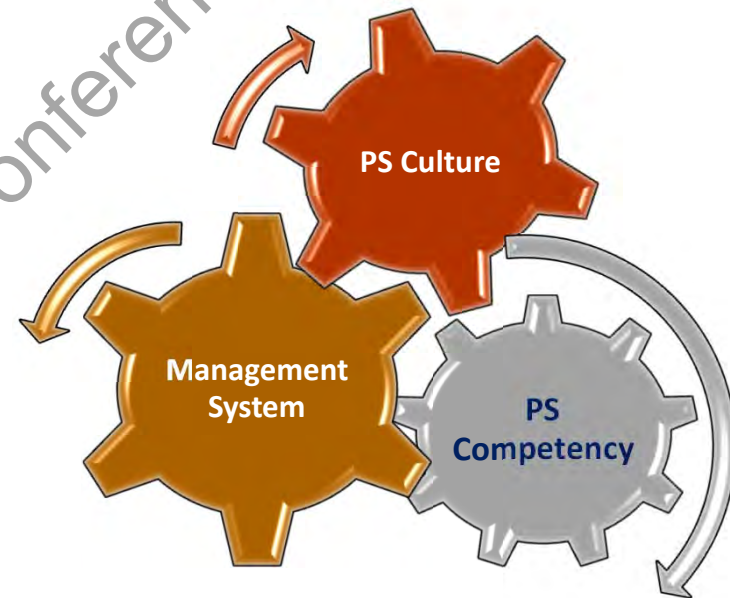
- Generic, easy to fix

- Not trackable

- Local fix

What Matters..... Learning & Takeaway

- Quality
- Consistency
- User friendly
- Simplicity
- Fit for purpose
- KPIs Audit



Corporate

Design

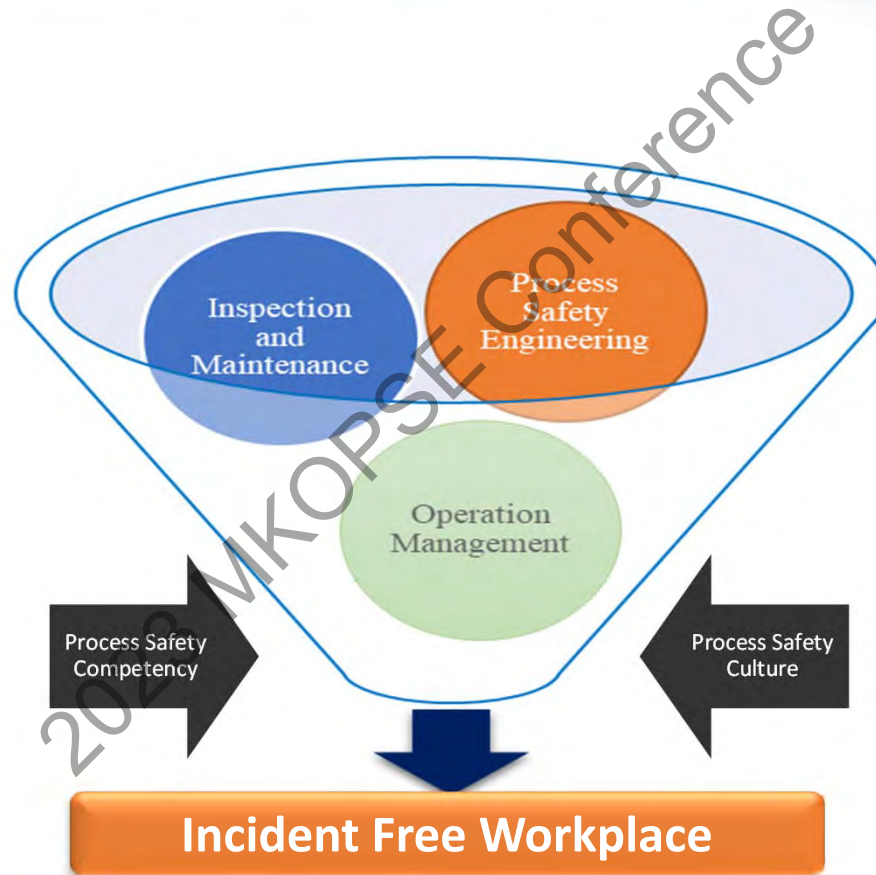
Operation



Summary

- FACT All incidents are preventable, but incidents keep repeating with severe consequences
- We know that whatever may be the causes, if hazard is identified and multiple safety systems work as designed, then the catastrophe could be avoided altogether, or be much less severe consequences
- Root causes of process incidents are deep rooted in the company's operating management systems, corporate process safety culture and competency of the employees – deep dive is MUST.
- Irrespective of the process hazards, the owner/operator is responsible for ensuring that safety critical equipment and systems are designed and maintained to prevent any accident – PSM covered or Not
- Process safety competency is more important for leaders than the employees.
- Inherently safer techniques are applicable for the facility lifecycle.
- Check Box Must Go Away

Conclusion



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Thank You

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Objective

- *Unlocking the Future of Control Systems, where precision meets uncertainty, and adaptability is paramount.*
- *Augmentation of safety-critical decision making with systems-based real-time operation to proactively reduce process safety losses.*

Challenges

Dynamic Environments | Uncertainty | Struggles of conventional control

Risk-Informed Model Predictive Control (R-MPC)

- **Bayesian-informed Control:** *Bayesian updates to leverage uncertainty as an asset, enhancing control system adaptability*
- **Real-Time Tolerance adjustment:** *Allowing control system to adjust tolerances in response to changing conditions, ensuring resilience and responsiveness*
- **Safety-centric strategy:** *Prioritizing safety and performance by actively monitoring and managing risk throughout the system operation*

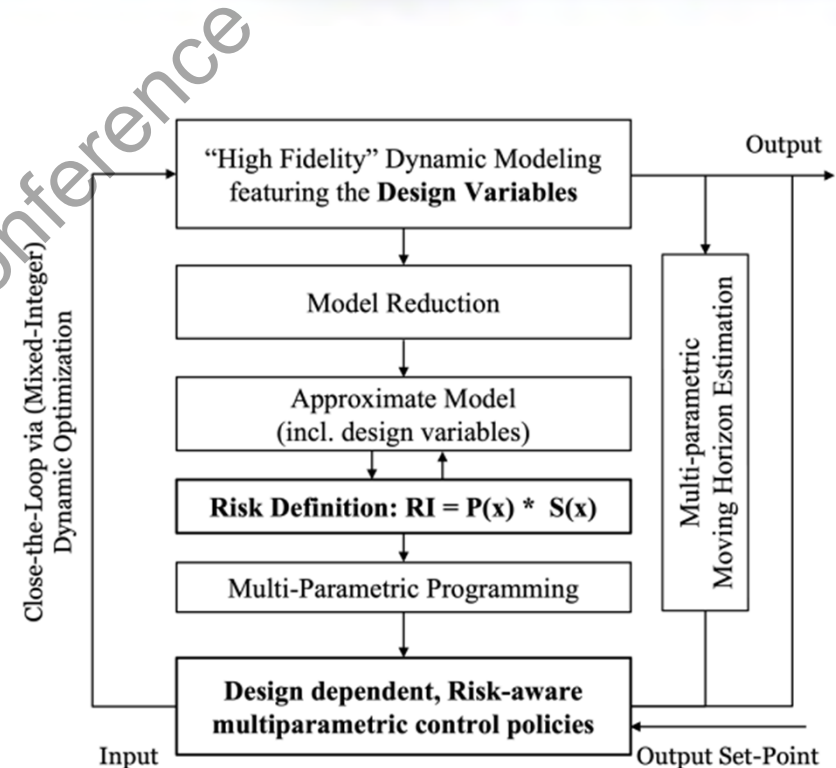
Literature Review

The inspiration for this work was drawn from:

“Ali, M., Cai, X., Khan, F. I., Pistikopoulos, E. N., & Tian, Y. (2023). Dynamic risk-based process design and operational optimization via multi-parametric programming. Digital Chemical Engineering, 7, 100096”

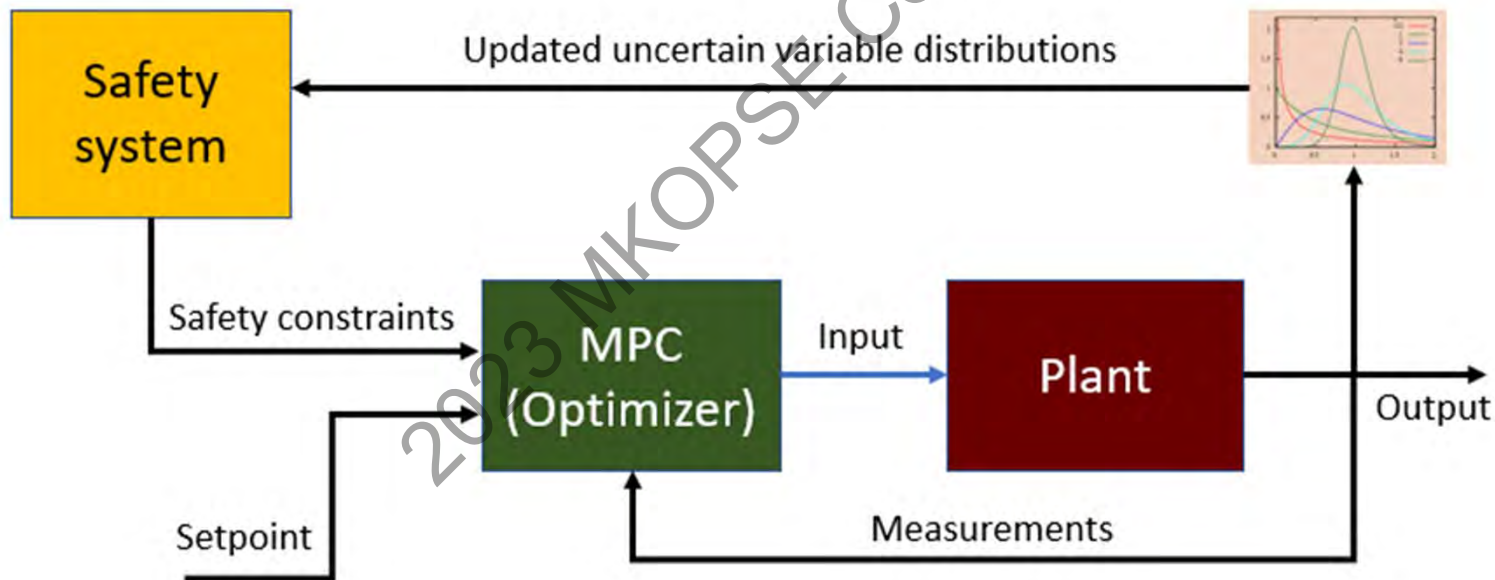
The proposed framework by the authors in this work includes:

- High-fidelity modelling of process and safety system
- Dynamic risk modelling as functions of process variables
- Design-dependent risk-aware control policies via multi-parametric policies

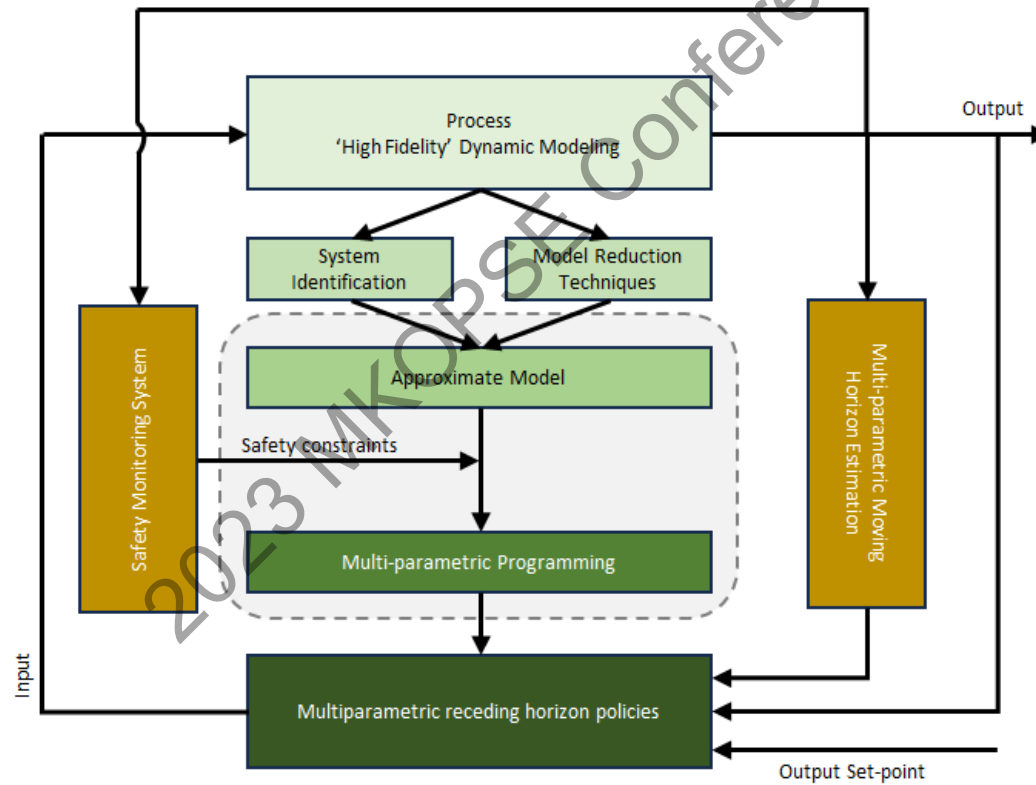


Research Objectives

The primary objective of this project is to design a controller that prioritizes the **probabilistic nature of risk**, employing **Bayesian inference methods for continuous risk updates within a rolling time horizon**, all while operating within a chance-constrained programming framework.



PAROC Framework



Formulation

$$\min J = x_N^T P x_N + \underbrace{\sum_{k=1}^{OH-1} (y_k - y_k^R)^T Q R_k (y_k - y_k^R)}_{\text{Control losses}} + \underbrace{\sum_{k=1}^{CH-1} (u_k - u_k^R)^T R_k (u_k - u_k^R)}_{\text{Safety losses}} + f(x_k)$$

s.t. $x_{k+1} = A x_k + B u_k + C [d_k; De]$ } Linear process model

$y_k = D x_k + E u_k$

$\Pr(a^T x_k \geq T) \leq \beta_k$ Violation-allowance constraint (risk)

$\underline{x} \leq x_k \leq \bar{x}; \underline{y} \leq y_k \leq \bar{y}; \underline{u} \leq u_k \leq \bar{u}; \underline{De} \leq De_k \leq \bar{De}$ Process bounds

$\beta_{k+1} = L(x_k, x_{k-1}, x_{k-2}, \dots, x_0) * \beta_k$ Bayesian update step

Where T is the maximum limit for violation of the constraint, L is the likelihood function for Bayesian update

Chance-constrained Programming

- Probability constraints in the optimization framework are converted to their deterministic approximates via chance-constrained programming.
- Only Gaussian probability distributions are considered in the current scope of applications.
- Deterministically approximated via reliability index methodology.

Probabilistic constraint

$$\Pr(a^T x_k \geq T) \leq \beta_k$$



Deterministic approximate

$$a^T x_k \geq T + z \cdot \sigma$$

Where,

- z is the reliability index calculated from the inverse cumulative distribution ($z = \varphi^{-1}(\beta_k)$)
- σ is the standard deviation associated with the probability distribution observed in the uncertainties.

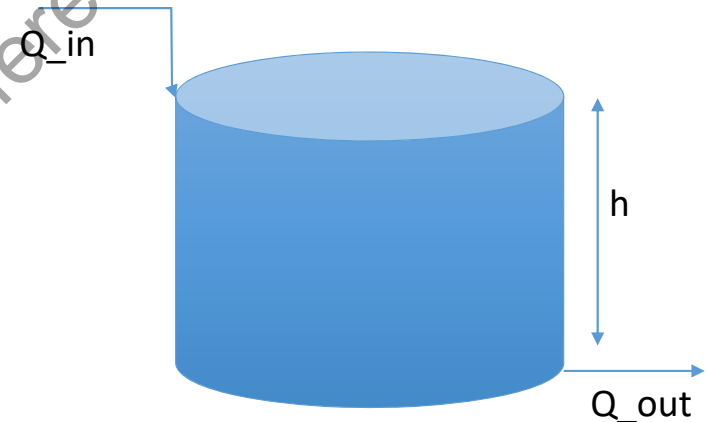
Case-study: Tank level control

Objective:

Control the level of the tank while adapting to changing levels of uncertainty in real-time

$$\frac{dh}{dt} = \frac{Q_{in} - Q_{out}}{A}$$

$$Q_{out} = k * h$$



State Space Model	
State Variables	Level in the tank (h)
Input Variable	Q_{in}
Disturbance	Uncertainty (w)
Design	Cross-sectional area (A)

Case-study: Formulation

$$\min J = \sum_{k=1}^{OH-1} (x_k - x_{sp})^2 + INLF(x_k)$$

$$h_{k+1} = \left(1 - \frac{kT_s}{A}\right) h_k + \left(\frac{T_s}{A}\right) Q_{in_k} + \left(\frac{T_s}{A}\right) w_k$$

$$P(x_k \geq x_{max}) \leq \epsilon_t \rightarrow P((x_k - x_{max}) \geq 0) \leq \epsilon_t$$

$$0 \leq x_k \leq x_{max}$$

$$\min J = \sum_{k=1}^{OH-1} (x_k - x_{sp})^2 + INLF(x_k)$$

$$h_{k+1} = \left(1 - \frac{kT_s}{A}\right) h_k + \left(\frac{T_s}{A}\right) Q_{in_k} + \left(\frac{T_s}{A}\right) w_k$$

$$x_k \geq x_{max} + \varphi^{-1}(\epsilon_t) \cdot \sigma$$

$$0 \leq x_k \leq x_{max}$$

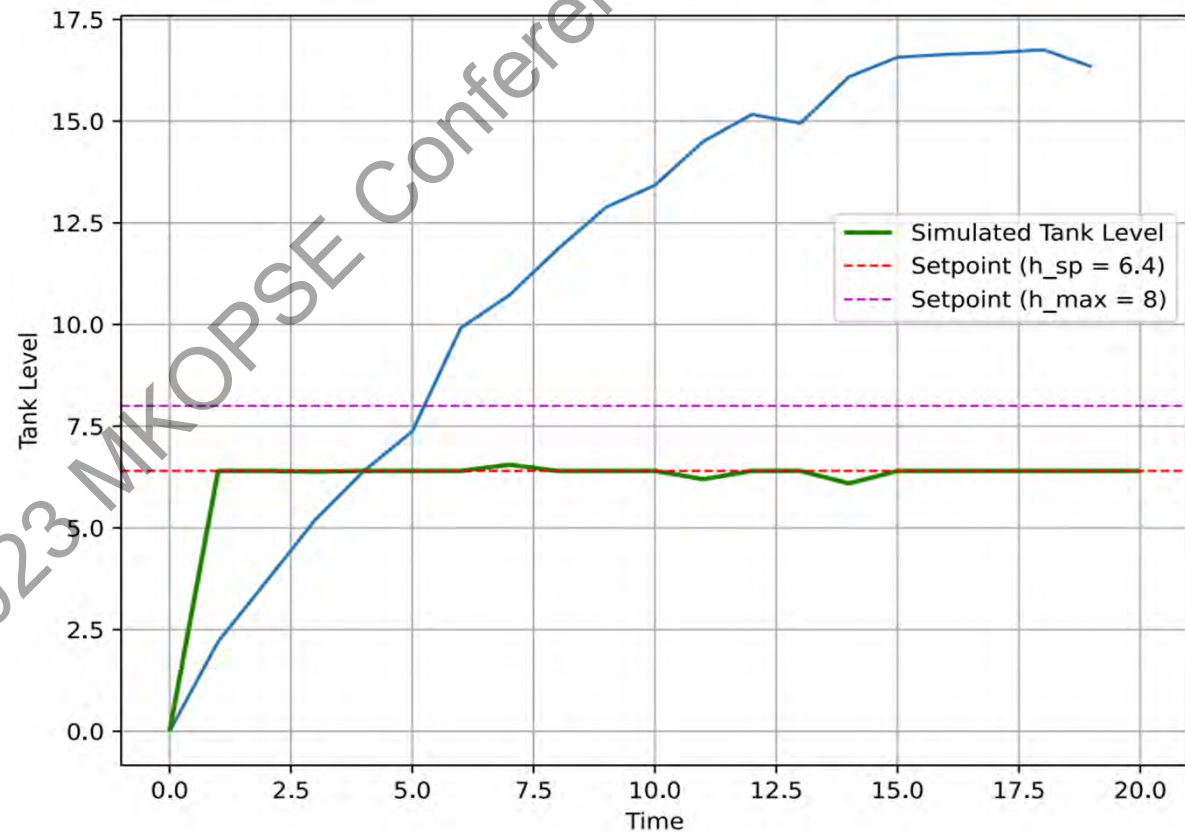
Updating probability tolerance on rolling horizon basis:

$$P((x_k - x_{max}) \geq 0)_{posterior} = L(x_k, x_{k-1}, x_{k-2}, \dots, x_0) \cdot P((x_k - x_{max}) \geq 0)_{prior}$$

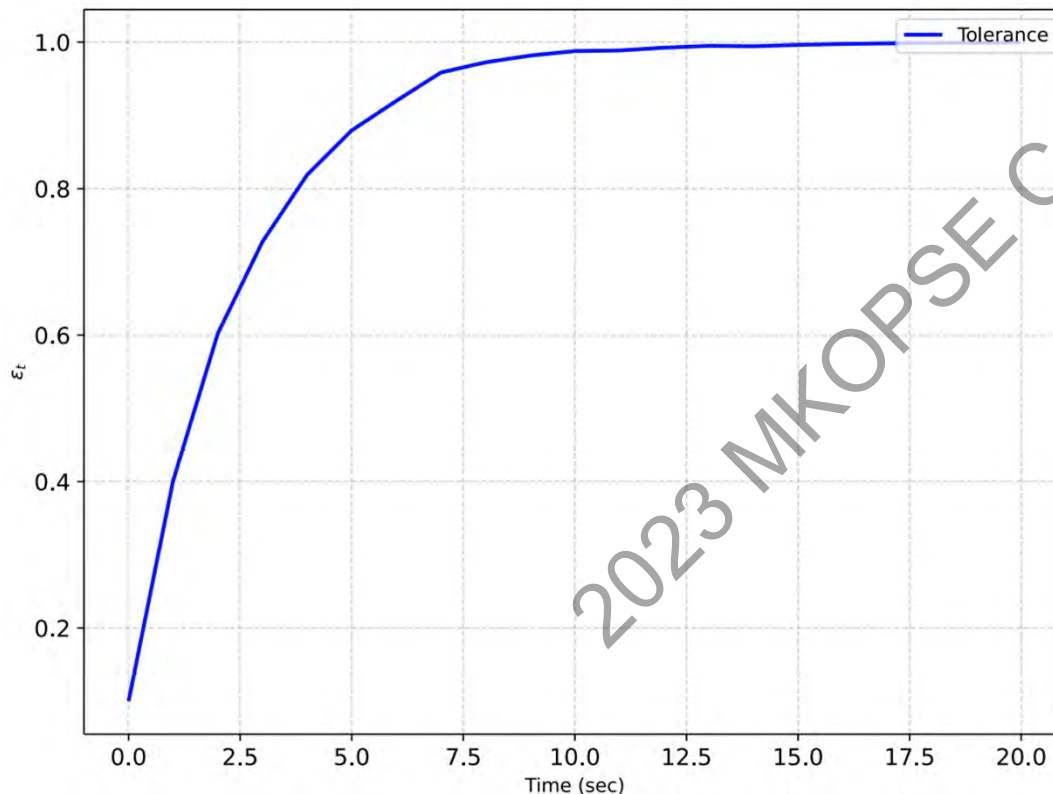
$$\epsilon_{t+1} = L(x_k, x_{k-1}, x_{k-2}, \dots, x_0) \cdot \epsilon_t$$

Results & Conclusions

- Level in the tank is being maintained with R-MPC by adjusting the input flowrate



Results & Conclusions



Permissive Constraint Approach:

The increasing epsilon trend reflects a deliberate move towards a more permissive constraint strategy, prioritizing system performance over strict constraint adherence.

Enhanced Adaptability:

The control system's increasing epsilon allows it to adapt more effectively to changing conditions, disturbances, and setpoint variations while managing the risk of occasional constraint violations.

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Thank you!

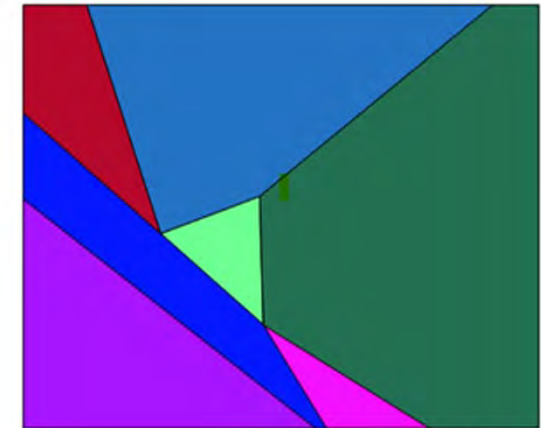
Additional slides: Multi-Parametric programming

$$z(\theta) = \min_x f(x, \theta)$$

$$\text{s.t.} \quad g(x, \theta) \leq 0$$

$$h(x, \theta) = 0$$

$$x^*(\theta) = \begin{cases} x^1(\theta), & \text{if } \theta \in CR1 \\ x^2(\theta), & \text{if } \theta \in CR2 \\ \vdots \\ x^v(\theta), & \text{if } \theta \in CRv \end{cases}$$



$\theta \in \theta$

2023 Mary Kay O'Connor Safety & Risk Conference

Safe and Sustainable Energy Transition

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October 11-13, 2023

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Hazard Recognition of Proton Exchange Membrane (PEM)
Hydrogen Production and Storage Installation

26th Process Safety International Symposium



Texas A&M Engineering Experiment Station

Mary Kay O'Connor
Process Safety Center

Speaker profile



- **Mohd Fadly Adnan** - Process Safety Staff Engineer/Manager at PETRONAS Group Technical Solution with 15 years experience in Oil and Gas sector.
- Providing process safety consultancy to PETRONAS Project and Operating Unit (OPU)/Asset.
- Experienced in LNG sector as Operation Lead Engineer (Process/Utility) and Technical Authority for Process Safety at Group Technical Solution (GTS) under Technical Delivery Excellence (TDEx).



Background

- Touted as Fuel of the future – Emerging green Hydrogen production facilities
- Inherent hazard needs to be recognized, assess, and mitigated
- PETRONAS H₂ project - safety analysis and hazard identification in a typical Proton Exchange Membrane (PEM) Hydrogen production/storage through qualitative (HAZID, HAZOP) and quantitative assessment (Dispersion Modelling) which influenced some of the design criteria consideration.

Recognizing inherent hazard of H₂

Flammability



Flammable range between 4% to 75% by volume in air



Minimum ignition energy (MIE) of 0.02 mJ, which is among the lowest compared to typical hydrocarbons.



Wide detonation range (20-65 vol%). High laminar burning velocity – deflagration, explosion

Behaviour



Small size of molecules – can easily leak, permeate through metal

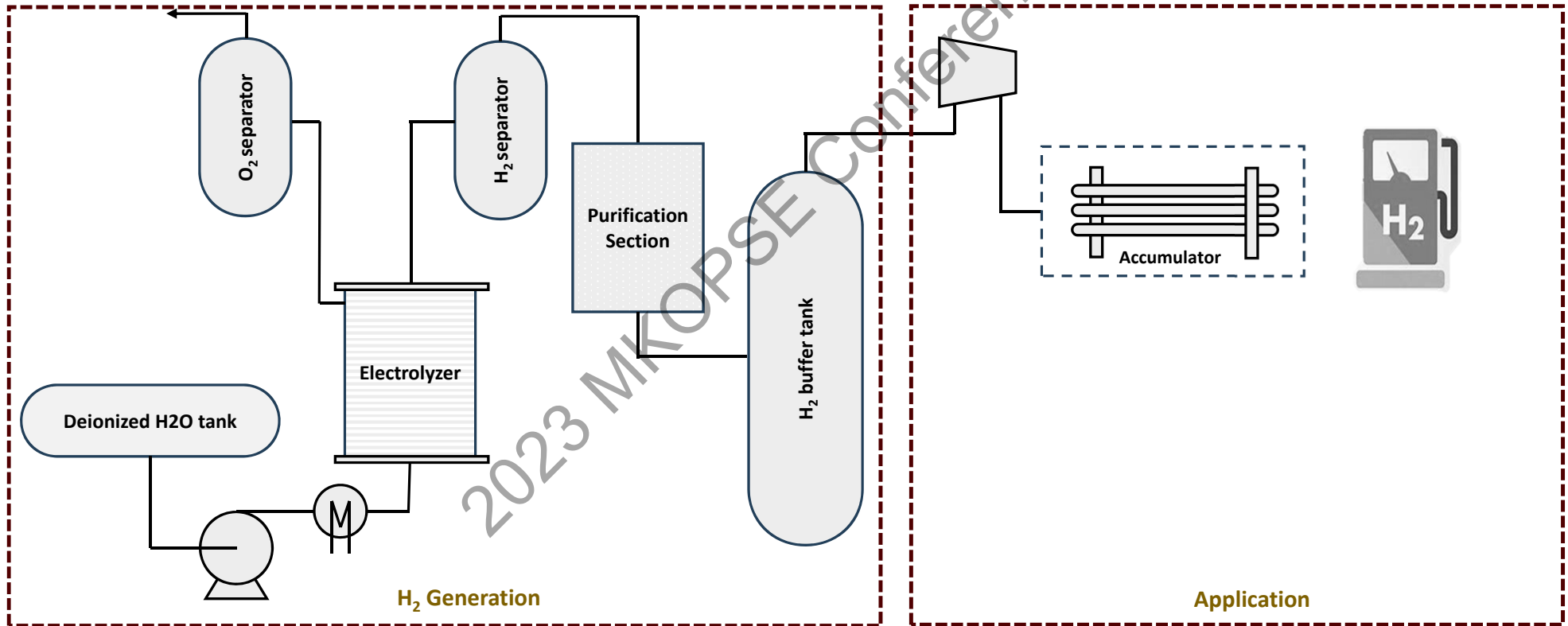


Fire almost invisible during daylight, can burn undetected

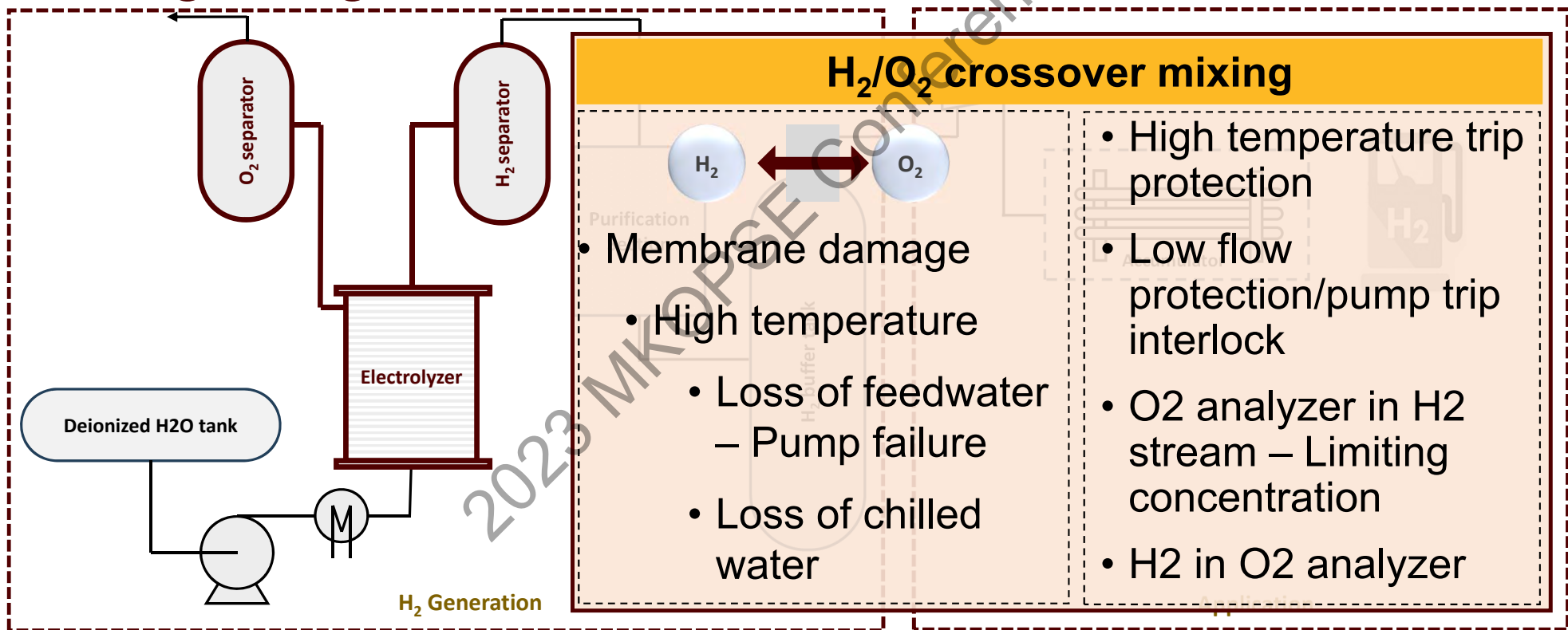


Buoyant nature – potential trapped at high point enclosure area

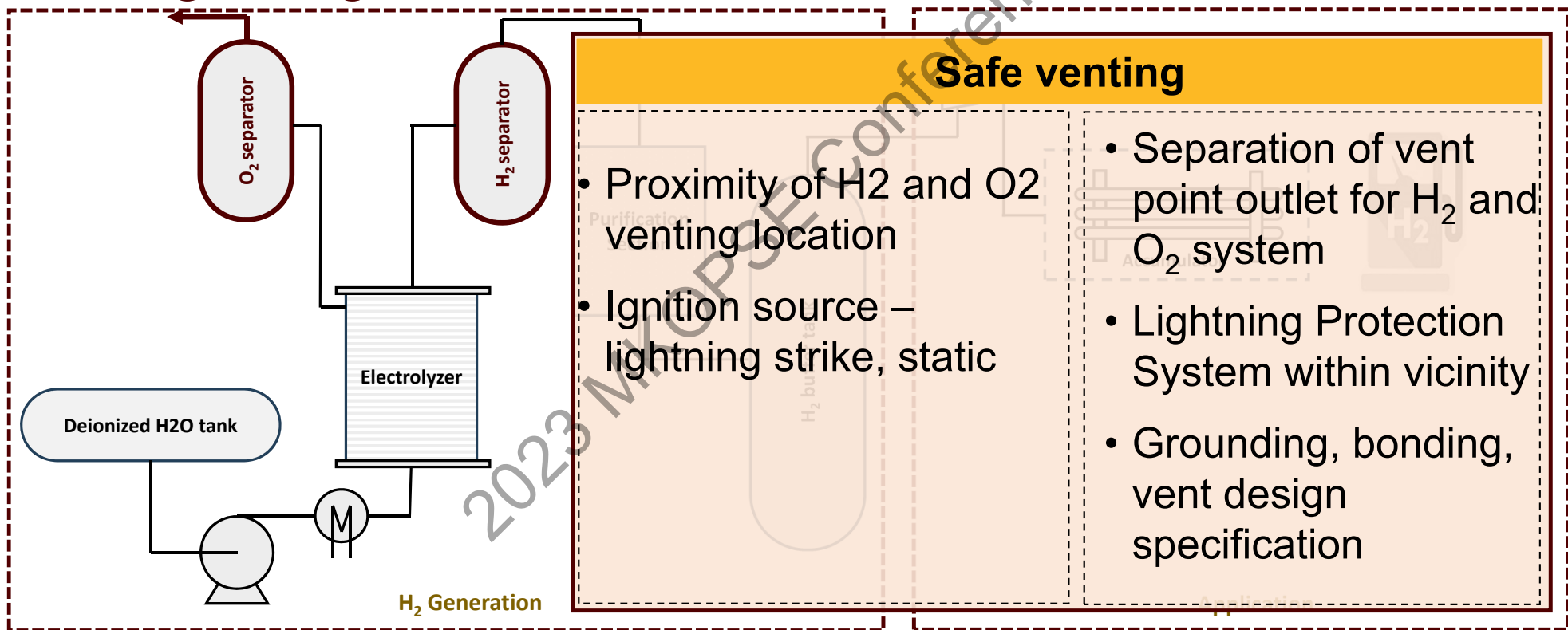
Recognizing component in typical H₂ electrolyzer



Recognizing threats - Qualitative



Recognizing threats - Qualitative



Recognizing threats - Qualitative

Failure of equipment integrity

- | | |
|--|--|
| <ul style="list-style-type: none">• Overpressure<ul style="list-style-type: none">• Blocked outlet of compressor, H₂ generator• Over temperature<ul style="list-style-type: none">• Failure of heating element in De-Oxo and Dryer | <ul style="list-style-type: none">• High pressure alarm and trip protection• Pressure Safety Valve (PSV)• High temperature trip protection |
|--|--|

Recognizing threats - Quantitative

Fire and explosion impact

- H₂ release – ventilation, early detection of gas/flame
- Jet Fire threat – Isolate and depressurize
- Sensitive receptor – Endurance time, fire/blast wall

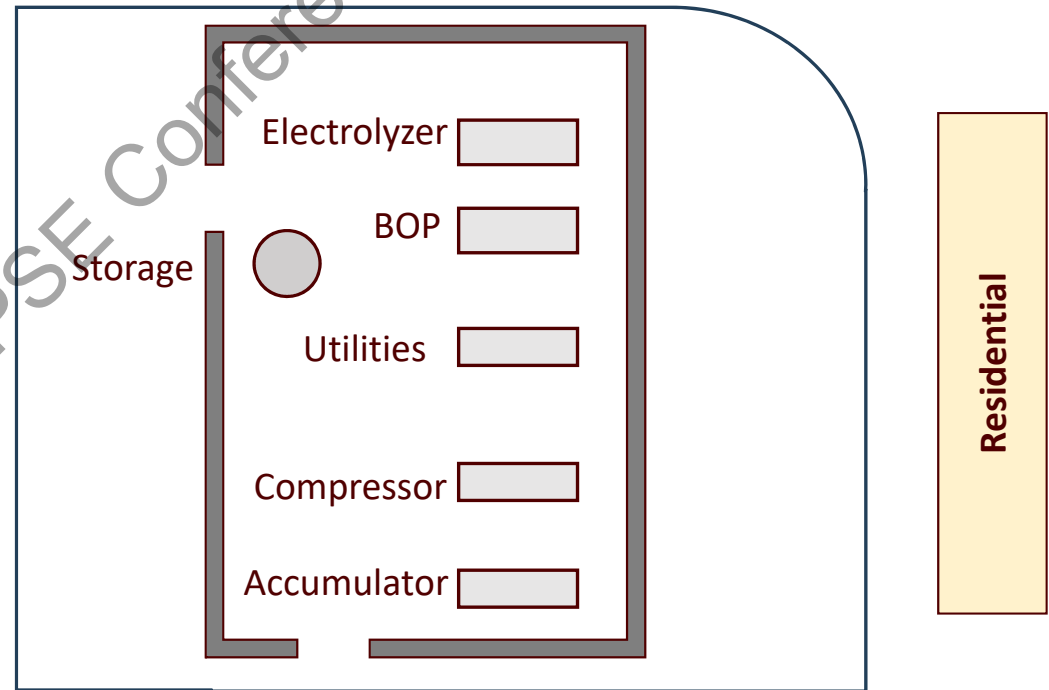
Key information output

- Jet flame length, thermal radiation and fire duration
- Unignited release radius
- Explosion radius and side-on peak overpressure

Recognizing threats – Case Study

Basis

- Highest pressure component – compressor (900 barg)
- Representative hole size (1% of flow area – 1" ID)*
- Inventory – 5 kg

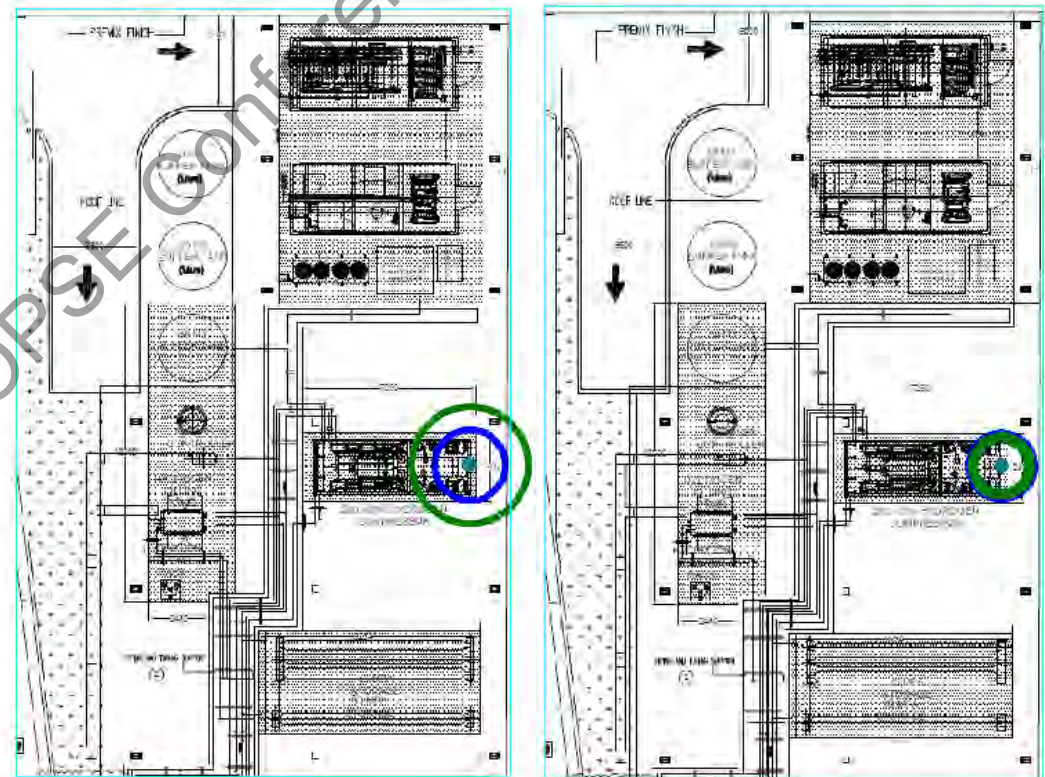


Site Layout Representation (not to be scaled)

*NFPA 2, 2020

Recognizing threats – Case Study

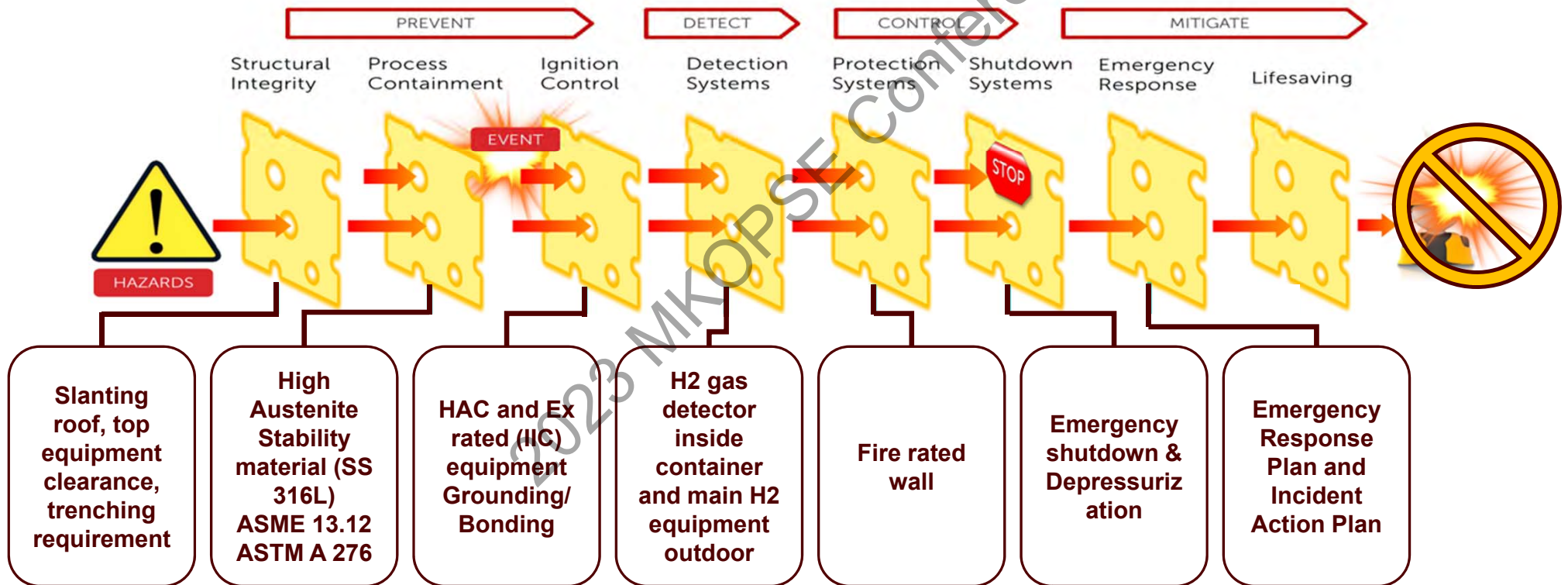
- Results:
 - Dispersion to LFL – 1.5 meter
 - Jet Fire radiation ellipse – 1.2 meter
 - Jet Flame length – 1 meter
- Full rupture fire duration is only <1 second even though the impact radius is large



Dispersion

Jet Fire

Post Hazard recognition – “Design-It-Right”



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78th Annual Instrumentation and Automation Symposium



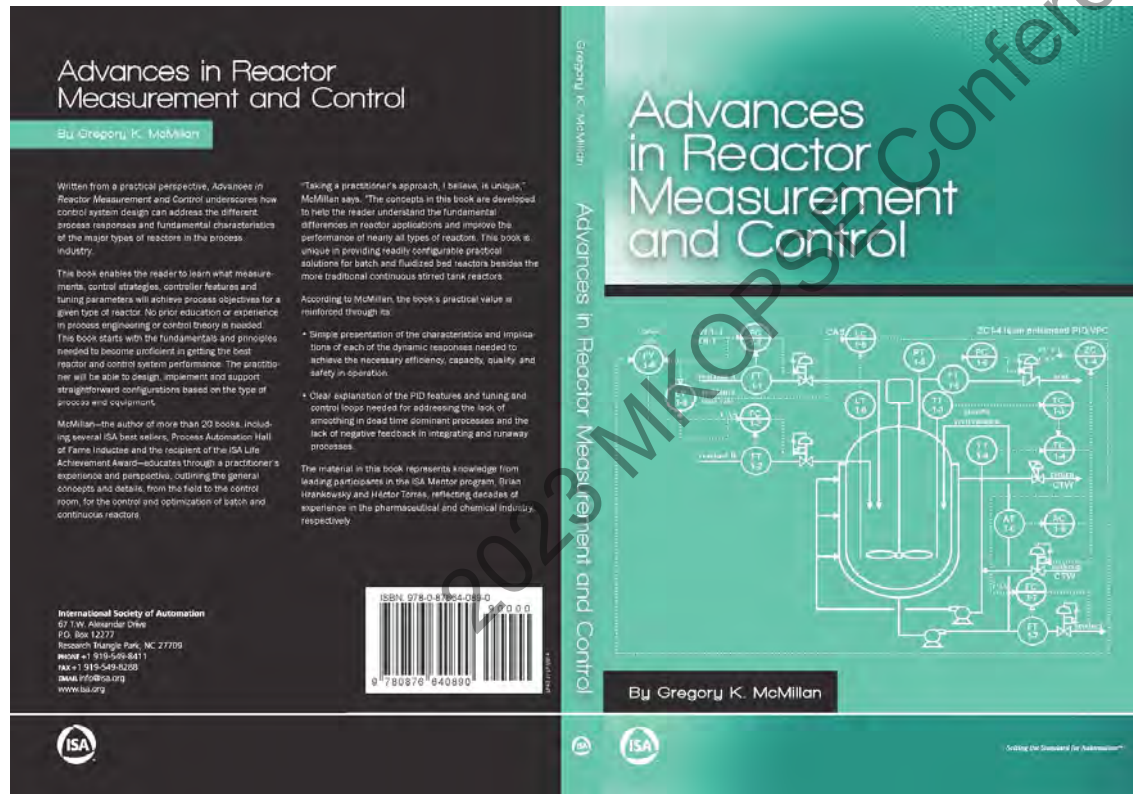
Speaker profile

- Gregory K. McMillan is a retired Senior Fellow from Solutia
- Control Magazine “Engineer of the Year” award in 1994
- Control Magazine “Automation Hall of Fame” inductee in 2001
- InTech Magazine “Most Influential Innovators” award in 2003
- International Society of Automation “Life Achievement” award in 2011
- Author of more than 30 books and 400 articles
 - <https://blog.isa.org/author/greg-mcmillan>
 - <https://www.controlglobal.com/blogs/controltalkblog>

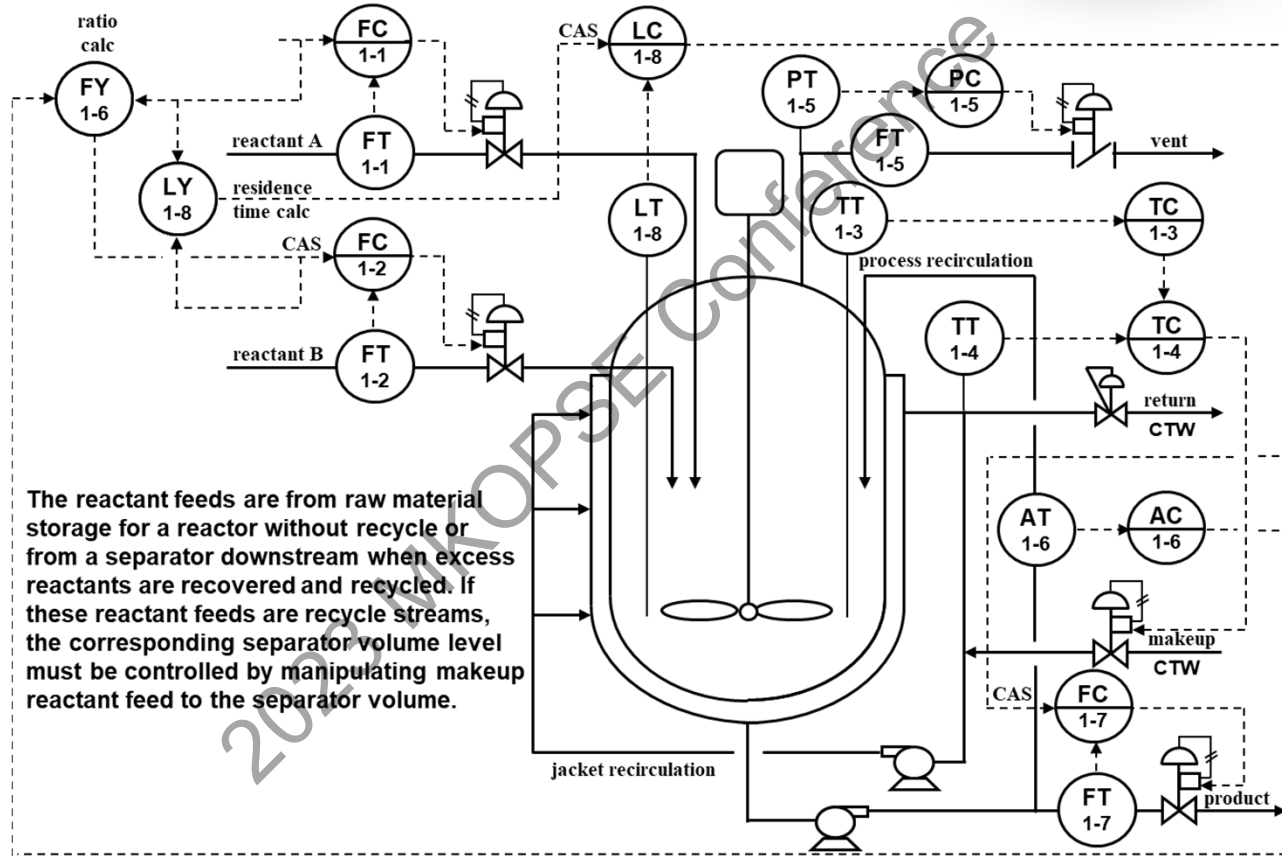




Control Strategies to Improve Reactor Performance

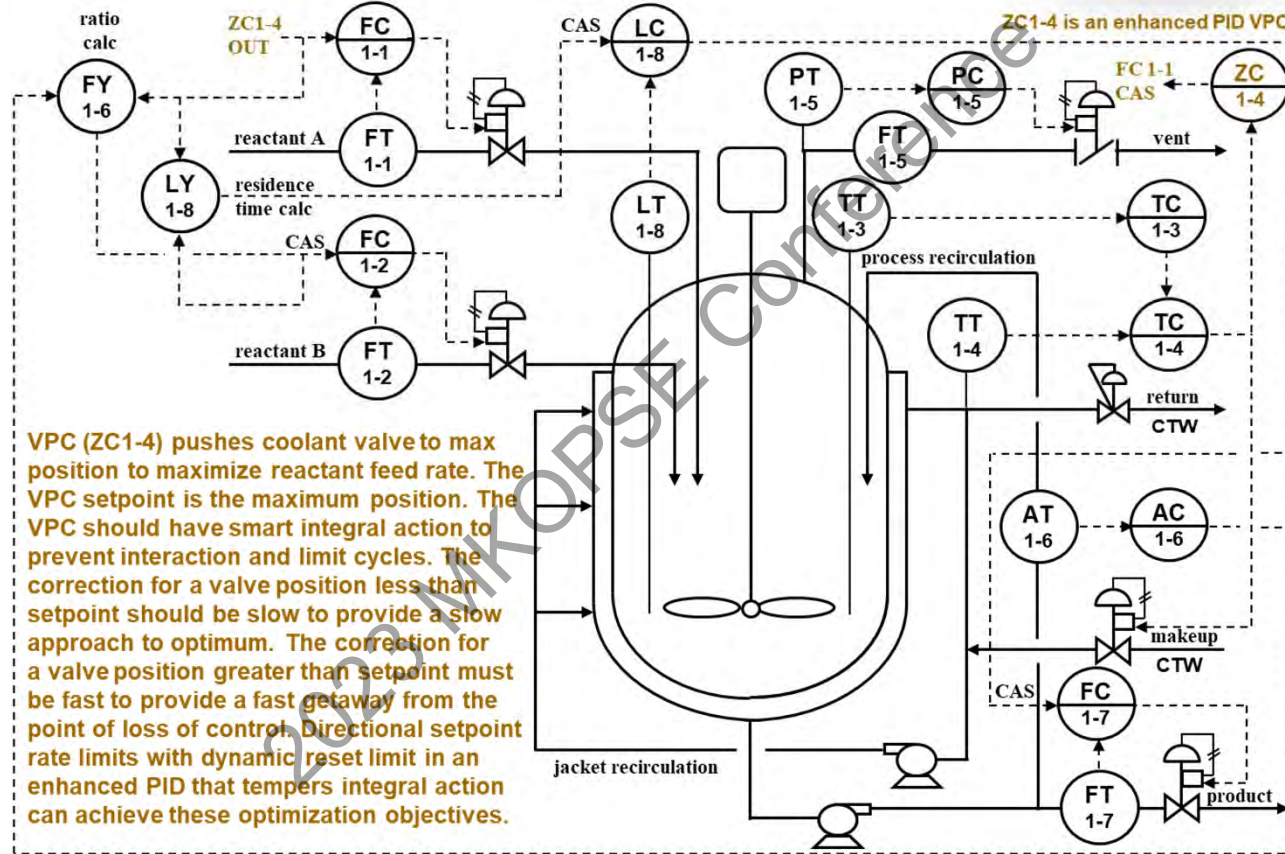


About 20 free copies will be available to give out to presentation attendees

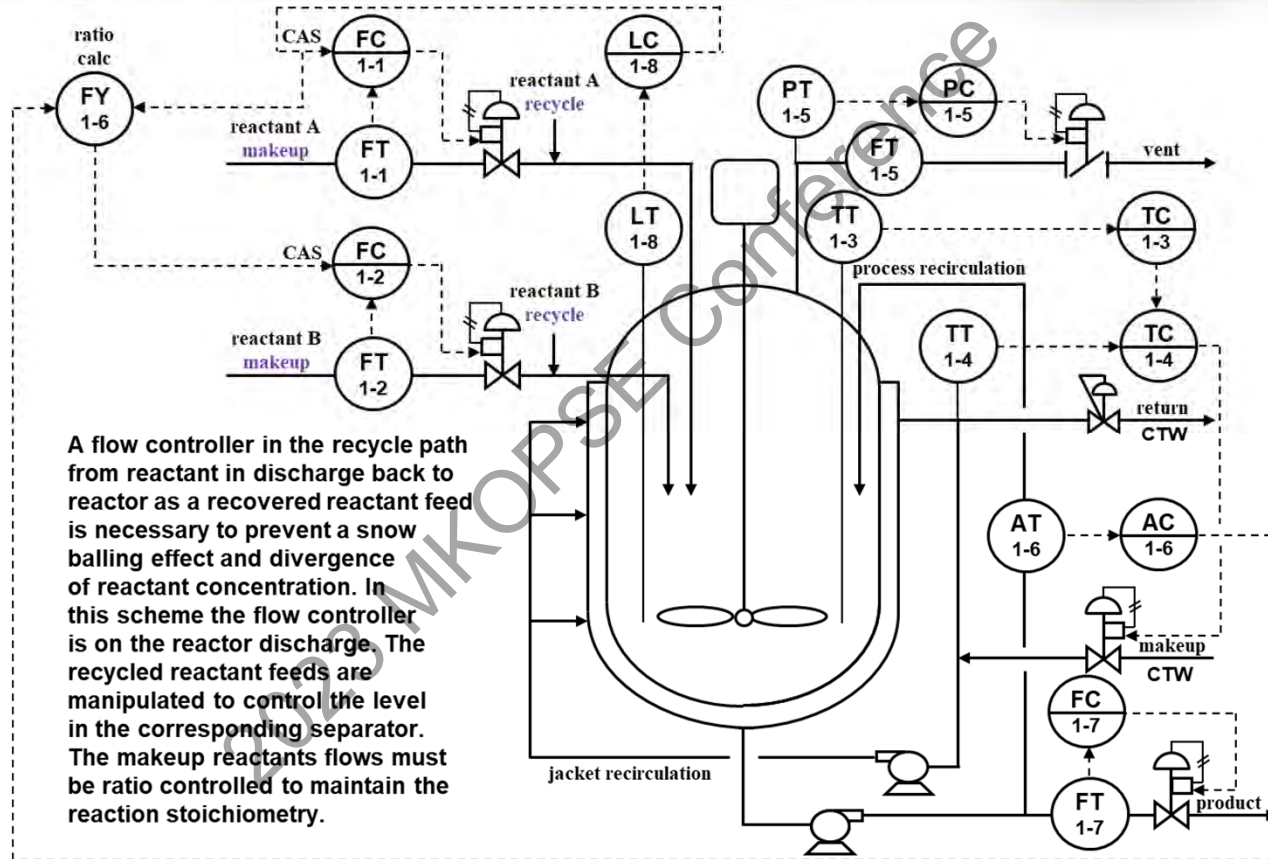


The reactant feeds are from raw material storage for a reactor without recycle or from a separator downstream when excess reactants are recovered and recycled. If these reactant feeds are recycle streams, the corresponding separator volume level must be controlled by manipulating makeup reactant feed to the separator volume.

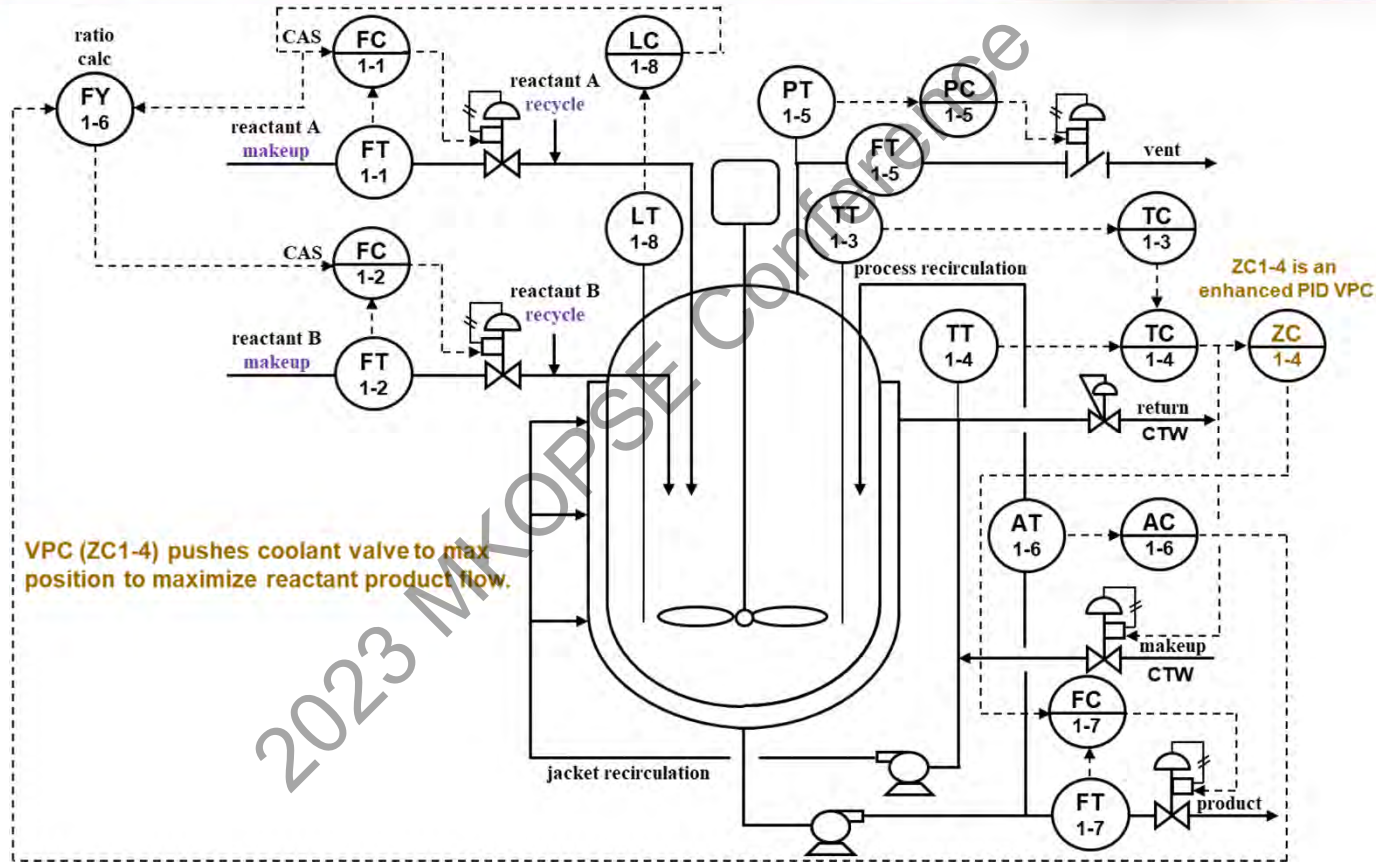
For a liquid reactor, level control sets reaction time via residence time, temperature control sets reaction rate via energy, and composition control enforces the stoichiometric ratio.



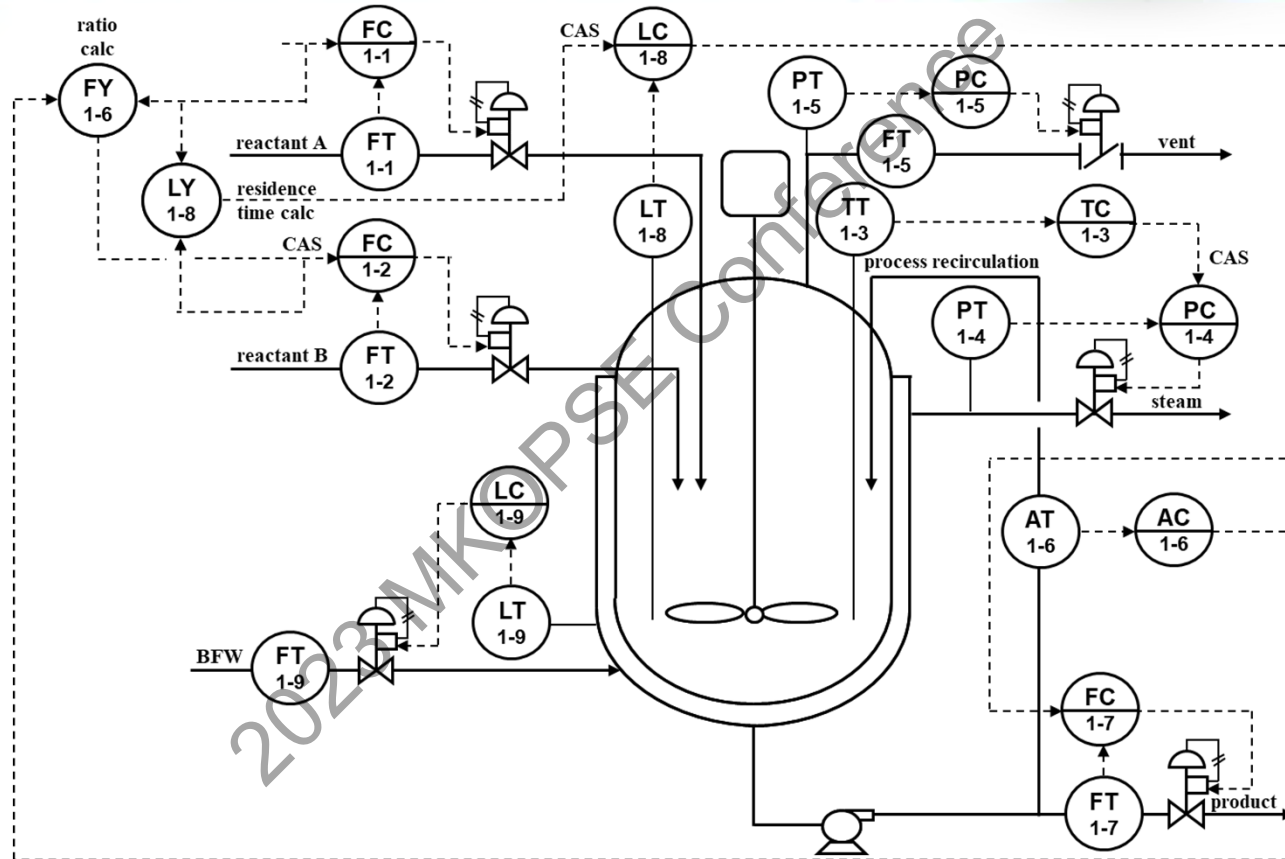
For a liquid reactor, the production rate can be maximized by a VPC (ZC1-4) that increases reactant feed till the jacket temperature valve reaches maximum position.



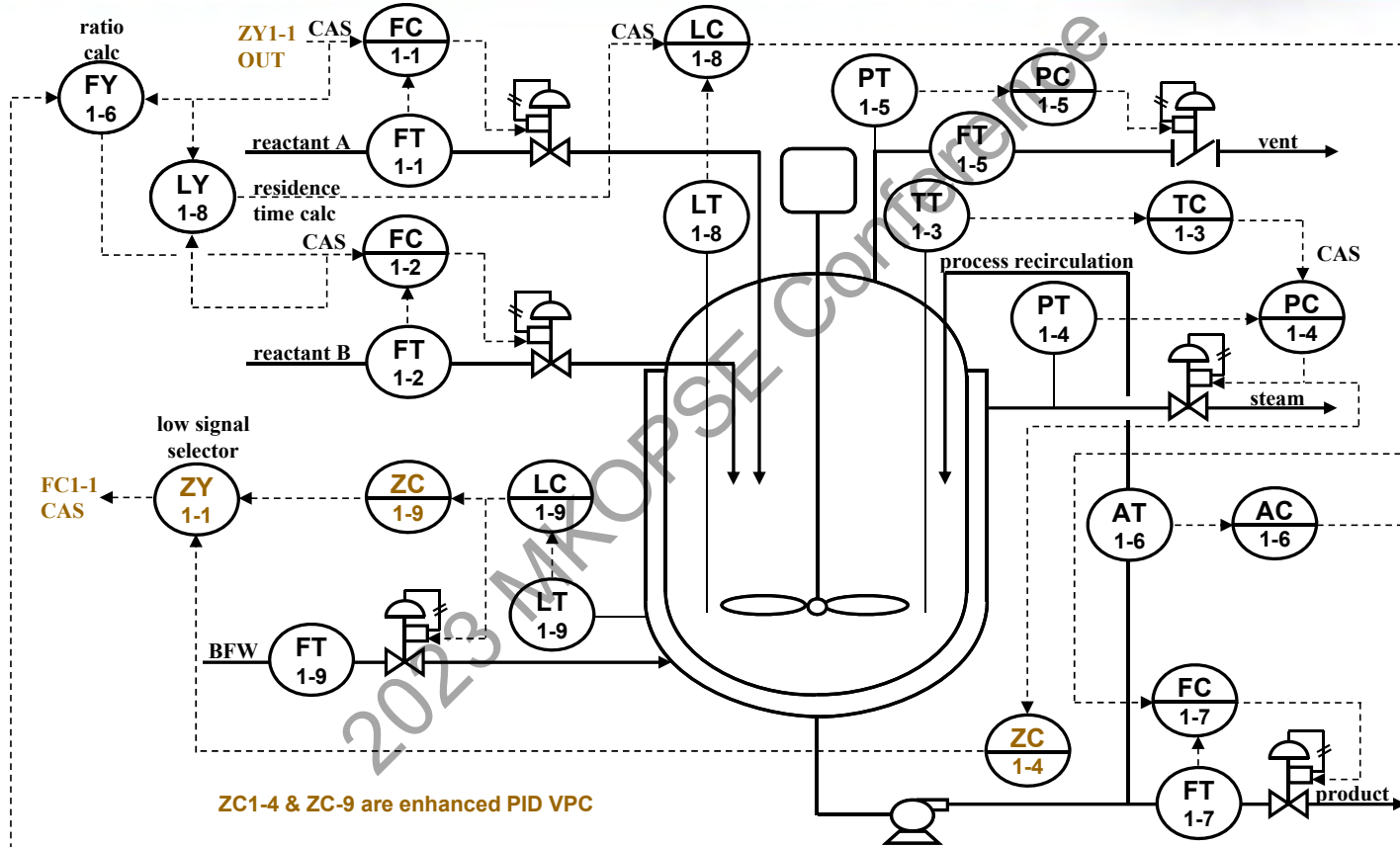
For a liquid reactor with recycle of recovered reactants set by downstream separator level controllers, the makeup reactant flows must be ratioed to maintain stoichiometry.



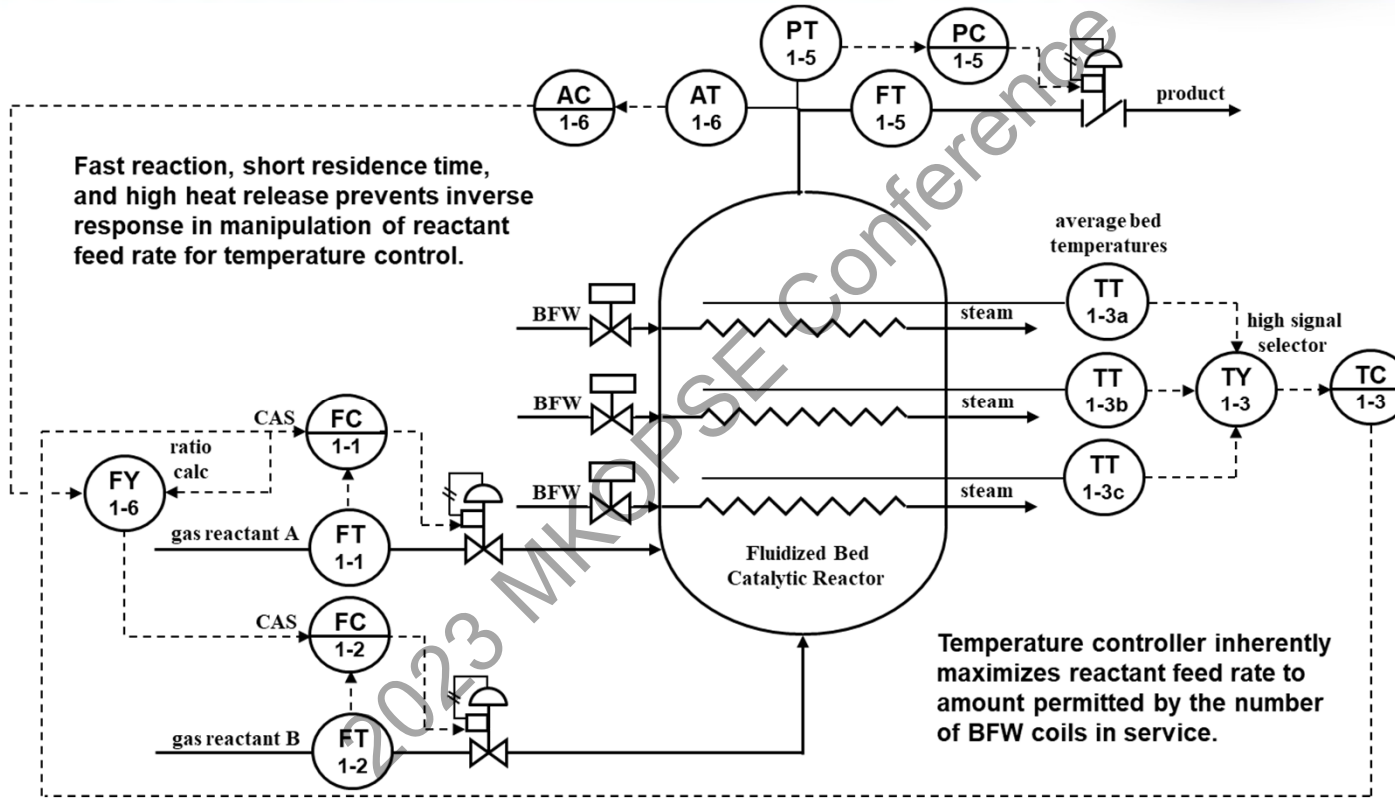
For a liquid reactor with recycle of recovered reactants set by downstream separator level controllers, the production rate can be maximized by VPC setting discharge flow.



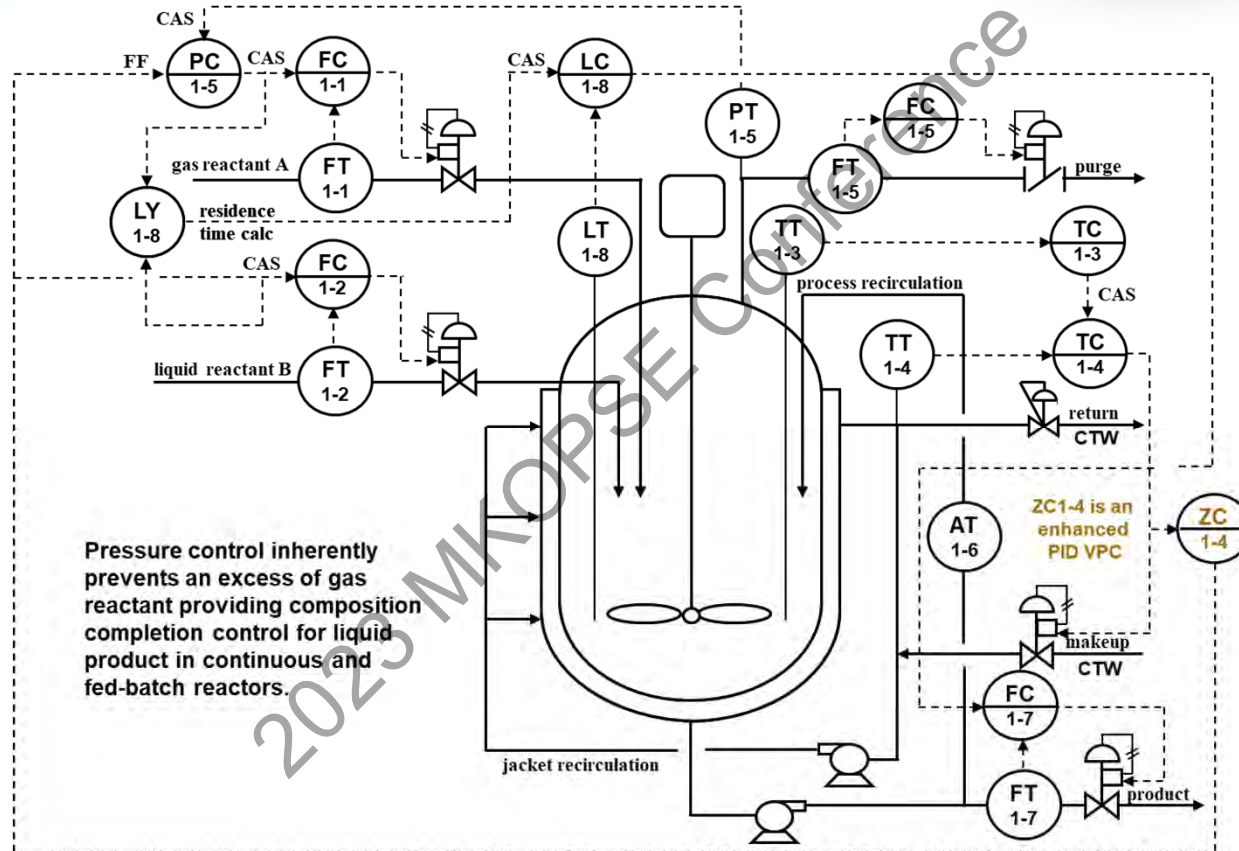
For a high temperature liquid reactor, coolant is replaced with the boiling of water to provide a constant temperature heat sink that helps stabilize highly exothermic reactions.



For a high temperature liquid reactor, the production rate can be maximized by a VPC that increases reactant feed till the BFW or steam valve reach maximum position.

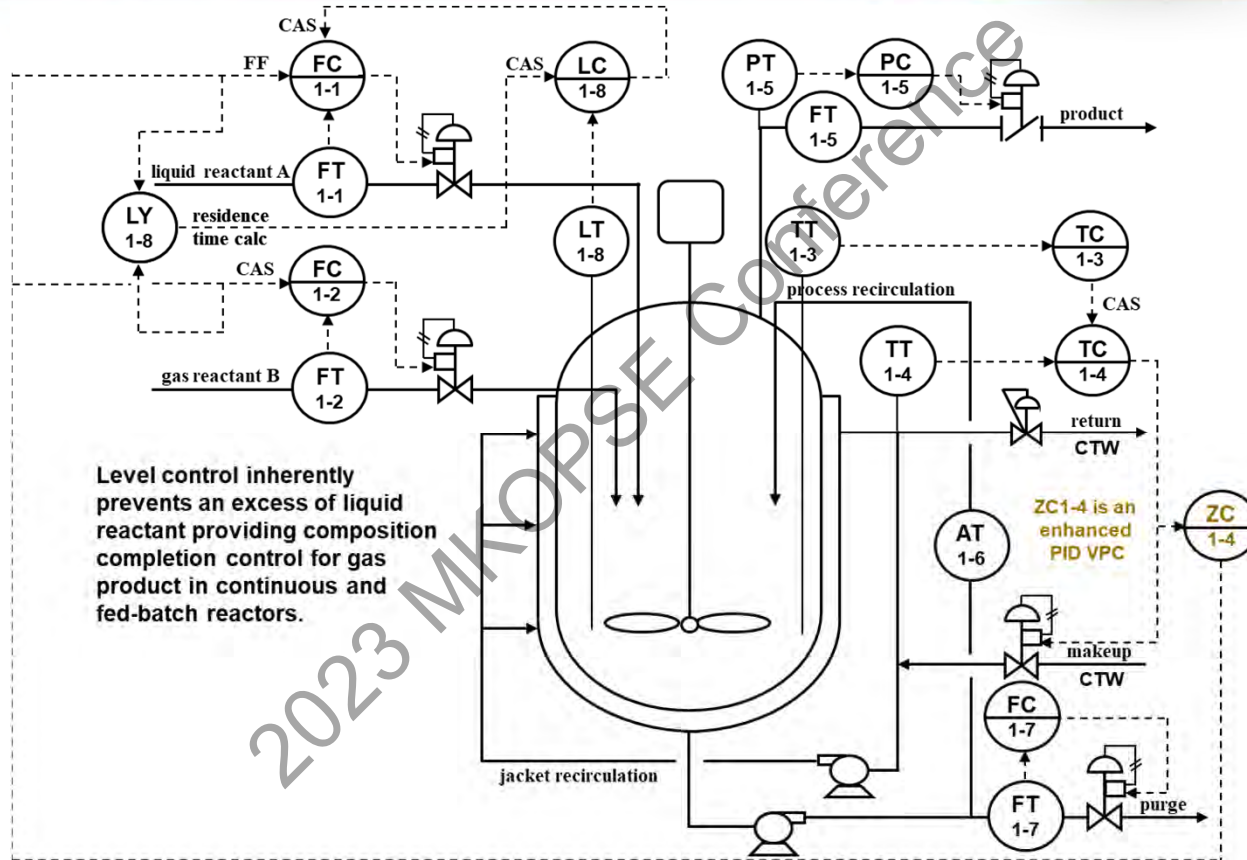


An enhanced PID using an at-line analyzer or inferential measurement for concentration control sets the gas reactant flow ratio, a pressure controller sets reaction time, and a temperature control system maximizes reaction rate by setting gas feed rate.

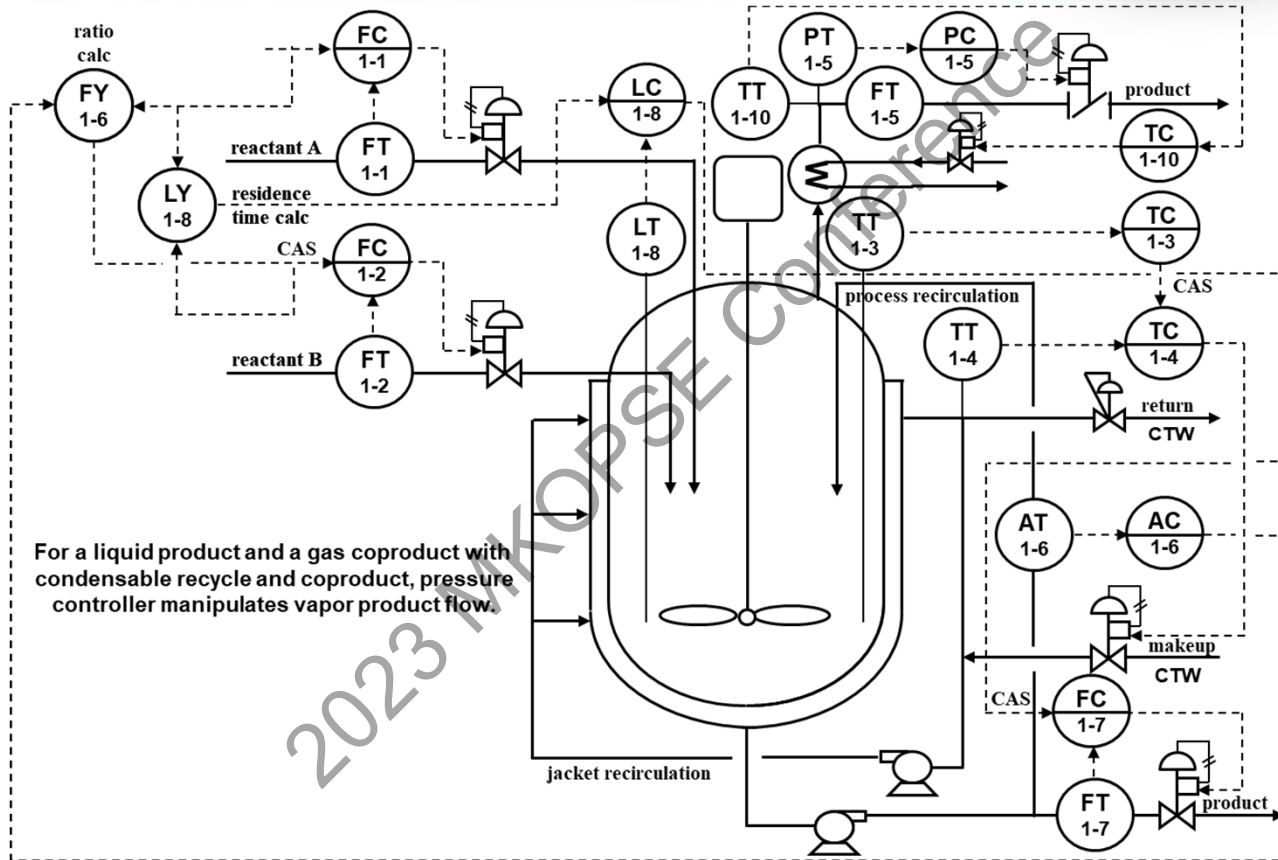


Pressure control inherently prevents an excess of gas reactant providing composition completion control for liquid product in continuous and fed-batch reactors.

For a liquid and gas reactants, and a liquid product, pressure control maintains continuous composition completion control and level control maintains the liquid inventory.

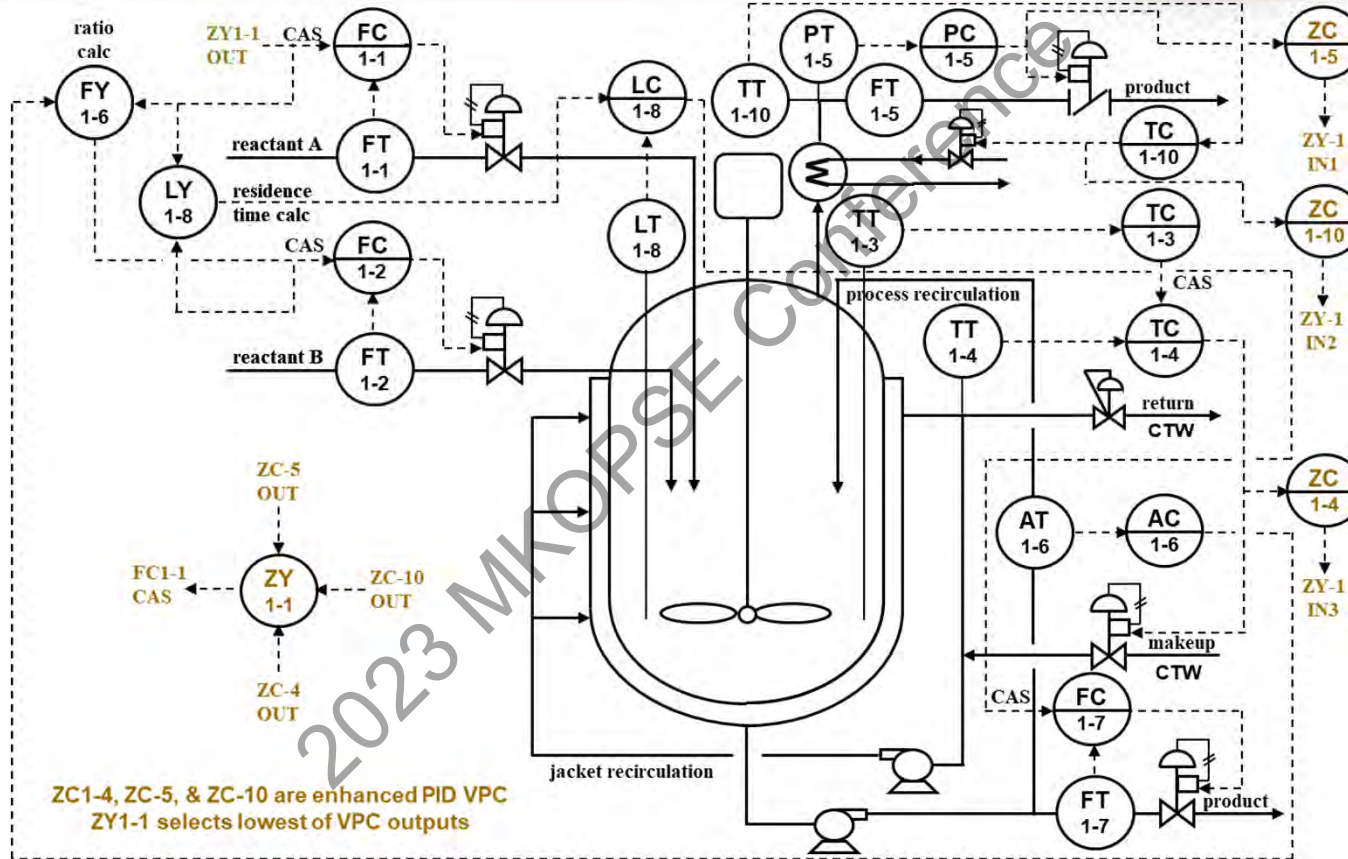


For a liquid and gas reactants, and a gas product, level control maintains continuous composition completion control and pressure control maintains the gas inventory.

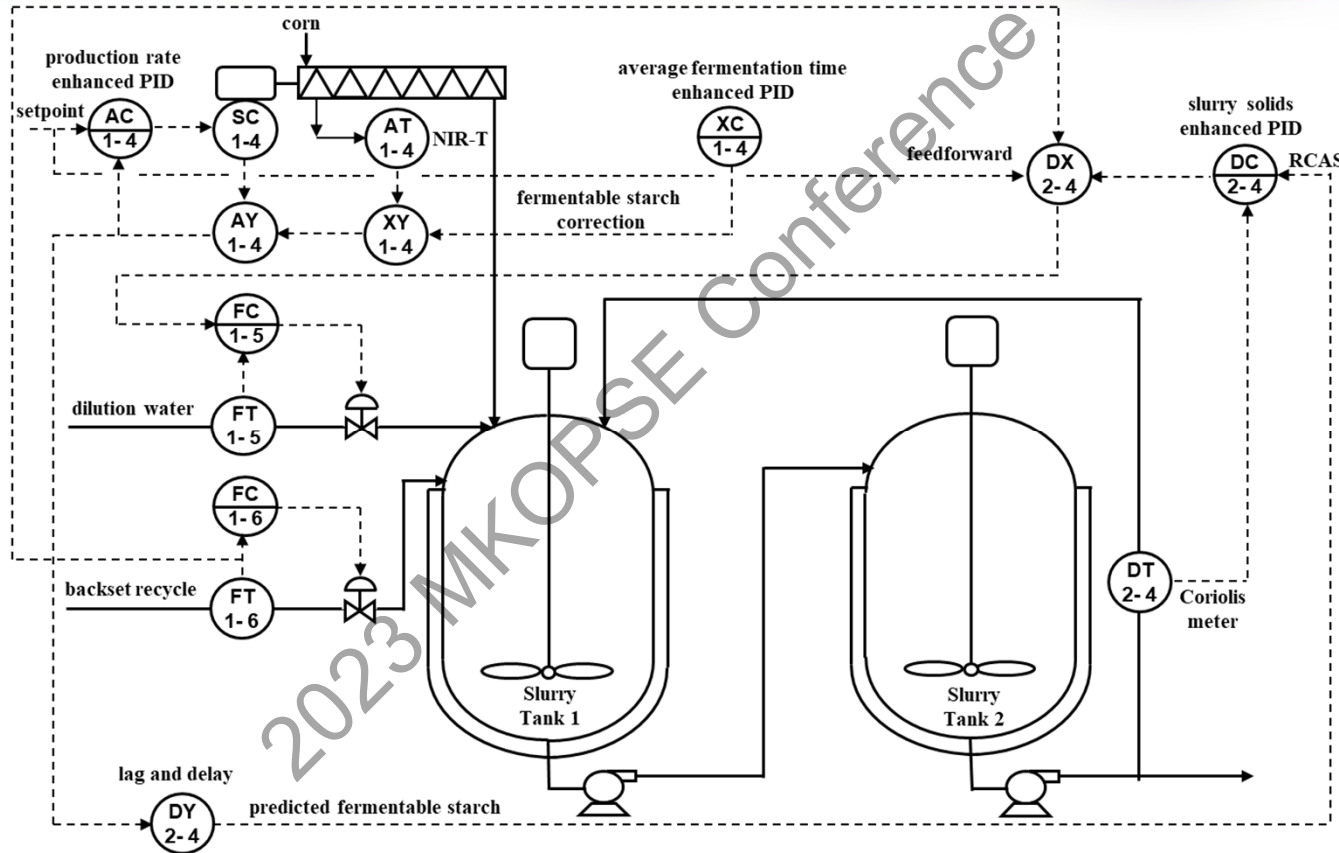


For a liquid product and a gas coproduct with condensable recycle and coproduct, pressure controller manipulates vapor product flow.

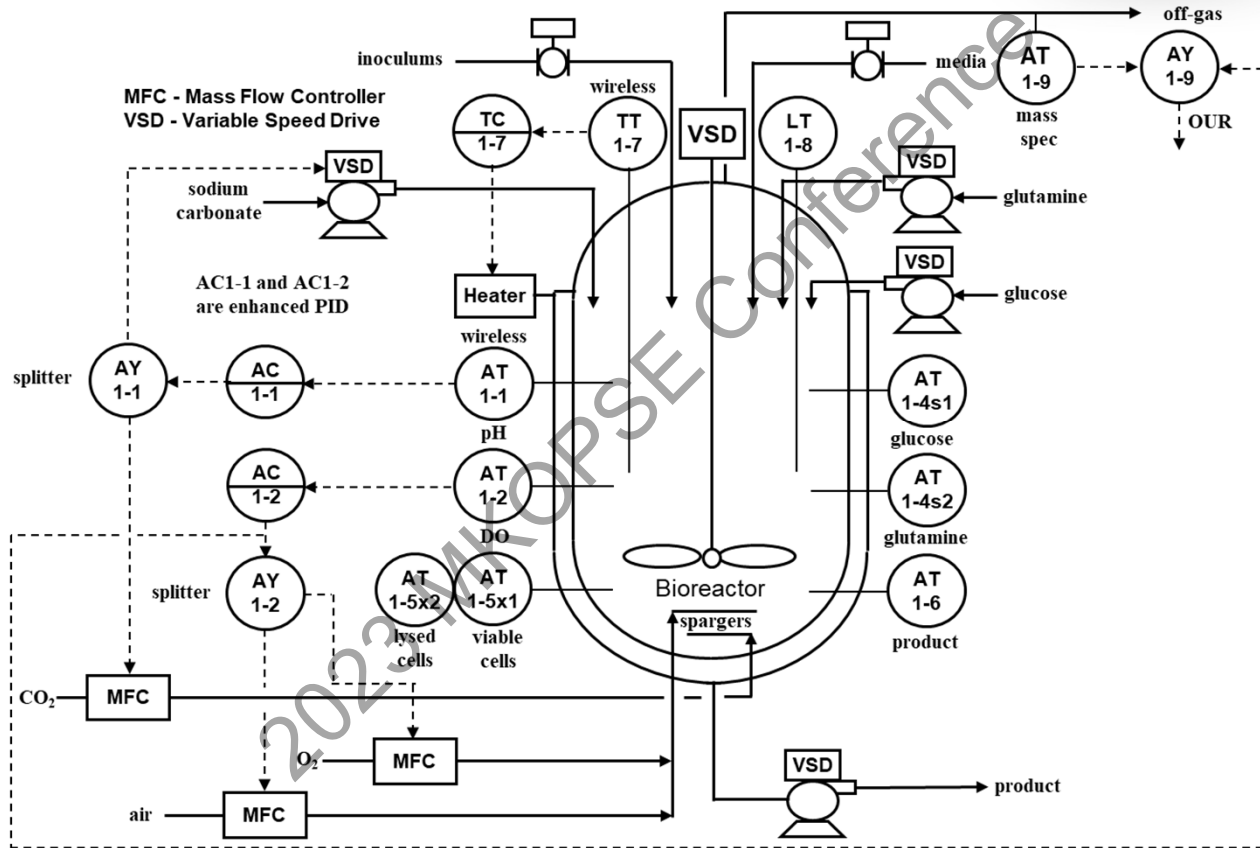
For a liquid product and a gas co-product with condensable recycle and co-product, a reactor pressure controller manipulates vapor product flow.



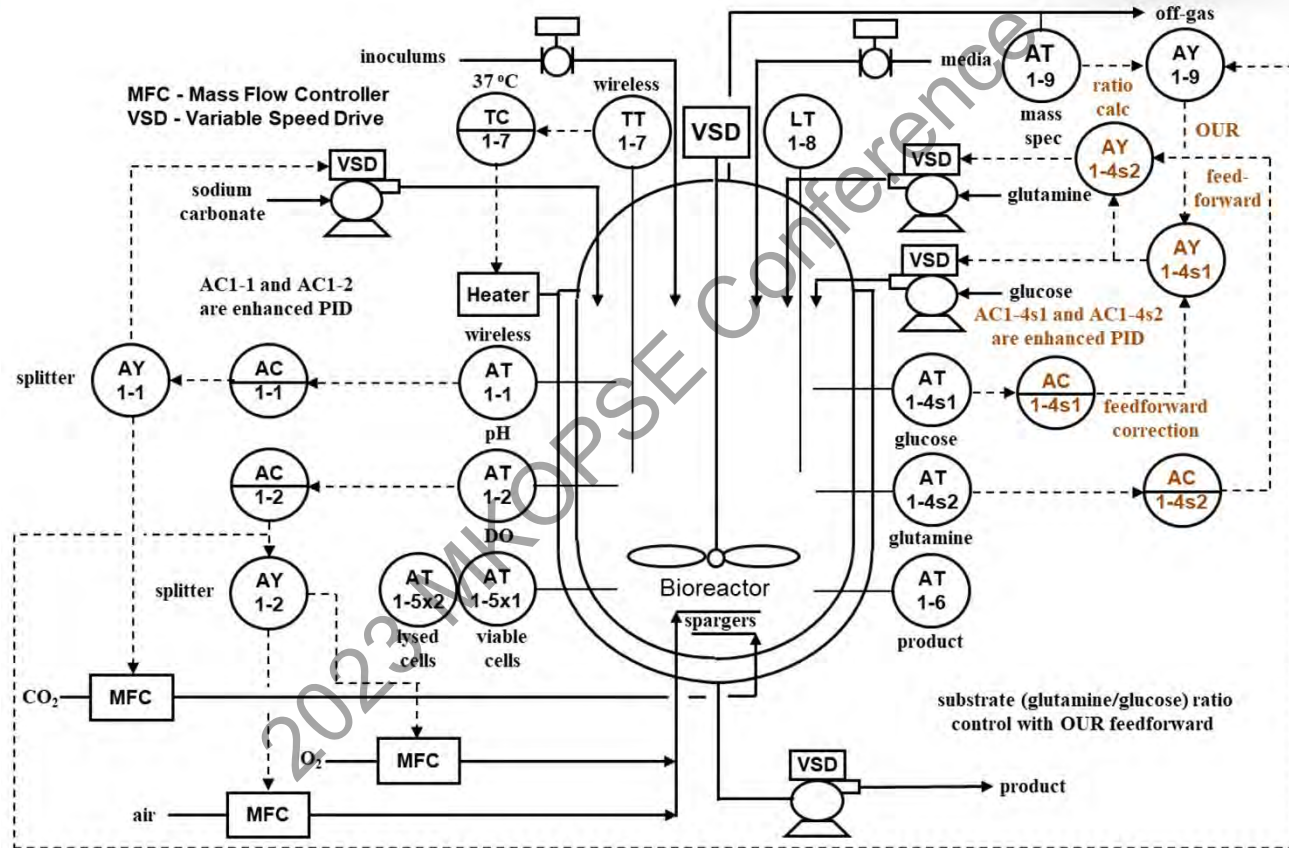
For a liquid product and a gas co-product, the production rate can be maximized by a VPC that increases reactant feed till the coolant valves and gas product valve reach maximum position



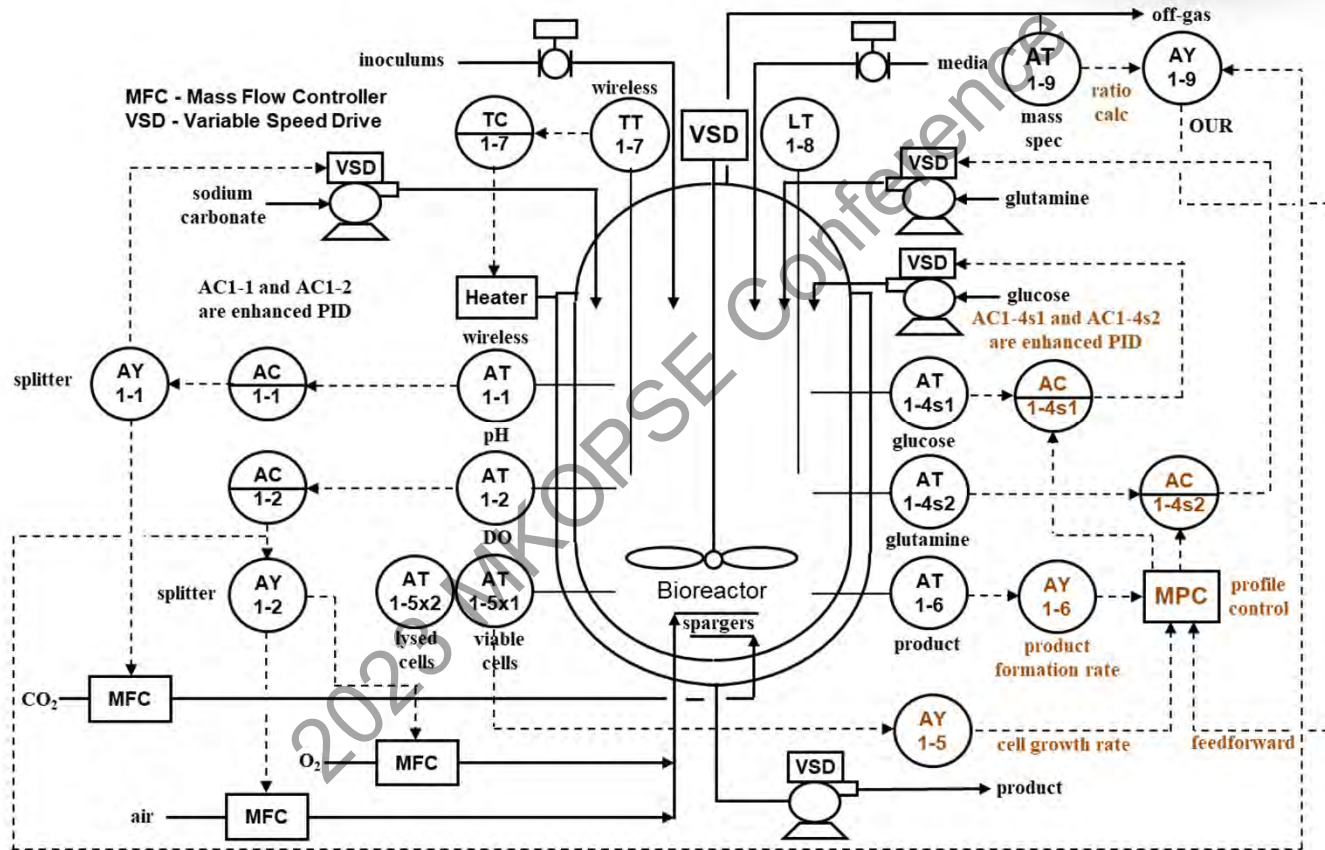
Ethanol plant yield can be increased by the use of an at-line corn analyzer and enhanced PID to optimize corn feed rate, slurry solids concentration, and batch time.



Mammalian bioreactors have all of the process control of bacterial reactors, but with more complex DO and pH loops with decoupling and smarter split ranged control.



Online and at-line analyzers enable substrate concentration control with glutamine feed ratioed to glucose. An OUR feedforward anticipates changes in glucose utilization rate.



Growth rate and product formation rate from the rate of change of actual or inferential measurements can provide fed-batch profile control by the manipulation of glucose and glutamine.

Coriolis Meters and Completion Control

- For well mixed reactors the largest sources of improper reactant concentration leading to excess reactant are errors in reactant flow measurement and changes in reactant composition. Note that a deficiency in one reactant concentration creates an excess of another reactant. Coriolis meters can be used to provide the greatest mass flow measurement precision and rangeability with density correction for any changes in reactant feed concentration. Consequently, Coriolis meters on reactant feeds eliminate most of the sources of reactant unbalances if the mass flow ratios are correct and coordinate to maintain reaction stoichiometry
- If density of the excess reactant is significantly different than the density of the other components in the reactor, a Coriolis meter in the recirculation line can provide an inline inferential measurement of the excess reactant concentration. Inline composition measurements by means of sensors in a vessel or pipeline provide a measurement in a few seconds whereas at-line analyzers with sample systems can have 30 or more minutes of dead time due to sample and analyzer cycle times. An enhanced PID is essential to deal with these cycle times.
- Completion control seeks to provide for both batch and continuous reactors a complete conversion of all the reactants and consequently no excess accumulation of a reactant in a particular phase. If the reactants are in different phases and the product is a single phase, inventory control can be used for reaction completion control. The product must be a gas, liquid, or solids with no recycle or co-products in the other phases.

Key PID Features for Valve Position Control

Feature	Function	Advantage 1	Advantage 2
Up Down SP Velocity Limits (Directional Move Suppression)	Limit VPC Action Speed Based on Direction	Prevent Running Out of Valve	Minimize Disruption to Process
External Reset Feedback (Dynamic Reset Limit)	Limit VPC Action Speed to Process Response	Direction Velocity Limits	Prevent Burst of Oscillations
Adaptive Tuning	Automatically Identify and Schedule Tuning	Eliminate Manual Tuning	Compensation of Nonlinearity
Feedforward	Preemptively Set VPC Out for Upset	Prevent Running Out of Valve	Minimize Disruption
Enhanced PID (PIDPlus)	Suspend Integral Action until PV Update	Eliminate Limit Cycles from Stiction & Backlash	Minimize Oscillations from Interaction & Delay

For much more on how valve position control (VPC) is used for optimization of unit operations checkout the Control magazine article “Don’t Over Look PID in APC”

<https://www.controlglobal.com/control/distributed-control/article/11380959/control-valves-dont-over-look-pid-in-apc>

2022 Mary Kay O'Connor Safety & Risk Conference

Health to Human is Safety to System:
Making Safety Second Nature

In Association with IChemE and C-RISE

Process Safety Health: How Should We
Approach Metrics and Monitoring?

October 5-7, 2022



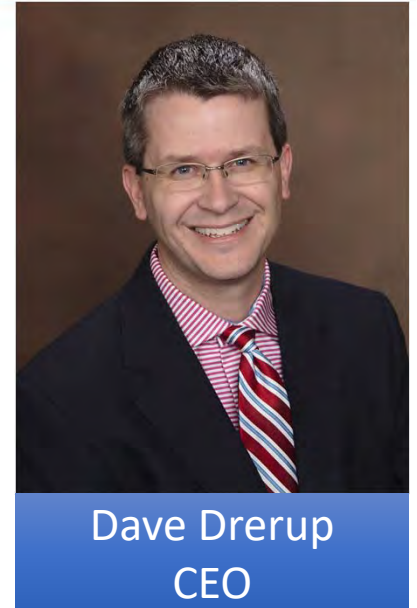
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Speaker profile

- Dave Drerup
- Operational Sustainability, LLC
- 29 Years in the Industry
- Field of Expertise: Process Safety, Mechanical Integrity, EH&S, Operational Excellence, IT Consulting
- Industry Involvement/Recognition: API Code Committees, AFPM, CCPS, Contribute to CCPS Publications



Process Safety Metrics

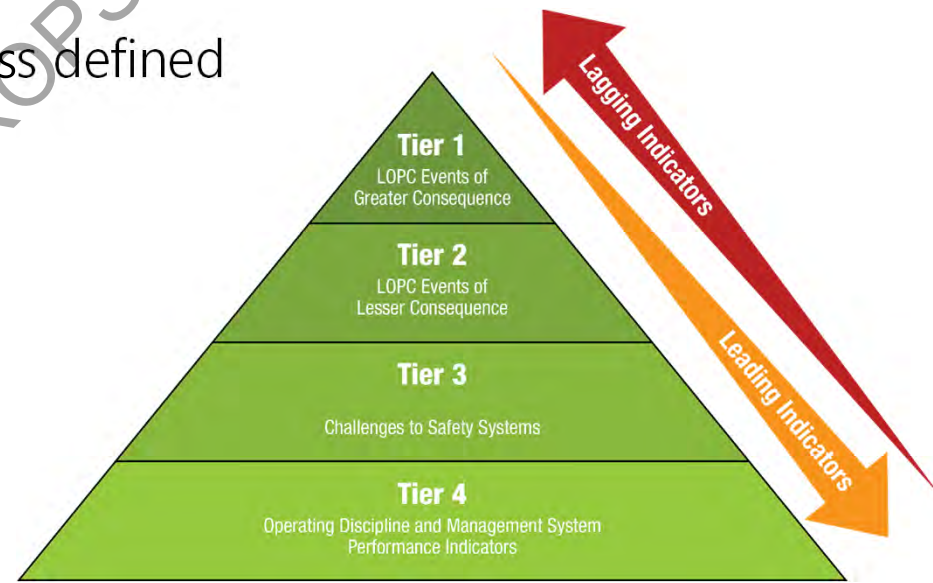
- Reporting and management system standards and guidelines
 - Good news ... They exist
 - Bad news ... There are lots of them
- Can be subjective and open for local or organizational interpretation
- Benchmarking efforts is challenging
 - AFPM, Phillip Townsend & Assoc., API 754...
- Leading indicators are more difficult



API-754

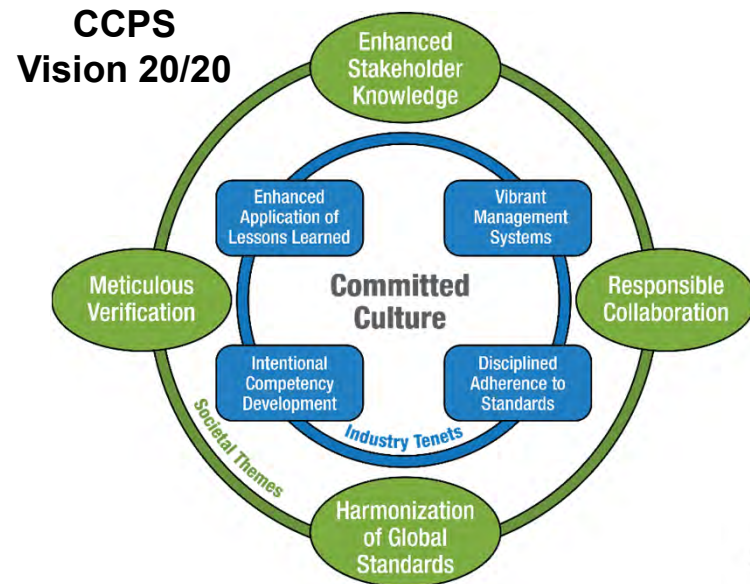
- Example: API RP-754 – Process safety indicators for the refining and petrochemical industries
- Helps assure accurate assessment of incidents for individual sites
- Drives consistency allowing Tier 1 & 2 comparison across an enterprise and with peers
- Leaves leading indicators less defined

- The count of **Tier 1** process safety events is the most lagging performance indicator and represents incidents with greater consequence resulting from actual losses of containment.
- The count of **Tier 2** process safety events represents loss of primary containment events with a lesser consequence, but may be predictive of future, more significant incidents.
- **Tier 3** events represent challenges to the safety systems. Indicators at this level provide an opportunity to identify and correct weaknesses within the safety system.
- **Tier 4** indicators represent operating discipline and management system performance.



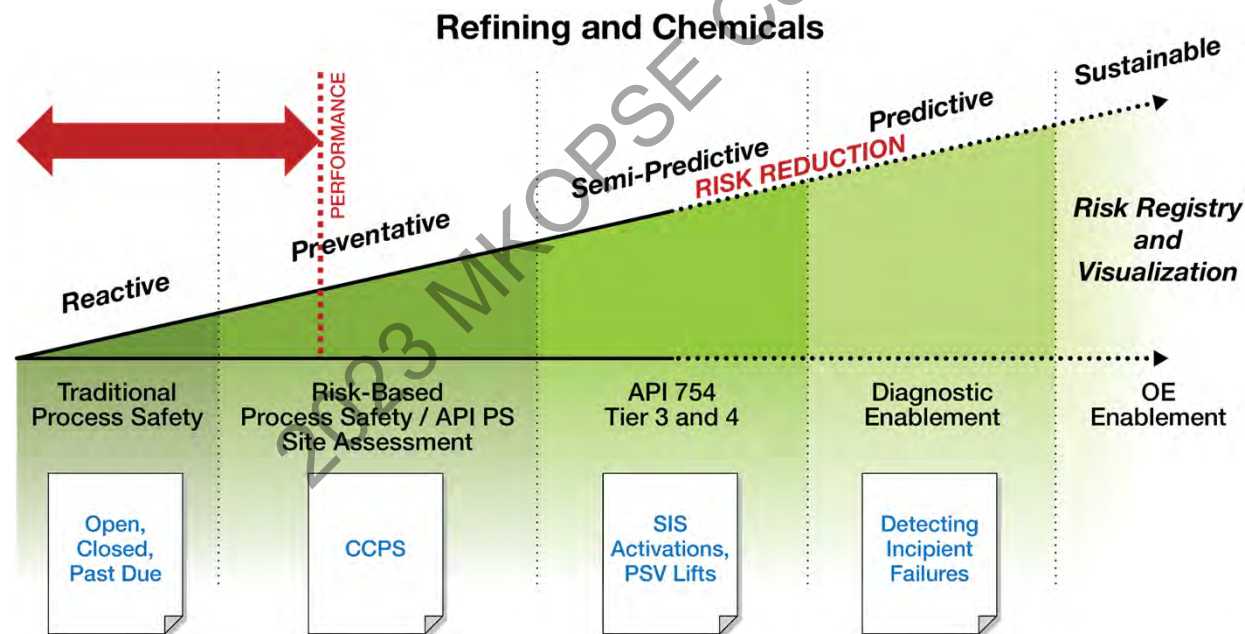
Why ESG Matters in Process Safety

- Societal Expectations on performance tied to privilege to operate
- Risk-Based Process Safety Brings in Conduct of Operations
- API 754 Tier 4 – “G” is in the management system performance
- Tier 4 also requires “Operational Discipline”
- Develop useful metrics for Tier 4 and enact “Orchestration”



Metric Maturity / Opportunity

- Advancing to predictive / sustainable levels of performance maturity depends upon leading indicators



Process Safety Metrics: "Leading is arguably lagging. Process Safety [today] is inherently reactive," per the Baker Panel Report.

Challenges



What is Process Safety Health?

A holistic, continuous monitoring methodology covering all process safety functional reporting areas to provide a clear picture of an organization's overall health.

- No IT strategy for process safety
- "Application / Data Silos" – can't aggregate, identify, and manage total risk
- Many data sets generating many reports
- Solutions need to incorporate asset-based intelligence, not just process workflows
- We aren't AI-enabled



To meet the need, companies will need to undergo significant re-architecting of their existing Process Safety IT portfolio.

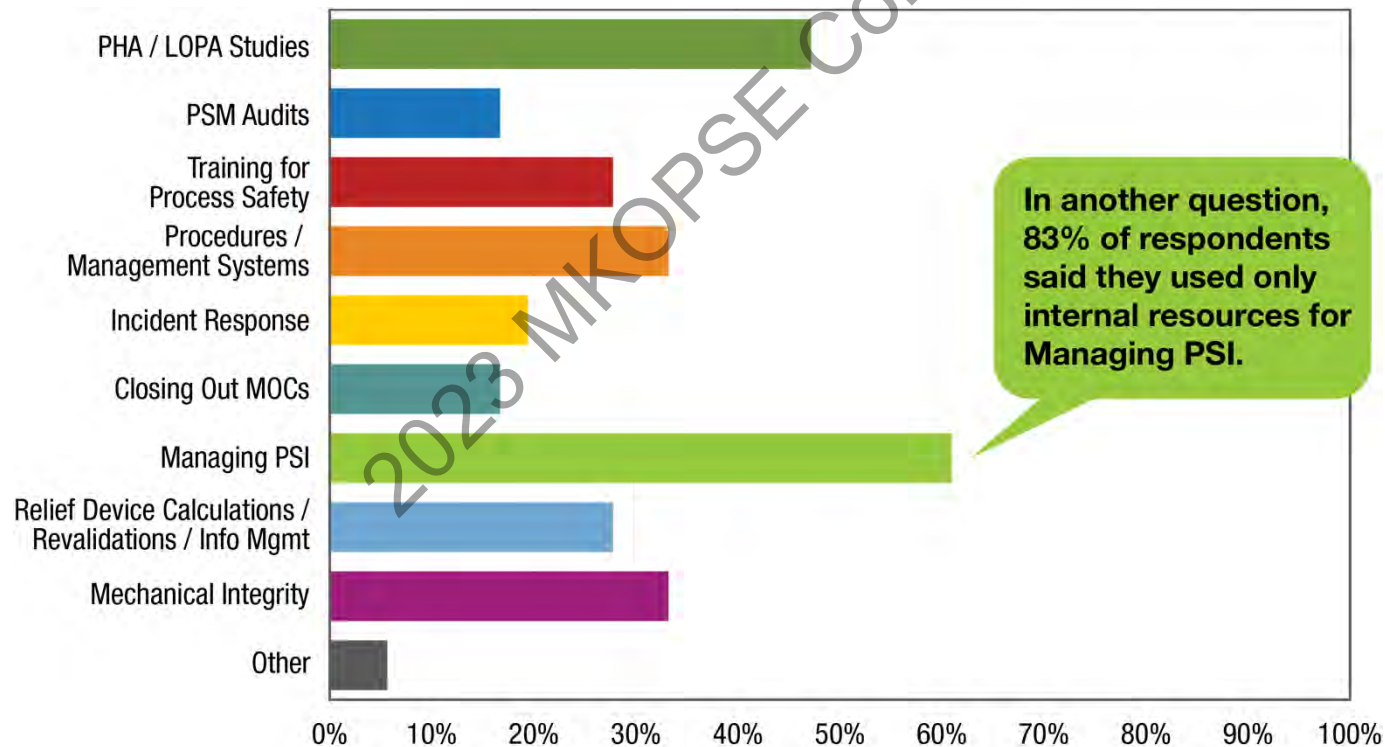
Challenges: Application Proliferation

Audit, Incident Investigation, Corrective & Preventative Actions (CAPA)	➔	Basic EHS compliance starting point focusing on safety with EHS vendors
PHA, MOC, PSSR, Organizational Change	➔	Core PSM focus
Mechanical Integrity	➔	Inspection and EAM software focus area
PSI, Relief Devices	➔	Engineering content vendors
Procedural Automation	➔	Boutique vendors
Training, LMS, Competency Management	➔	LMS vendors
LOPA, SIS, Alarm Management	➔	Safety lifecycle vendors
Work Permitting	➔	EHS vendors

OS PSM market research indicated that nearly two-thirds of respondents from companies with more than 2500 employees were operating in basic, siloed IT systems to manage process safety.

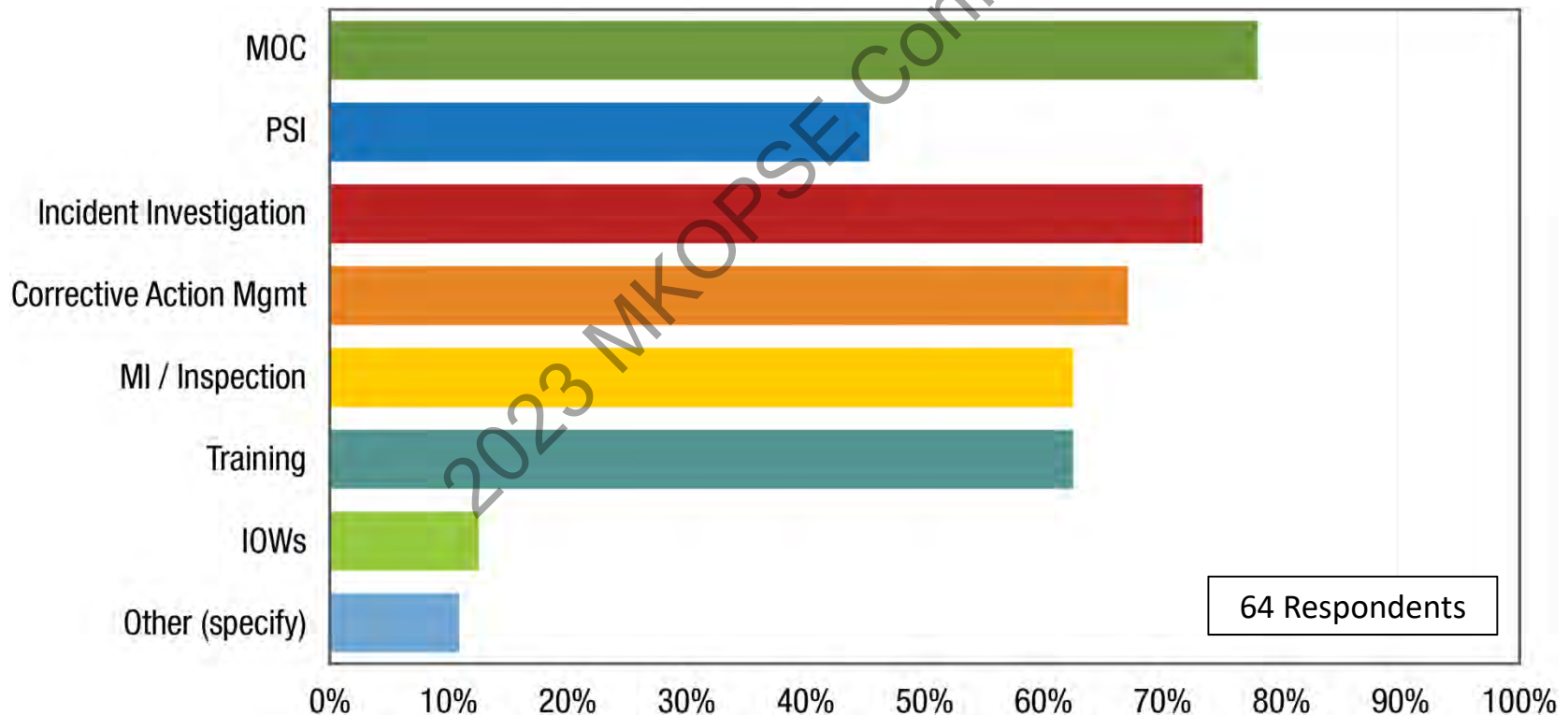
Which Elements Are Most Challenging Today?

- In your opinion, what elements of Process Safety are the hardest to provide adequate resources for, whether internal or external?
(check all that apply)



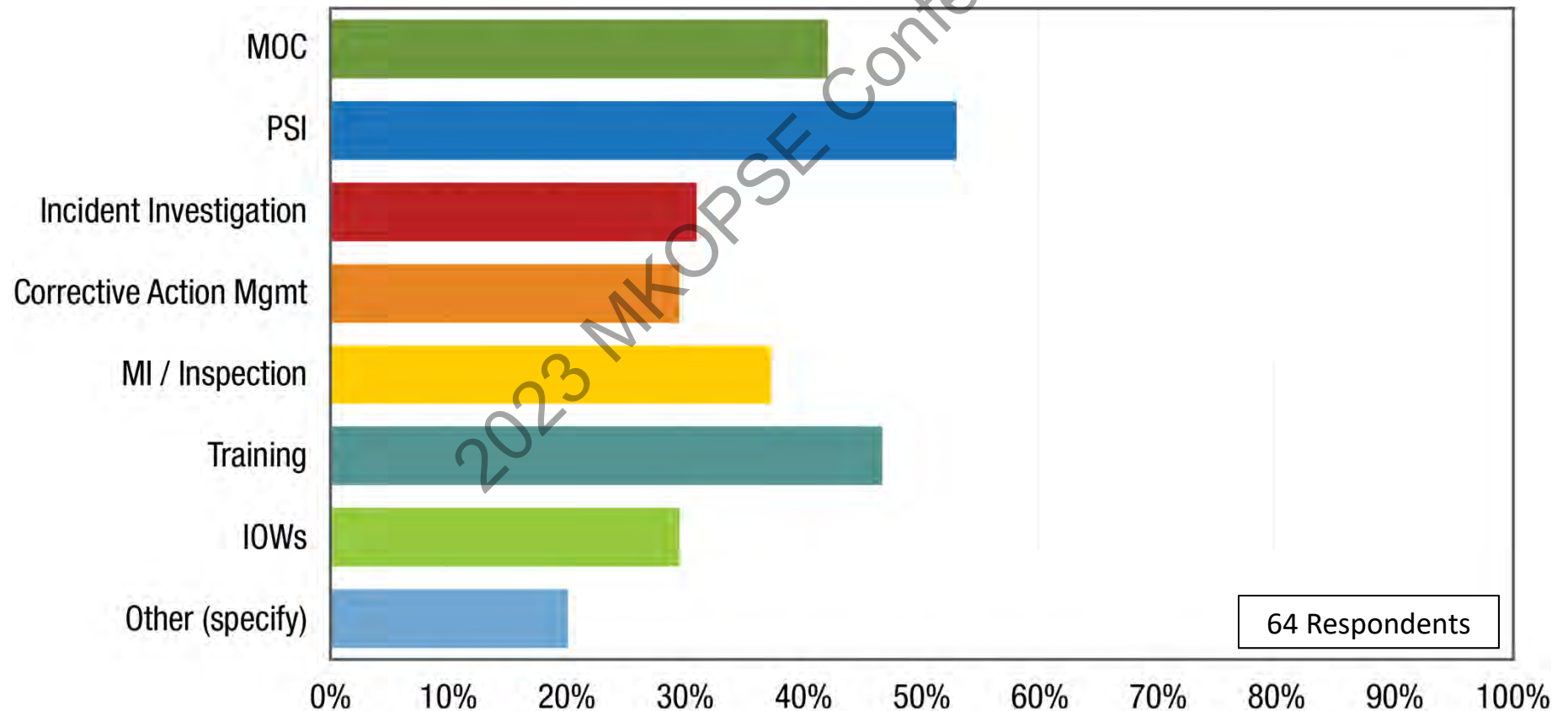
PSM IT Portfolio

- What Process Safety processes currently use significant automation and/or technology in your organization? (check all that apply)



Challenges: Survey – PSM IT Investment

- Thinking about your own facility or organization, do you anticipate an increasing need for automation of these processes within the next 3 years?



Need a Digital "Strategy" for PSM

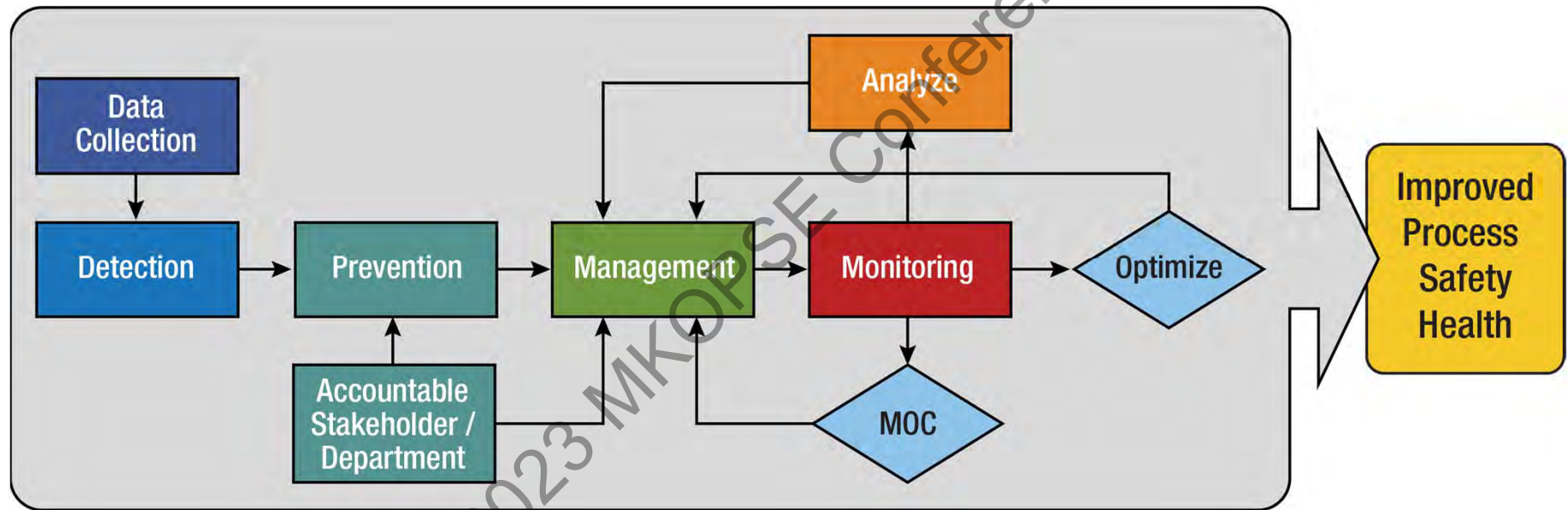


Process Safety
Framework

Strategy to Enable Holistic PSM / Dynamic Risk Management

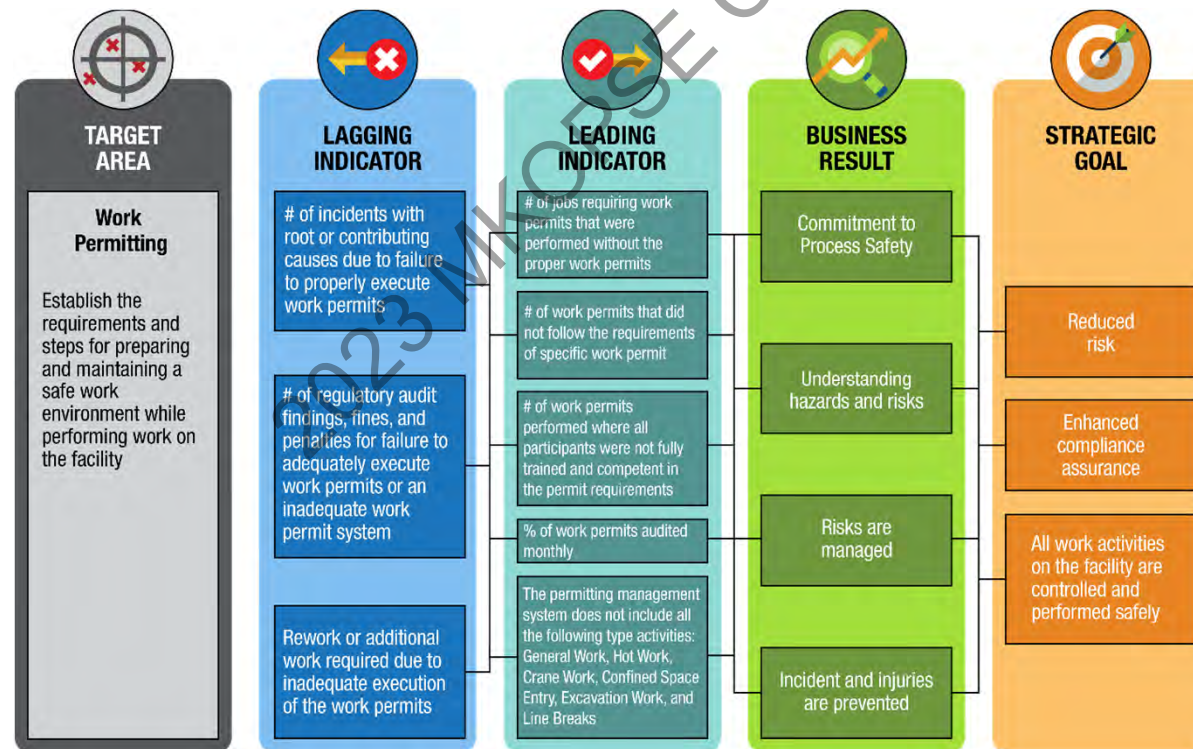
Phase 1	"Basic PSM" CAPA, Incident, Process Risk / PHA
Phase 2	"Intermediate PSM" MOC, PSSR, Document Management, Training, LOPA, Audit
Phase 3	"Advanced PSM" Inspection, Organizational Change, Relief Device Management, Task Management, CoW / LOTO
Phase 4	"Mature PSM" IOWs, RBI, Alarms, SIS, Procedures, PSI, Competency, Production Loss

Process Safety Health



Path Forward: Define Metrics

- Identify indicators tied to quantifying performance risks and risks to achieving Strategic / ESG goals / targets
- Ensure the metrics drive and support the desired actions and culture
- Establish sustainable methods to consistently providing auditable metrics



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Health to Human is Safety to System: Making Safety Second Nature

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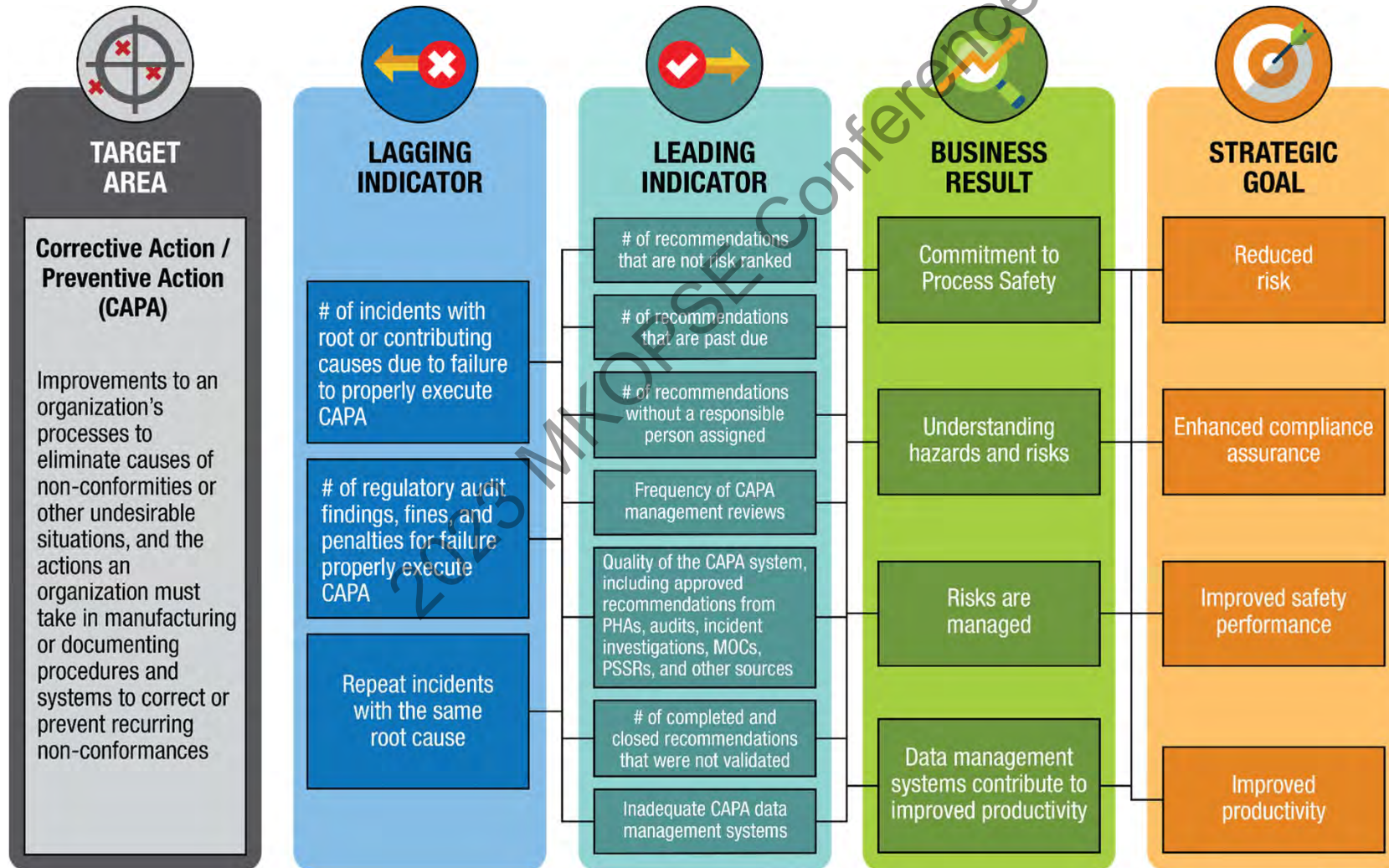
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Create Indicators

Control Theme	Indicator	Implementation
Maintenance and Inspections	Number of overdue BMI inspections	<input type="radio"/>
	Number of watch list items	<input type="radio"/>
	Number of alarm points built and monitored by the Power Optimization Center	<input type="radio"/>
	Number of operational rounds performed	<input type="radio"/>
	Routine maintenance spend (fixed and variable)	<input type="radio"/>
	Capital spend	<input type="radio"/>
	Failures detected by the POC and during rounds	<input type="radio"/>
	Reliability and Availability (GADS)	<input type="radio"/>
Management of Change Process	Number of individuals trained on MOC process and categories	<input type="radio"/>
	Number of changes	<input type="radio"/>
Leadership Behaviors	Number of issues reviewed in leadership meetings	<input type="radio"/>
	Number of issues acted on in the leadership meetings	<input type="radio"/>
	Number of leadership communication on issues and strategy	<input type="radio"/>
Staff Competence and Task Understanding	Number of personal development plans developed by the staff in a specified period of time	<input type="radio"/>
	Number of positions with a defined minimum hiring or transfer qualification	<input type="radio"/>
	Number of tailgate discussions	<input type="radio"/>
	Time since last review of succession planning at plant level w/ SUPT	<input type="radio"/>
	Number of failures due to operator error	<input type="radio"/>
Operating, Start-up, and Shutdown Procedures	Procedures that have a defined review process	<input type="radio"/>
	Procedure review frequency	<input type="radio"/>
	Number of inconsistent operations	<input type="radio"/>

LEGEND	
Leading Indicator	<input type="checkbox"/>
Lagging Indicator	<input type="checkbox"/>
Easy to Implement	<input type="radio"/>
Moderate to Implement	<input type="radio"/>
Difficult to Implement	<input type="radio"/>

Target Metrics



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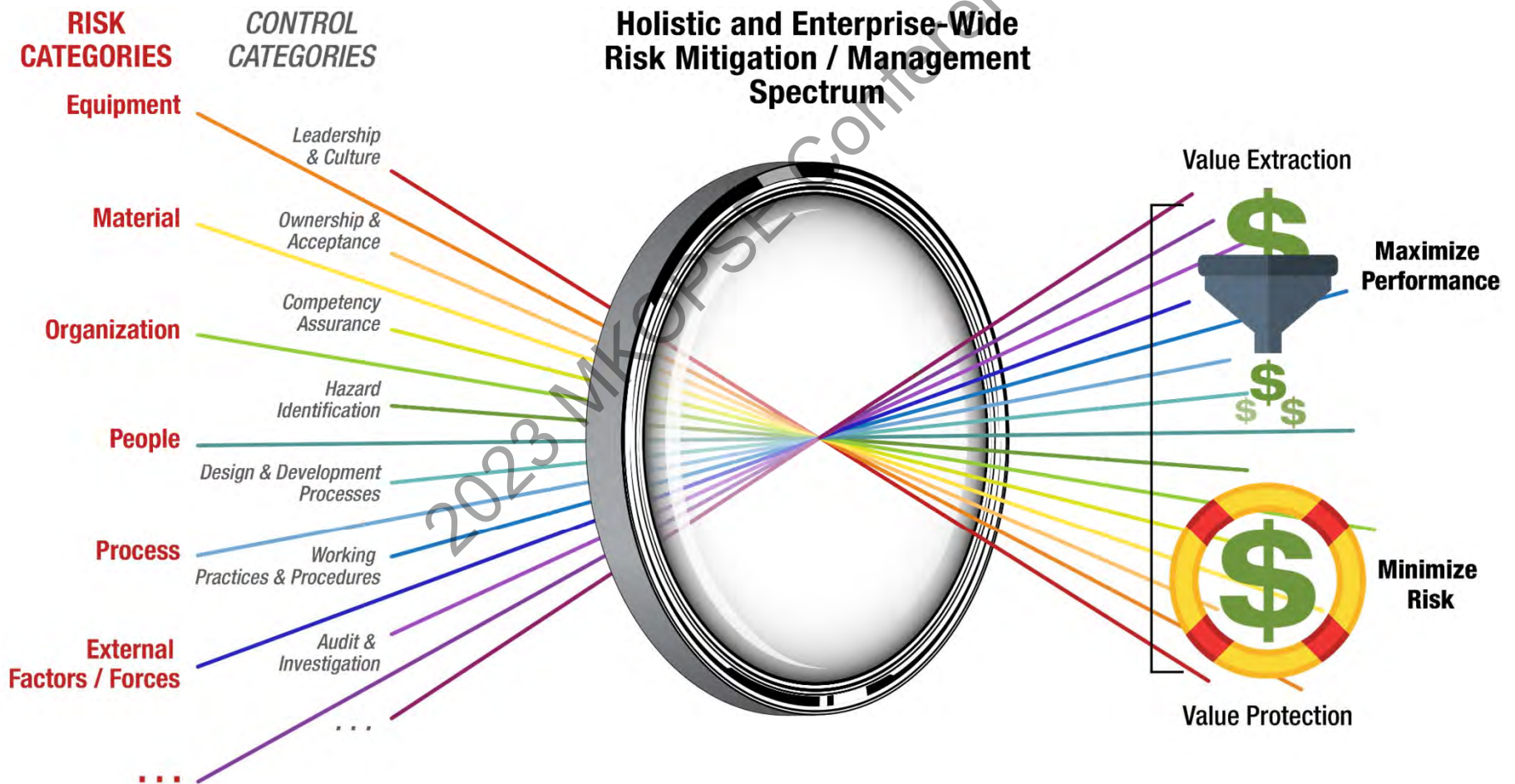
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Shift from "Safety" to "Risk Management"



Path Forward: Operational Risk

Path Forward: Enterprise Risk

- Manage all risks in a single environment with *common risk categorization*, including risks to achieving committed ESG targets.



Enterprise Risk

ENTERPRISE RISK DASHBOARD

Entity	Type	Category	Risk #	Event/Scenario	Discipline	Risk Status	Unmitigated Risk	Mitigated Risk	# of Mitigation Steps
HOU-FCCU	Asset Risk	Equipment Failure	20-RSK-0031	Runs between 3 year 1/A intervals	Inspection, Reliability	Closed	6	8	1
HOU-Maintenance Admin	Asset Risk	Equipment Failure	20-RSK-0032	Run regen to regen (6-8 months)	Inspection, Reliability	Closed	5	6	2
HOU-Reformer	Asset Risk	Equipment Failure	20-RSK-0033	Runs between 3 year T/A intervals	Inspection, Reliability	Closed	3	5	1
Houston Plant (HOU)	Facility Risk	Natural Disaster (Hurricane, Earthquakes)	20-RSK-0034	Infrastructure damage, plant damage, loss of containments leading to spill and consequence fire and explosion or contamination (wash up on shore), facilities possible.	Environmental, Asset integrity	Managing Recommendations	5	6	2

Artificial Intelligence

- Where are We Today?
 - Are We AI Enabled?
 - Do we have Data Scientists?
- What Problems are Worth Solving?
- What are Some Practical Examples?
- How good is your data?
 - Do you have enough data?
- What are Limitations / Challenges
 - Be Careful of Data Virtualization
 - Create a "Console"



Conclusion

- How easy is it for you to roll-up all elements of your PSM program digitally?
 - Do you have a single source of truth or do you have architectural limitations?
 - Do you need to aggregate and are you able to leverage data virtualization?
- Do you have a clearly defined sets of metrics?
- Do you have a sense of how to detect potential deviations that may lead to incidents?
- What is your risk tolerance and are you operating withing that constraint?
- What's your strategy for Process Safety Digitalization?

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Application of Natural Language Processing for Spill
Reduction in an Exploration and Production Company

26th Process Safety International Symposium

OPSE Conference



Speaker profile

- Jamison Chang, Risk Lead with Oxy
- 10 years' experience in process risk management in Upstream and CCUS segment
- B.S. in Chemical Engineering at Texas A&M University

2023 MKPSE Conference



Outline

- Spill Reduction Initiatives
- Process Safety Indicators
- Natural Language Processing
- Results

2023 MKORSE Conference



Spill Reduction Initiatives

- Why
 - Protect People and the Environment
 - Maintain production
- How
 - Identify bad actors, root causes
 - Predictive and proactive replacements



Process Safety Indicators

- API 754
- Spills may be Tier 1 or Tier 2 events
- Learn from events to mitigate higher-level consequences
- Corrective actions to improve performance

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Challenges

- Limited time and resources
 - Focus on higher-level consequences (e.g. Tier 1 PSEs)
- Data quality
 - Limited time for detailed reporting of spills
 - Free-text inputs
- Lagging indicators

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Natural Language Processing

- In computer science, NLP is the task of designing a system to take human text as input and “understand” some feature from it
- Entity extraction: From a text, identify the span related to a particular entity (e.g. leaks, dates, people, organization, etc)
- Two main approaches: Rule-based and machine learning
 - Rule-based: from a given set of rules to identify a leak we let the system find the span of the text where it matches any of the rules given
 - Machine learning: rules are learned from the data
 - There are pros and cons to both approaches



MI KPI Classification

- Goal: Identify leaks that can help focus mechanical integrity programs
- Challenges
 - Manual review of data
 - Look for keywords in different columns
- Opportunity to speed up data review and have timely results
 - Live data -> more accurate snapshot of MI performance

Leak Classification – MI KPIs



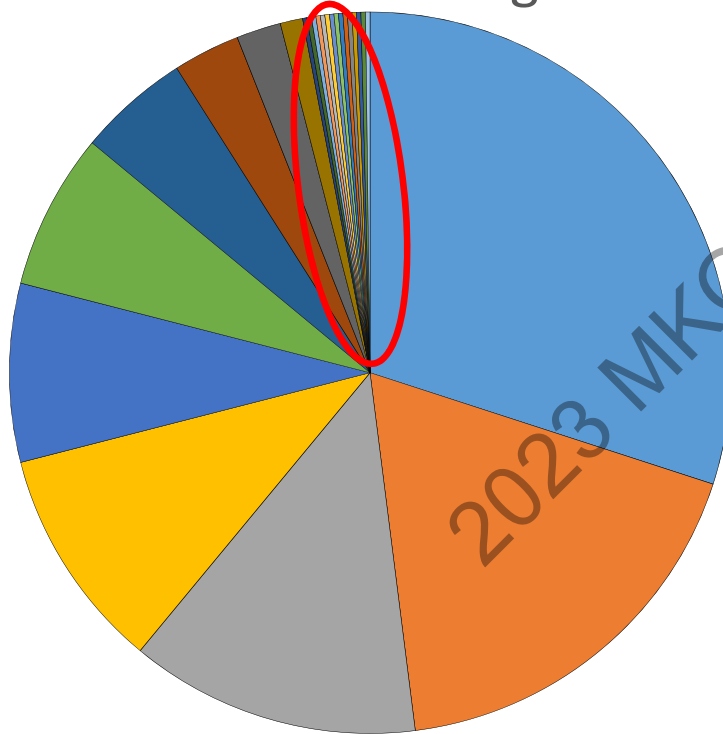


Results – MI KPI Classification

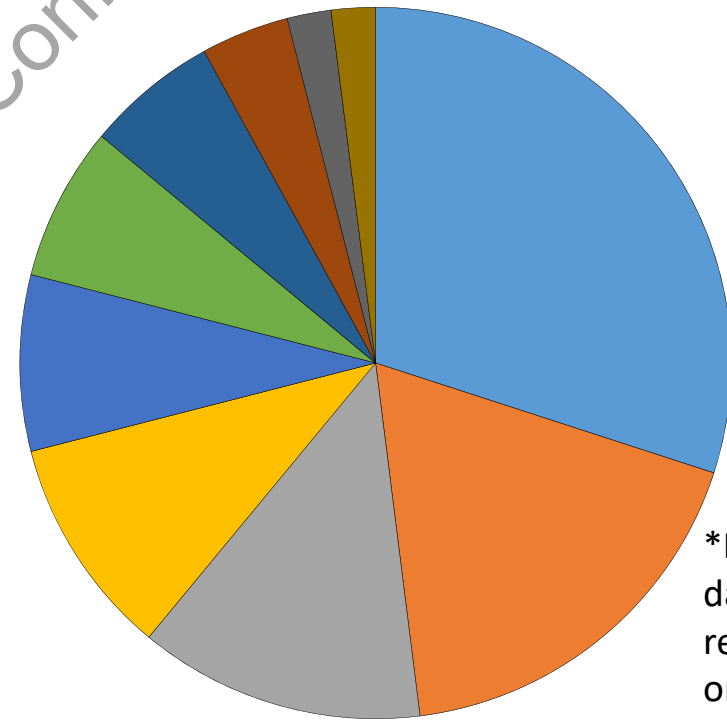
- Rule Based Approach
- Model had 90+% accuracy
 - Compared results with last 3 years of data
- Benefits
 - Save man-hours
 - Focus time on analysis
 - Expand ability to trend data, especially historical data

Cause of Leak – Rule Based Approach

Pre-Processing



Post-Processing



*Not actual data, for visual representation only



Cause of Leak Prediction – Machine Learning

- Problem: original leak report may not always have “cause of leak” identified
 - User may not know the cause or did not include
- Solution: Prediction based on other data in the report
 - Provide sample set
 - Either fully trained model or a few shot pre-trained model
 - Evaluate if model can determine a pattern
- Goals
 - More accurate analysis of trends by “filling in blanks”
 - Ability to validate previous user inputs

Natural Language Processing

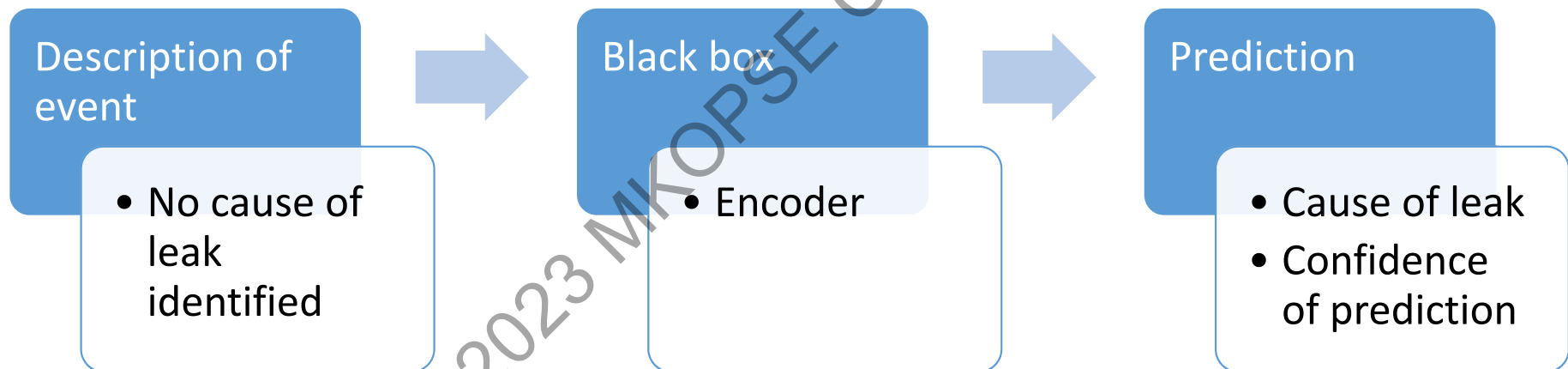
Training Example – cause of leak defined

- Description of event
- Equipment type
- Service type

Black Box

- Transformer model
 - Encoder-decoder
- Type of neural network
 - Architecture behind ChatGPT

Natural Language Processing

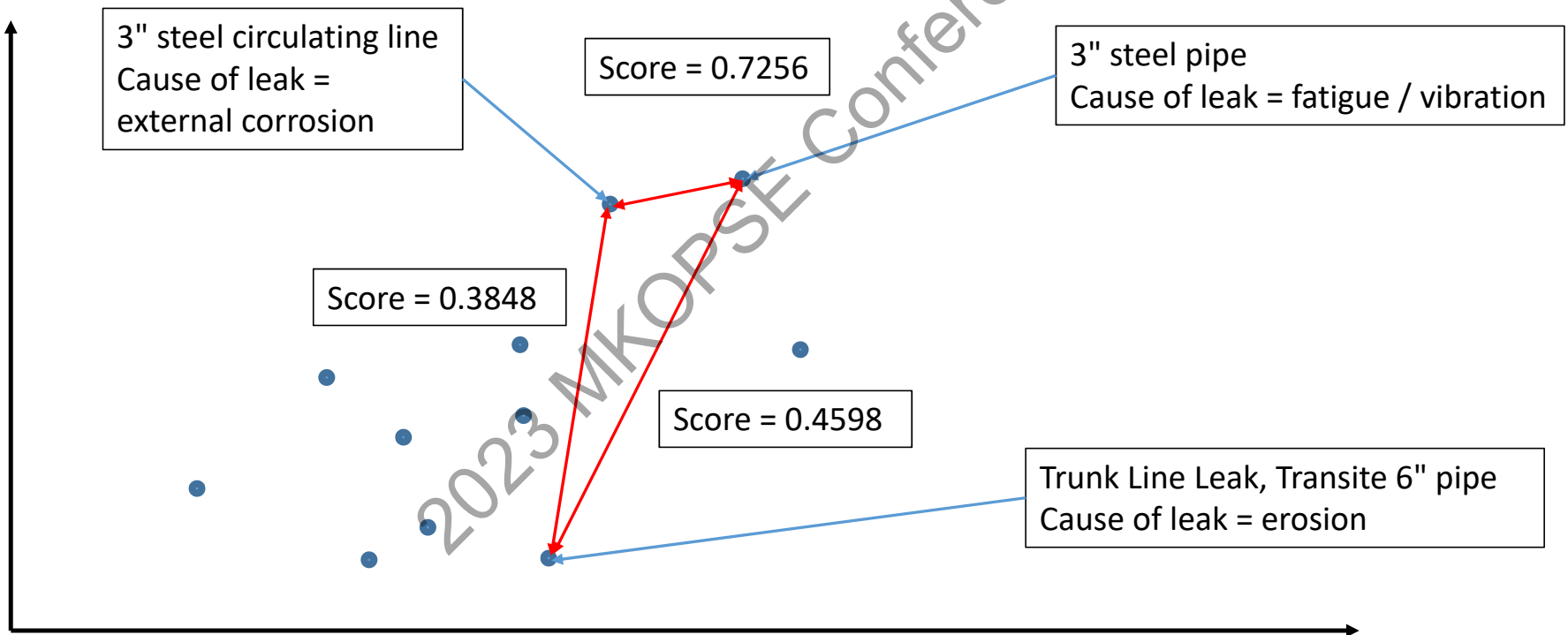




A Simple Machine Learning Approach

- Inputs would be leak report data (or any text)
- Assumption: Similar text inform common causes.
 - For a given corpus of text, if we've seen a similar text before, we may tag similarly.
- Goal: Given a new set of leak report data, without the cause of leak defined, find most "similar" set of data with semantically similar information to assign a cause of leak

Machine Learning Approach





Results - Cause of leak prediction

- Model with 54% accuracy out of 837 training cases
- Bias towards most common causes
- Advantage: using purely semantically similar sentences to assign the most probable cause
- Next steps: Model can be refined by using additional information from leak report to enrich the sentence we are encoding



Example Results

Cause	Long_Text	Best_Guess	Score	Correct
SEAL/PACKING	PACKING ON STUFFING BOX, BACKHOE/VAC TRUCK.	SEAL/PACKING	0.88	TRUE
INTERNAL CORROSION	2" Steel nipple	FATIGUE/VIBRATION	0.49	FALSE



Final Thoughts on Machine Learning Models

- These days, people use either public OpenAI models or models hosted on Azure or AWS; however, we should never disregard data privacy as a major security concern
- We used completely open-source locally hosted models to ensure data privacy; particularly when top state of the art models are not worth using when information is low to begin with
- Smaller models can perform just as well, and have full control of where data resides



Opportunities

- Focus on larger data set (e.g. Tier 2 events)
 - More representative data to analyze
- Communicate lessons learned more widely
- Quicker, more up-to-date analysis
- Improve data quality for human review (e.g. RCFA)



Future applications

- PSE classification – tier 1 / 2 / 3 / 4
- Tie with spill volumes data

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Acknowledgments

- Co-author: Jesus Martinez, Senior Analytics Engineer

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2023 Mary Kay O'Connor Safety & Risk Conference

Safe and Sustainable Energy Transition



Texas A&M Engineering Experiment Station

Mary Kay O'Connor
Process Safety Center

In Association with IChemE

October 11-13, 2023

Sponsored by **aramco**



26th Process Safety International Symposium



Fire Behaviour of Liquid Solvents by Cone Calorimeter

Gianmaria Pio*, Benedetta A. De Liso, Ernesto Salzano

Department of Civil, Chemical, Environmental and Materials Engineering – University of Bologna (IT)

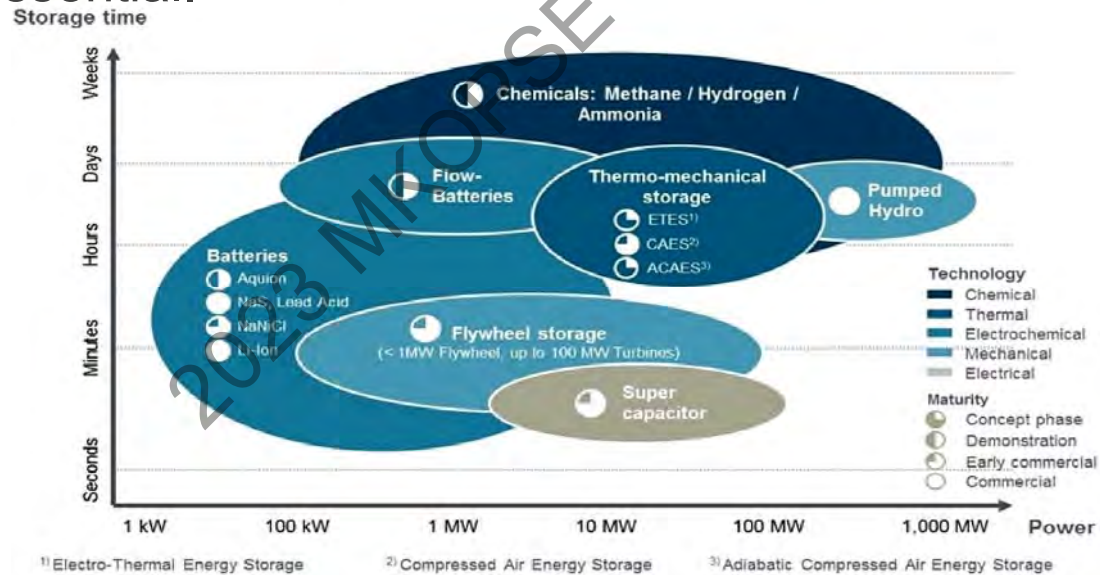
gianmaria.pio@unibo.it



ALMA MATER STUDIORUM
UNIVERSITÀ DI BOLOGNA

Introduction: Electrification in Chemical Industry

The energy transition is promoting the integration of storage systems in large-scale traditional processes, making the development of energy storage technologies essential.



¹ Electro-Thermal Energy Storage

² Compressed Air Energy Storage

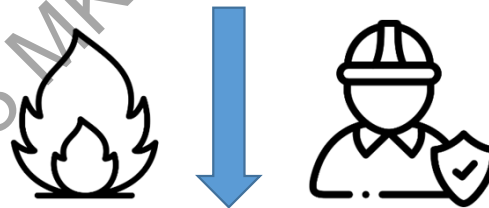
³ Adiabatic Compressed Air Energy Storage

Introduction: New Challenges in Fire Safety

Several energy storage technologies using non-aqueous solvents have been recently developed, introducing new challenges in industrial safety.

Among possible scenarios, runaway and pool fire are of concern.

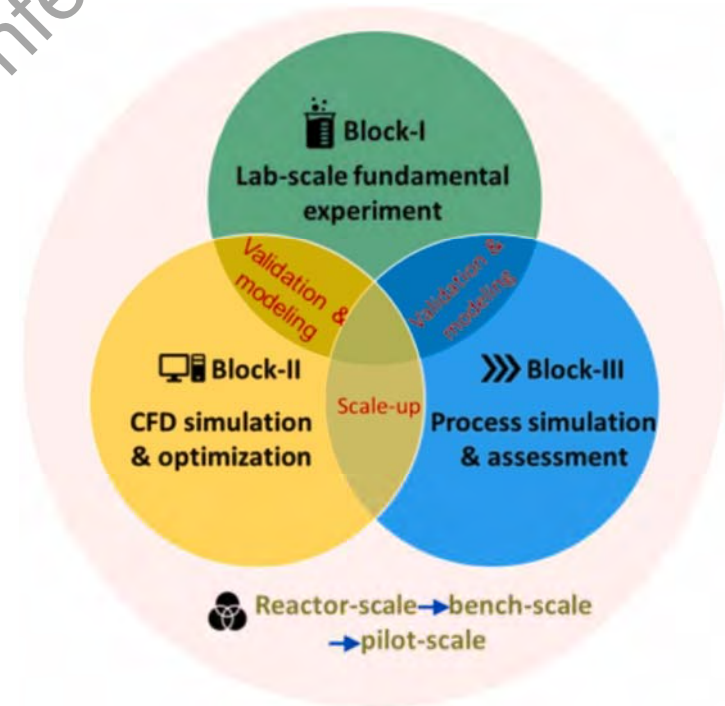
Different parameters have a significant impact on fire-related phenomena and thus macroscopic properties.



Standardized procedures to determine the safety parameters are essential

Introduction: New Challenges in Fire Safety

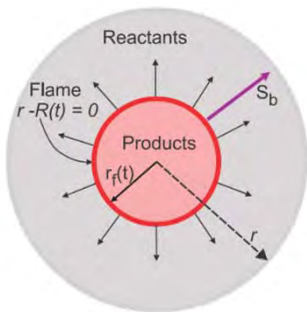
- The need for sustainable technologies introduced alternative solvents, requiring the characterization of physic-chemical behaviour under fire conditions.
- The experimental approach shall be preferred to characterize innovative solutions
- The experimental systems shall be selected to allow a robust validation of numerical models



Introduction: New Challenges in Fire Safety

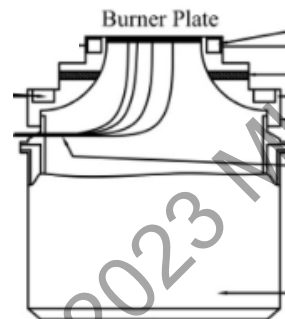
The overall reactivity and the composition of exhaust gases shall be considered as the main targets for an experimental campaign.

Spherical Vessel

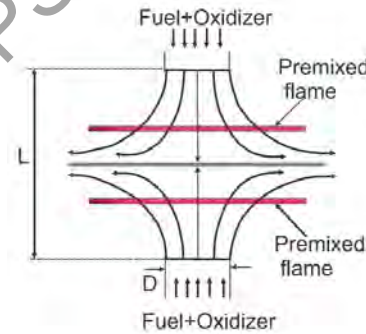


Evaporation needed

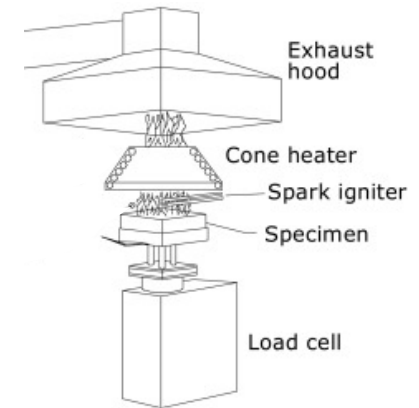
Heat Flux Burner



Counter Flow Flame



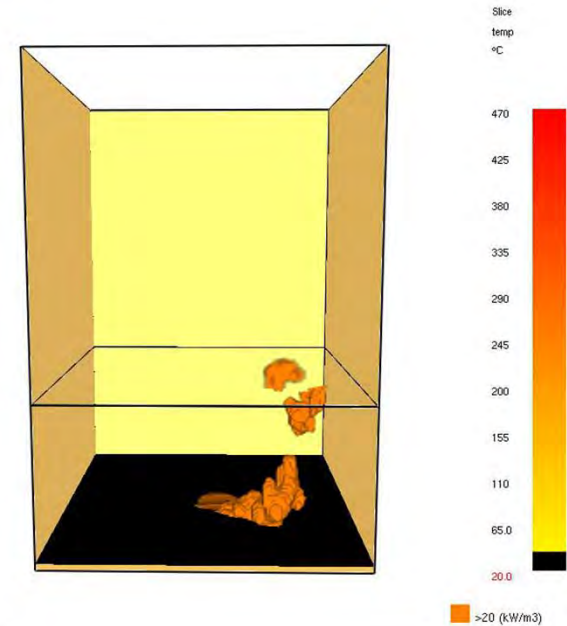
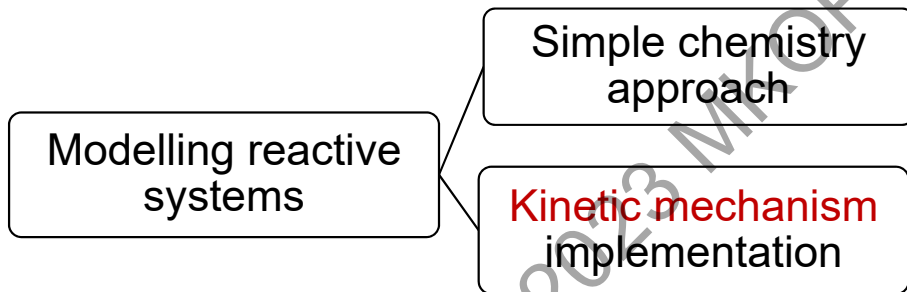
Cone Calorimeter



Standardized for solids

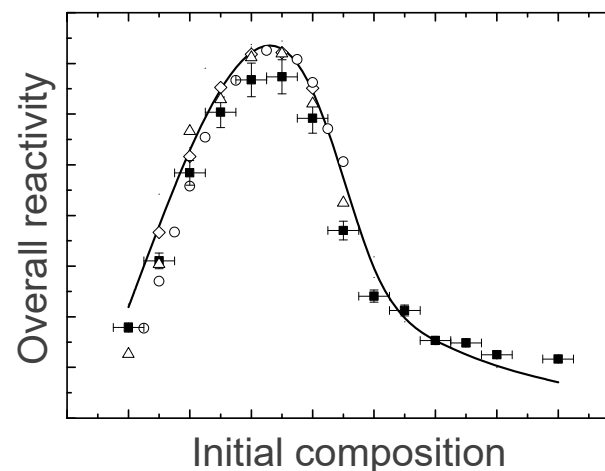
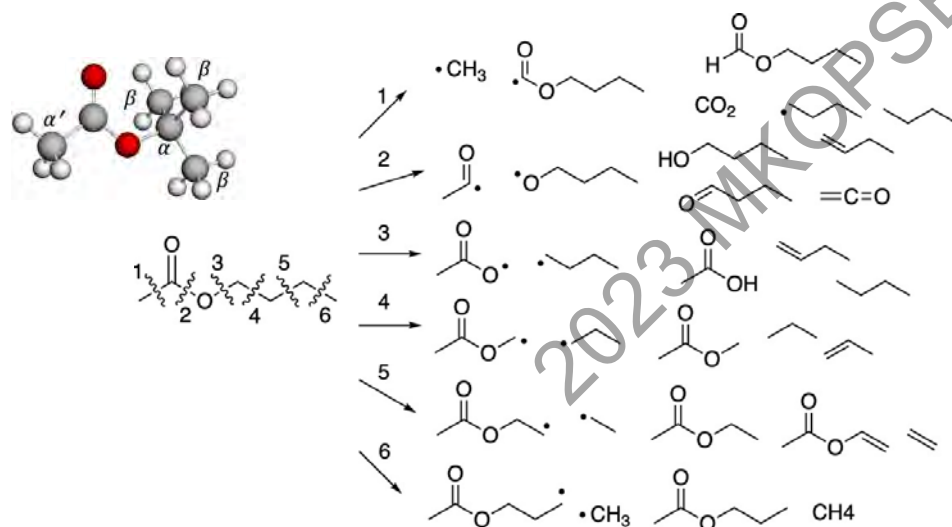
Introduction: New Challenges in Fire Safety

The data potentially obtained from experimental campaigns can be compared with numerical estimations deriving from computational fluid dynamics having different chemical submodels.

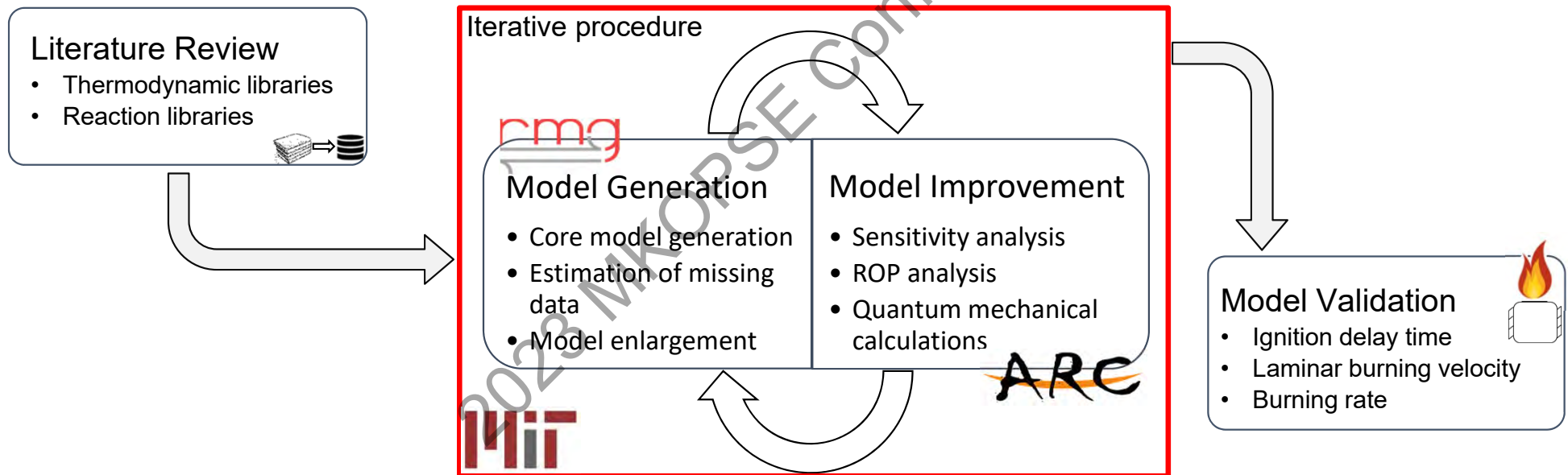


Introduction: New Challenges in Fire Safety

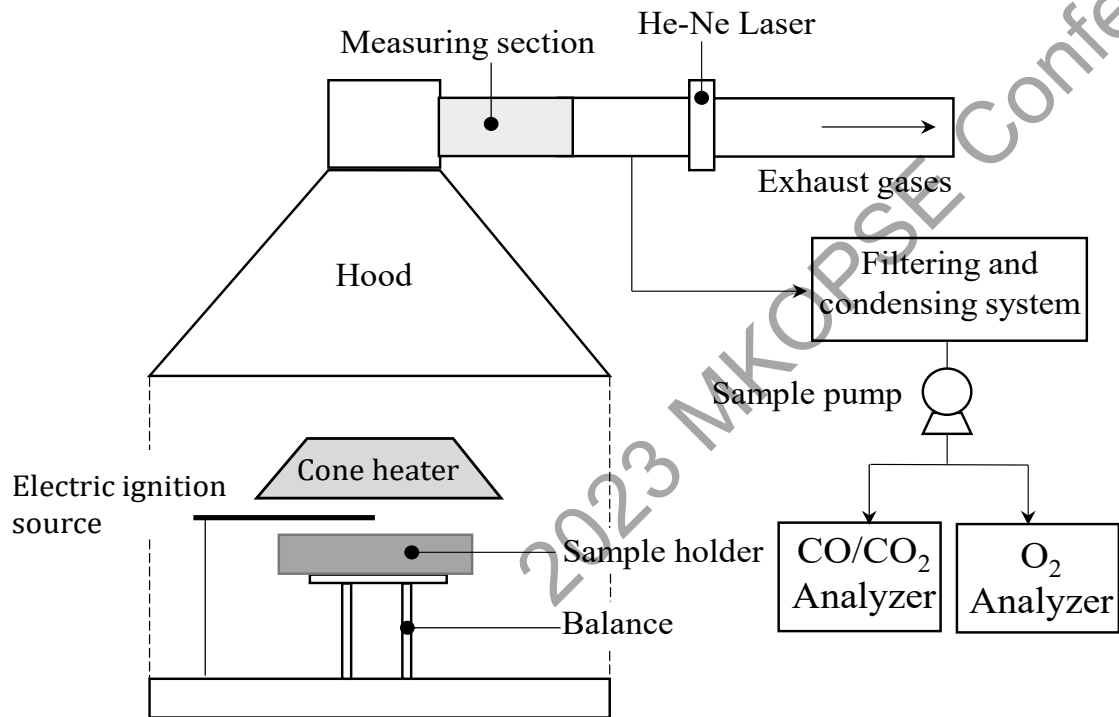
The use of a detailed kinetic mechanism allows for the identification of possible products, the quantification of the reactivity, and the exhaust composition in a wide range of temperature, pressure, and composition.



Introduction: New Challenges in Fire Safety



Methodology: Cone calorimeter



Direct output

- Heat flux [kW/m^2]
- Ignition time and extinction time [s]
- Specific extinction area [m^2/kg]
- CO₂ yield [kg/kg]
- CO yield [kg/kg]
- Heat release rate [kW/m^2]
- Smoke production rate [m^2/s]
- Mass loss, Mass loss rate [g, g/s]
- Effective heat of combustion [MJ/kg]
- Total oxygen consumption [g]

Methodology: Tested Materials and Conditions

Component	T_a [°C]	T_F [°C]	T_B [°C]	k_L [W/(mK)]	ρ_L [g/m ³]
Acetonitrile	523.9	5.5	81.6	0.120	777
Ethyl Acetate	426.7	-4.0	77.2	0.193	894
Lactic Acid	> 400	110.0	216.0	0.144	1200
Hexane	224.0	-23.0	68.9	0.203	656

- Autoignition temperature (T_a)
- Flash point temperature (T_F)
- Bubble point temperature (T_B)
- Thermal conductivity (k_L)
- Density of the liquid solvent (ρ_L)

Sample surface [m ²]	0.01
Sample thickness [m]	0.01
Distance from cone heater [m]	0.025
Heat flux [kW/m ²]	7 – 50
Initial mass [kg]	0.050 – 0.055
Cone heater orientation	Horizontal

Methodology: Derived Parameters

Heat Release Rate = HRR

Peak of Heat Release Rate = pHRR

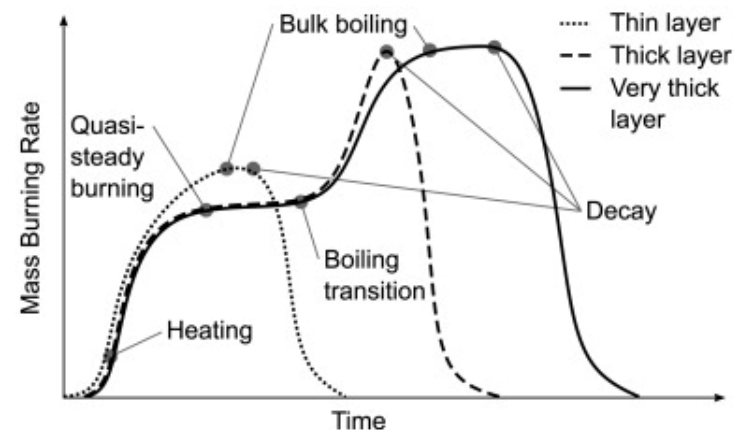
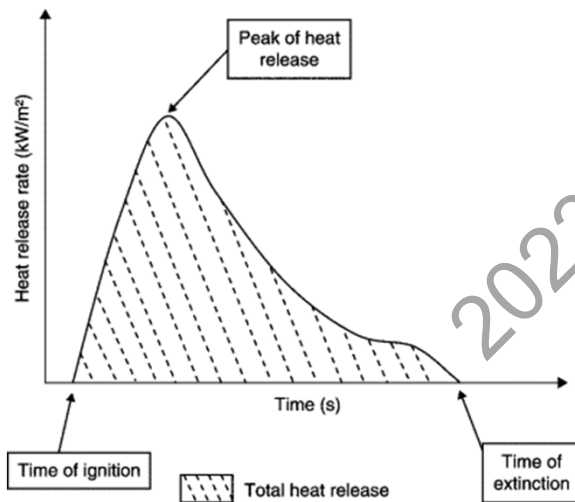
Time of Peak in Heat Release Rate = tpHRR

Mass Loss Rate = MLR

Peak in Mass Loss Rate = pMLR

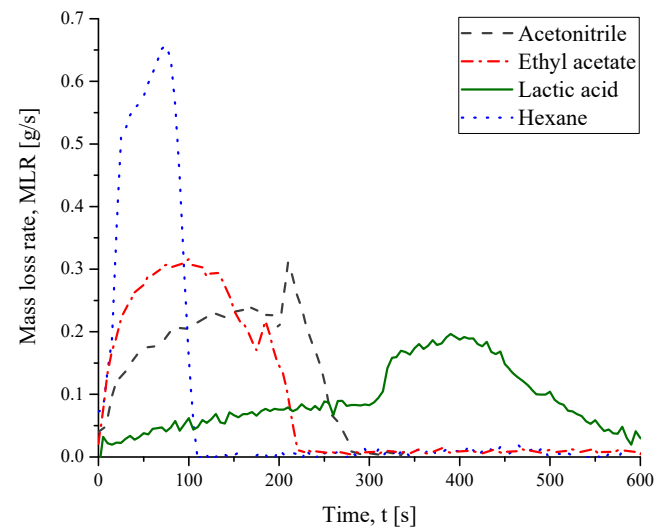
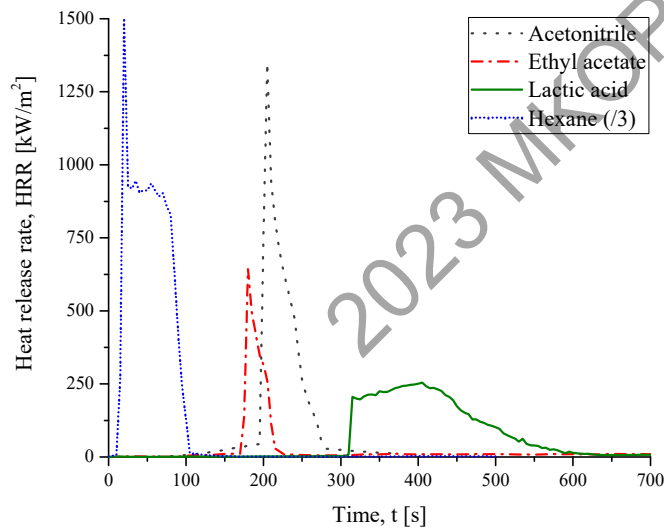
Overall Reaction Rate = ORR = $\frac{MLR}{Area \cdot Density}$

Peak in Overall Reaction Rate = pORR

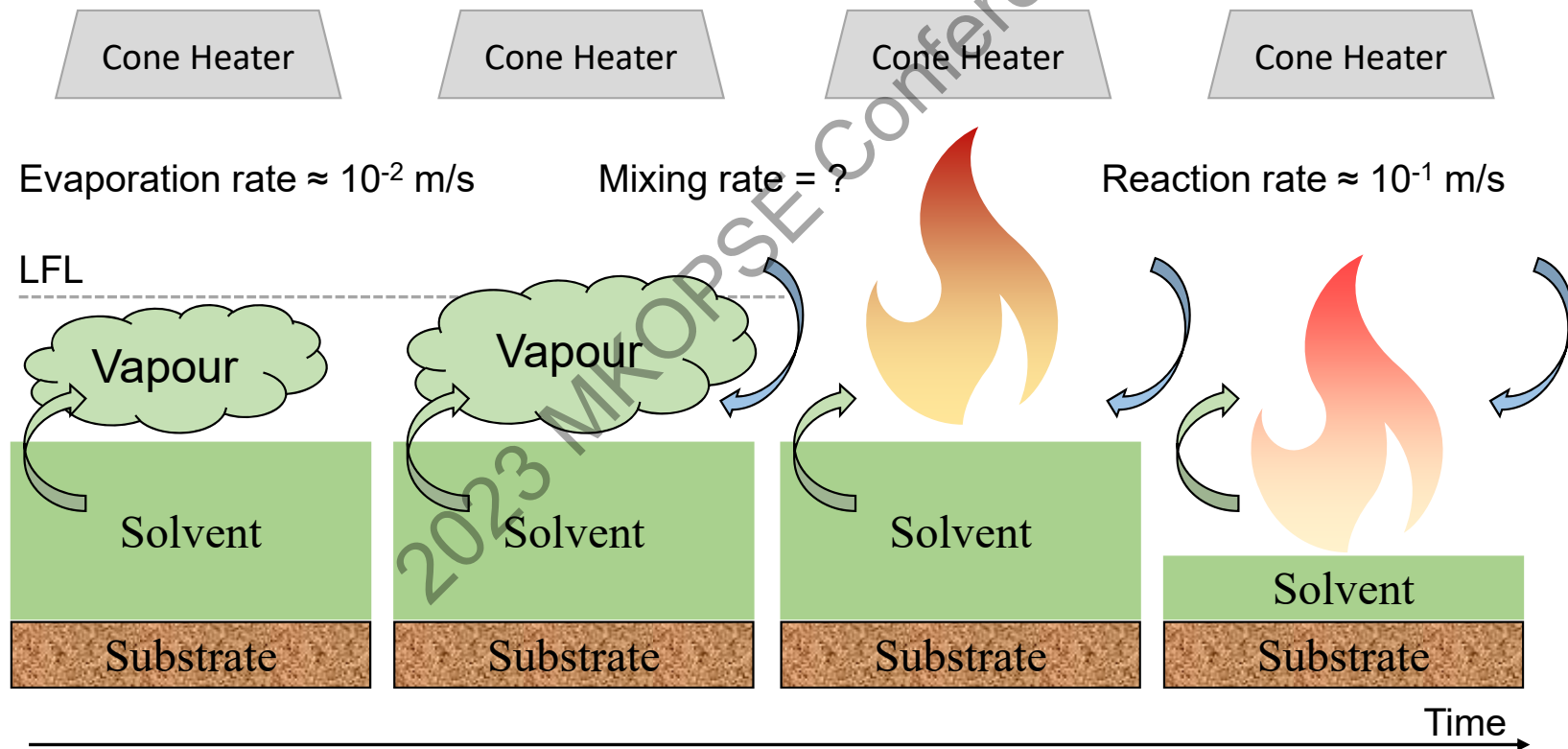


Results: Base Case Scenario (25 kW/m²)

- ❑ Hexane and ethyl acetate show a thin layer behaviour with different heating time
- ❑ Acetonitrile has a thick behaviour and lactic acid a very thick
- ❑ Mass decay does not correspond to the peak of Heat Release Rate

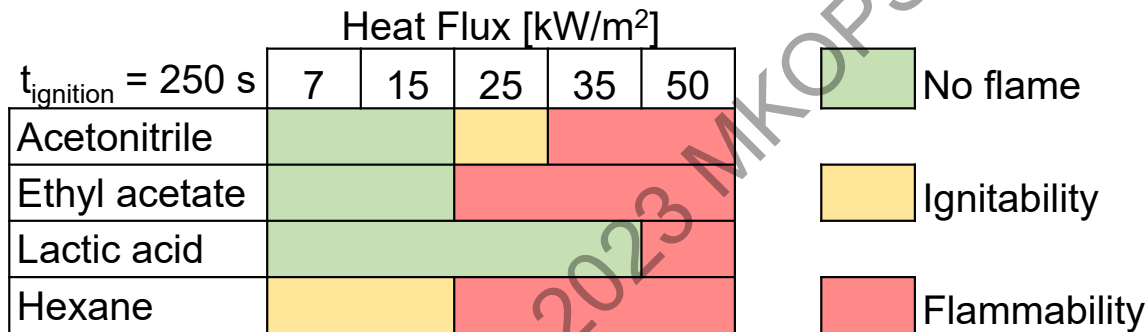


Results: Observed Stages and Characteristic Time



Results: Heat Flux and Observation Time

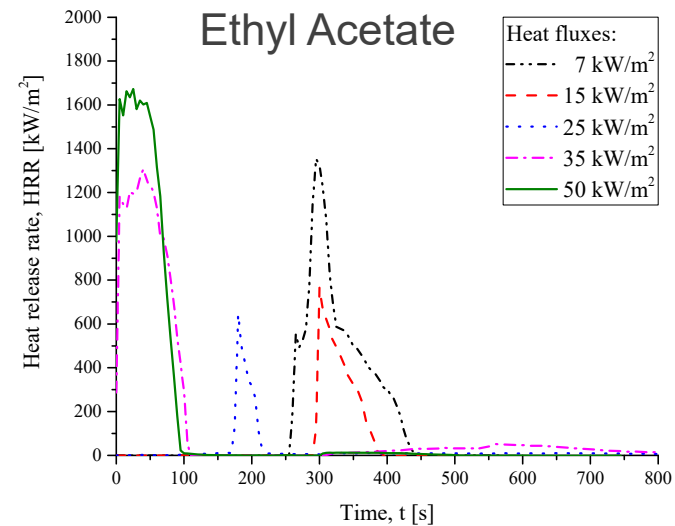
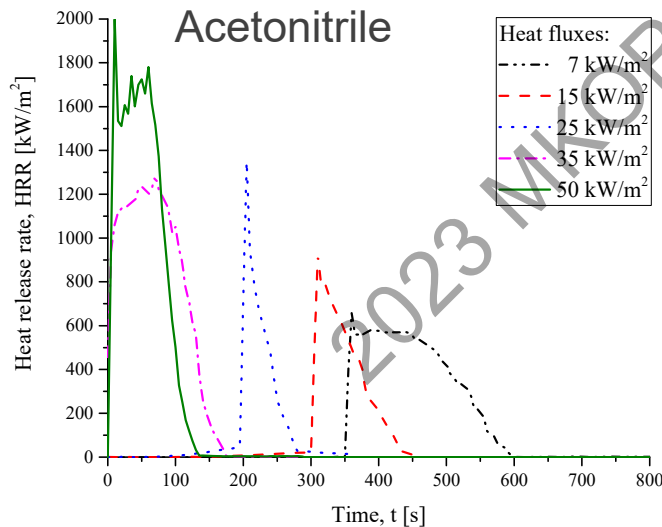
According to the obtained characteristic times and pORR, mixing is identified as the rate-determining step



Component	Heat flux [kW/m ²]	pORR ($\cdot 10^{-5}$) [m/s]
Acetonitrile	7	0.98
	15	1.41
	25	1.82
	35	3.89
	50	4.68
Ethyl Acetate	7	1.56
	15	1.76
	25	1.14
	35	3.38
	50	3.20

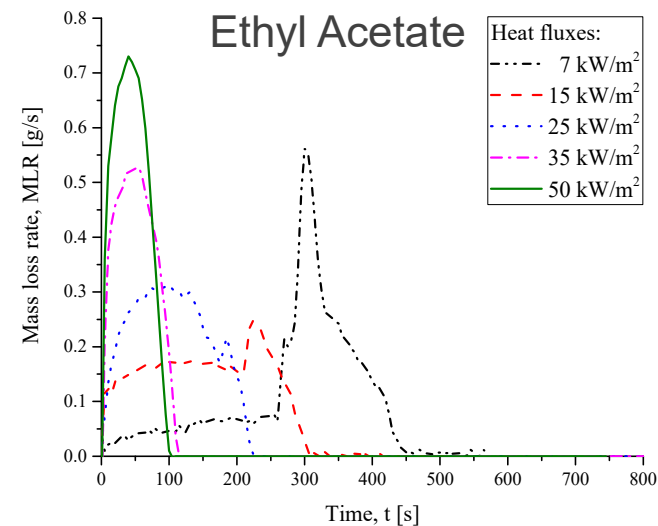
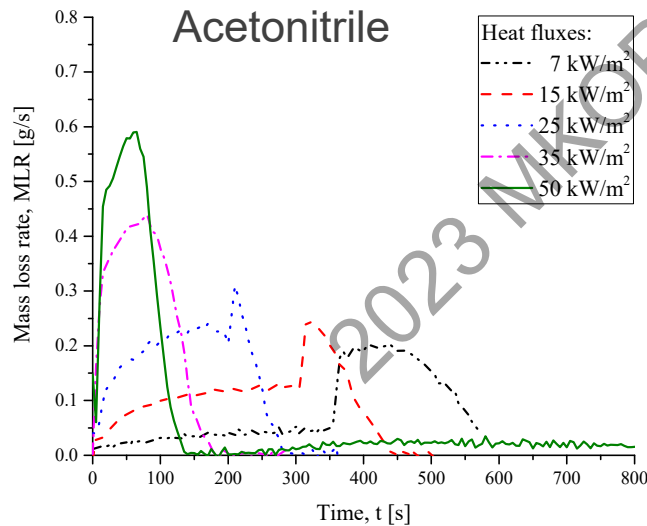
Results: The Effects of Heat Flux

- Increasing the heat flux, Acetonitrile shows a decrease in t_{pHRR} and $pHRR$
- Ethyl acetate at 7 kW/m^2 is affected by the given ignition (ignitability)



Results: The Effects of Heat Flux

- ❑ The heat flux provided affects the liquid behaviour (from thin to thick layer)
- ❑ Uncomplete conversion can be observed for acetonitrile only



Conclusions & Future Developments



Experimental determination of the flame characteristics of liquid solvents



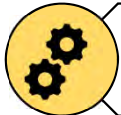
Assessment of the chemical and visible features of a solvent-derived flames



Comparison of safety performances of different solvents exposed to fire and under a wide range of boundary conditions (e.g., heat flux, distance, thickness)



Identification of the most critical conditions and phenomena characterizing the analysed scenario



Realization of a robust and standardized procedure to characterize the sustainability of solvents

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Process Safety Center
Texas A&M Engineering Experiment Station



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<https://site.unibo.it/lises/en>



LISES – Laboratory of Industrial Safety & Environmental Sustainability

The staff of the laboratory of industrial safety and environmental sustainability is engaged in edge-cutting research on chemical and process safety, risk assessment and management, sustainability assessment and environmental management of industrial processes, also addressing the development of new technologies.

Acknowledgments

Authors gratefully acknowledge the Italian Ministry of University and Research (MIUR) for the financial support through the project “Dipartimenti di Eccellenza 2018-2022” and the National Recovery and Resilience plan (PNRR), Extended Partnership PE2: NEST – Network 4 Energy Sustainable Transition”, Spoke 6: Energy Storage - - T6.4.4 Safety, LCA and sustainability studies of energy storage systems and processes.



Piano Nazionale
di Ripresa e Resilienza

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Process Safety Culture in Research Centers. Road Map Toward Enhancement



[Abstract](#)

Hesham K. Al-Subait

aramco

2023 MKOPSE Conference

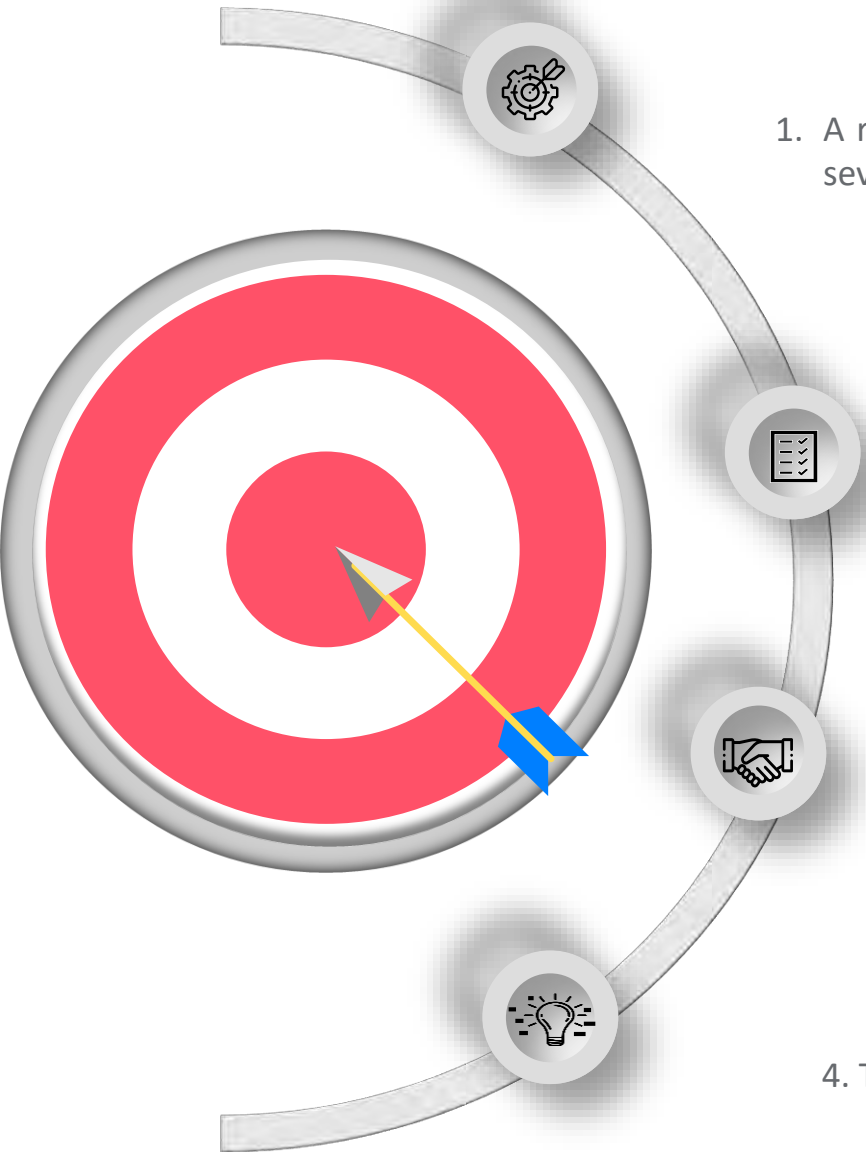
Abstract Summary

Process Safety Culture in Research Centers. Road Map Toward Enhancement

Process Safety culture enhancement in a research center requires a systematic and comprehensive approach to ensure that all aspects of the organization's operations are aligned with its safety goals. Here are some steps to enhance process safety culture in a research center:

1. **Assessment:** Conduct a process safety culture assessment to identify strengths and weaknesses in the existing safety culture of the organization. The assessment can be used to identify areas requiring improvement in communication, training, and workforce involvement in safety issues.
2. **Leadership commitment:** The management of the research center should demonstrate their commitment to process safety culture improvement and encourage employee participation in safety-related activities.
3. **Employee involvement:** Encourage employees to be more involved in the safety management process by including them in decision-making processes, hazard identification, and risk assessments.
4. **Training and Development:** Train employees in process safety management principles and ensure that they understand the importance of safety in the workplace. Refresher training can be conducted on a regular basis to help maintain the culture of safety.
5. **Two Way Communication:** Ensure that employees receive clear and concise safety-related information. Consider ways to use posters, meetings, and email communications to emphasize safety culture to employees.
6. **Continuous improvement:** Establish systems to track progress and identify opportunities for improvement in process safety culture. Regularly engage stakeholders, review data, conduct audits, and conduct periodic assessments to identify areas that need attention.

Why do we need PS Culture Enhancement?



1. A recent in-depth internal analysis-2019 / and 2020 SMS internal review has revealed several PS improvement opportunities namely around:

- the level of engagement and commitment of employees to HSE,
- the need to enhance PS core competencies,
- the need to focus on pro-active risk discovery and mitigation,
- the need to enhance the current SMSs/OEs audit mechanism and
- increasing the ownership by all of our SMS .

2. Despite substantial improvement in PS overall performance between 2019 and 2020 led by STTF team , recent incidents and near misses have generated a sense of urgency to steeply increase risk management effectiveness across the Dept.

3. As part of Major Safety Goals established in the Safety Annual Letter for 2021, Strengthen of Safety Culture as an overall has been targeted by implementing a series of activities and communications across the department to reinforce our unmistakable commitment to safety and excellence.

4. This has resulted in deciding to form a Major **Safety Enhancement Culture Committee** sponsored by Head of the Organization.

Expected Outcome



Assessing the key PS risk from operating, maintaining and modifying existing Assets (Pilot Plants, Labs, Facilities, etc.)



Development of specific Mitigation Plans following targeted in-depth risk assessments



Increase ownership on SMS Expectations in SMS Element Champions and Process Owners



Support the implementation of risk management in the field through an appropriate set of tools and KPIs.



Support the delivery of enhanced competencies and functional SMS ownership and understanding, and skills on process safety throughout the department and leadership in particular.

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Process Safety Management in the Semiconductor Industry



Expanding horizons through innovation and progress

Samsung Austin Semiconductor is a world-class technology leader with 25 years of storied history in the Central Texas area. We're breaking barriers with help from outstanding employees.

SAMSUNG
AUSTIN SEMICONDUCTOR



Zero Harm Habits



Bio: Mike Stone

- BS Chemical Engineering from the South Dakota School of Mines and Technology
- 10 years Halliburton
 - Wireline Field Engineer
 - Performance Development Coordinator
 - Logistics Manager
- 6 months Upstream Brewing
 - Brewer and expert beer taster
- 4 years Green Plains
 - PSM Engineering Manager
- 2 years Samsung
 - Sr. Engineer PSM/ RMP



By the Numbers

Samsung Austin Semiconductor saw massive growth in 2022. These numbers are just a snapshot of the impact we're having on the community.



- Received Zero Waste to Landfill Gold level validation for recycling or reusing 97% of waste
- Powered by 100% renewable energy



- Investment in Austin facility since 1996



- Plus 9,935 additional workforce (includes on-site vendors, partners and contractors)



- Total economic impact in Central Texas in 2022 (includes Taylor construction site)



- \$400,000 in charitable giving by employees
- \$1.5 million in corporate giving

What is a semiconductor chip?



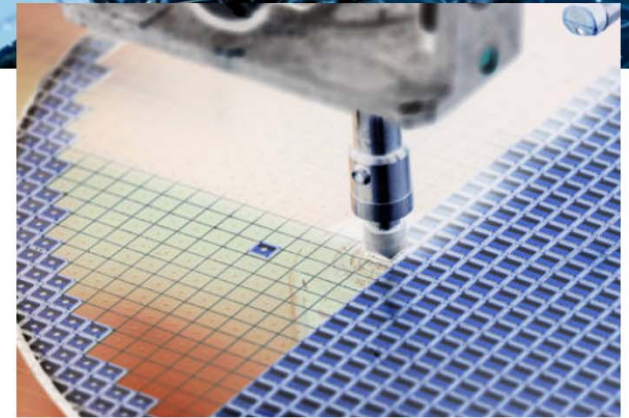
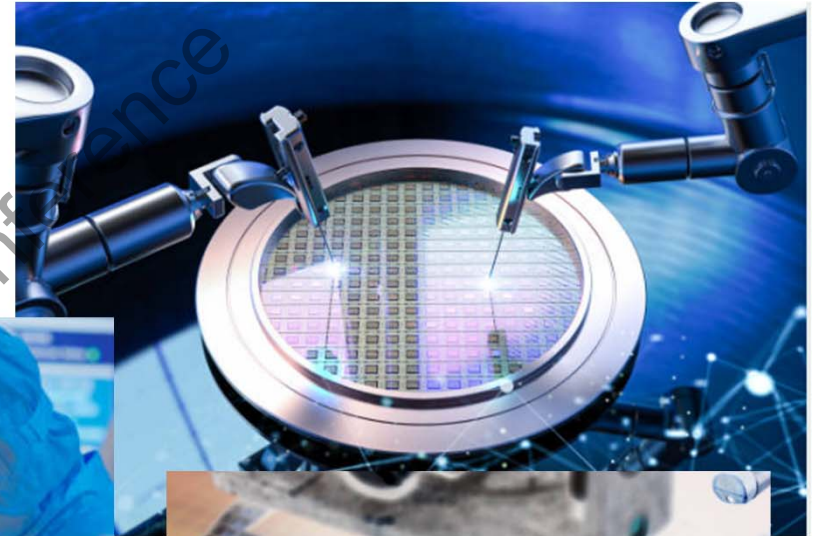
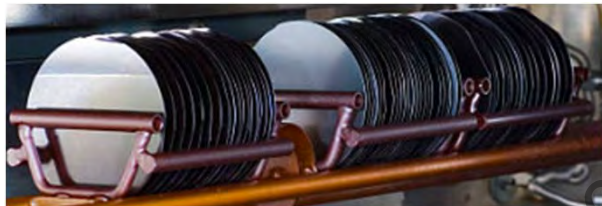
“Semiconductors are the brains of modern electronics, enabling advances in medical devices and health care, communications, computing, defense, transportation. Clean energy, and technologies of the future such as artificial intelligence, quantum computing, and advanced wireless networks.”



Semiconductor Chip Manufacturing in 8 Simple Steps

<https://semiconductor.samsung.com/emea/news-events/tech-blog/a-short-introduction-to-semiconductor-fabrication/>

1. Build the silicon wafer
2. Imprinting the Integrated Circuit
3. The Etching Process
4. The Thin Film Process
5. The Metal Interconnect Process
6. The EDS Process
7. Packaging
8. Testing



Incidents in the Semiconductor Industry

2011 Intel Chandler, Arizona

- Leak of Nitrogen Trifluoride
- 43 treatments and 12 hospitalizations
- Result of an O-ring failing in the gas exhaust system

<https://bit-tech.net/news/tech/cpus/intel-chemical-leak/1/>



OSHA PEL 8-hour TWA (ST) STEL (C) Ceiling Peak	
PEL-TWA	10 ppm (29 mg/m ³)
PEL-STEL	
PEL-C	
Skin notation	N



Incidents in the Semiconductor Industry

2013 SK Hynix Wuxi, China

- 1 minor injury
- Halted production of half the foundry for 6 months
- Result of installation of new equipment
- \$1 billion in damages

<https://www.computerworld.com/>



Incidents in the Semiconductor Industry

2013 Samsung Hwaseong, South Korea

- 1 fatality
- 10 L diluted HF acid leaked
- Likely resulted from a damaged gasket

<https://theseoultimes.com>



Process Safety Management

“Process safety management (PSM) is addressed in specific standards for the general and construction industries. OSHA's standard emphasizes the management of hazards associated with highly hazardous chemicals and establishes a comprehensive management program that integrates technologies, procedures, and management practices.” – OSHA

14 Elements

- Employee Participation
- Process Safety Information
- Process Hazard Analysis
- Operating Procedures
- Training
- Contractors
- Pre-Startup Safety Review
- Mechanical Integrity
- Hot Work
- Management of Change
- Incident Investigation
- Emergency Planning and response
- Compliance Audits
- Trade Secrets



PSM Boundary in Manufacturing



Chemical Manufacturing



Oil and Gas

PSM Boundary in the Semiconductor Industry

- Specifically challenging that the standard was not written to include unique processes used within the semi-conductor industry.
- Small quantities of the chemical used after the bulk distribution system.
- Highly specialized tools with built in controls and interlocks to prevent potential incidents.
- Fast paced manufacturing environment with processes that are installed and uninstalled within a relatively short time period due to new process designs.
- Limited experience with PSM applicability within the industry.
- Various interpretations of PSM coverage applicability.
- Tool level coverage creates a significant financial and resource allocation burden that could cripple operations.



Jim Testo, CSP, CIH
Ashley Moll

Process Safety Management & the Semi-Conductor Industry

Greystone Risk Management - <https://sesha.org/wp-content/uploads/2019/11/Greystone-PSM-Presentation.pdf>



Azko-Nobel Chemicals – Limits of a Process 1997

In this case, the company does not dispute it has a covered process, as defined by 29 CFR 1910.119. However, what is disputed is the limits or the boundaries of the process downstream from the equipment the company stipulates is part of the covered process. The company contends that interconnected equipment downstream from what it stipulates as the covered process should not be included in the boundaries of the covered process. The company contends there is no circumstance, i.e. deviations, upsets, releases, etc., which might occur downstream (outside) from the stipulated covered process, which could affect a catastrophic release of HHC in the upstream stipulated covered process. Therefore, the company contends that since there is no potential for a catastrophic release of a HHC, those downstream aspects should be considered as being outside the limits or boundaries and should not be considered as part of the covered process.

It is OSHA's position that this issue can be resolved through the following analysis: Employers must determine:

- 1) the extent of process(es) by utilizing the definition of process [1910.119(b)] which includes any vessels which are connected and separate vessels located such that a HHC could be involved in a potential release. Engineering and administrative controls required by the PSM standard to prevent catastrophic release of a covered HHC may not be used to determine the extent of a process as defined in paragraph 1910.119(b). This interpretation is predicated on the assumption that an event such as an explosion will take place in the process notwithstanding such controls;
- 2) determine whether the process contains at any particular time a threshold quantity (TQ) or greater amount of a PSM HHC. If so, the process is covered by the PSM standard; and
- 3) consider each aspect of the process as defined to determine the extent of PSM coverage for each particular aspect. Aspects of the process which contain a HHC would be covered by all PSM elements, such as information, process hazard analysis and mechanical integrity. Aspects which do not contain HHC, but are interconnected or located nearby are part of the process. Such aspects may or may not be covered by the PSM standard based on whether the particular aspects could cause a HHC release or interfere with mitigating the consequences if there was a HHC release. If the particular aspects do not contain a HHC but could cause a HHC release or interfere with mitigating the consequences of a HHC release, then based on the employers analysis, various elements of PSM would apply to these aspects;

If based on this analysis, it is determined that interconnected equipment downstream from the stipulated covered process cannot cause a HHC release or interfere with the mitigation of the consequences of a HHC release, and the equipment does not itself contain a TQ or greater amount of a HHC, then such equipment could safely be considered outside the limits or boundaries of the covered process.

OSHA intends that the PHA be an objective verification to ensure that the process, as determined by the employer (using steps including #1 through #3 above) is managed in accordance with the requirements of the PSM Standard.

Paragraph 1910.119(l) process safety management of changes are anticipated over the service life of the process. Aspects of the process impacted by a change must be reevaluated to determine the extent to which they are covered by the PSM standard. Of concern is that aspects could be removed from further consideration by an earlier evaluation of the process if the extent of the process was determined other than described above. As a consequence of a change, an overlooked aspect could contribute to the cause of a catastrophic release or interfere with mitigating the consequences if there was a HHC release.



Azko-Nobel Chemicals – Limits of a Process 1997

Employers must:

- Determine the extent of the process such that a HHC that could be involved in a potential release
 - Administrative and Engineering Controls can't be used to make the determination
- Determine if the process has a TQ or greater of PSM HHC
 - If so, it is covered by PSM
- Consider each aspect of the process to determine the extent of the PSM coverage

AkzoNobel

Based on the above determination:

- The interconnected equipment downstream cannot cause a HHC release or
- Interfere with the mitigation of the consequences of a HHC release
- The equipment itself does not contain a TQ or greater of amount of HHC
- Not PSM
- Verified by conducting a PHA



Key Take Aways

- Making Semiconductor chips is a long, complicated, expensive and hazardous process
- OSHA regulates many of the chemicals used in Semiconductor manufacturing
- Each employer should determine the PSM boundary for their process
- OSHA responded to Azko-Nobel Chemicals and laid out the rules for determining the PSM boundary
 - Determine where the process no longer has a HHC TQ
 - Confirm the boundary with a PHA



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**Thank
you!**



2023 Mary Kay O'Connor Safety & Risk Conference

Safe and Sustainable Energy Transition

In Association with IChemE and C-RISE

October 11-13, 2023

Session 82: Safety First: Innovative Advanced Analytical and Automation Solutions For Improving Safety

Doug White
Emerson Automation Solutions

26th Process Safety International Symposium




Texas A&M Engineering Experiment Station

Mary Kay O'Connor
Process Safety Center



2023 Mary Kay O'Connor Safety & Risk Conference
26th Process Safety International Symposium

In Association with IChemE

Sponsored by aramco 



Mary Kay O'Connor
Process Safety Center
Texas A&M Engineering Experiment Station

Doug White (doug.white@emerson.com)
Principal Consultant
Emerson Automation Solutions

Background: Many years of experience designing, justifying, installing and commissioning advanced real time modeling, optimization, digitalization and automation applications in the process industries and assessing their impact on safety, sustainability and profitability.



Safety Moment: Safety on the Stairs



- Most of us use stairs everyday at home and work without thinking about the risk.
 - Falls are the most common incident reported at both home and work.
 - Over 1 million Americans are treated for fall-related injuries every year.
 - Estimated medical costs for falls in 2015 was \$50B
- Take care to stay safe on the stairs:
 - Use the handrail
 - Avoid distractions like texting, conversation or reading
 - Walk, not run
 - Take one step at a time
 - Get help or use the elevator if moving things
 - Wear good footwear
 - Clear up spills when observed

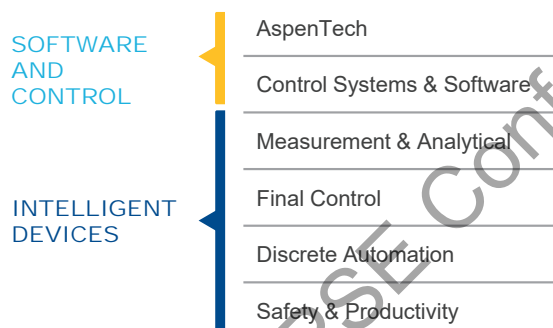
Emerson At-A-Glance

(Continuing Operations)

COMPANY PROFILE

Emerson is a global leader in automation technology and software. We help customers in critical industries, like energy, chemical, power and renewables, life sciences and factory automation operate more sustainably while improving productivity, energy security and reliability.

BUSINESS SEGMENTS

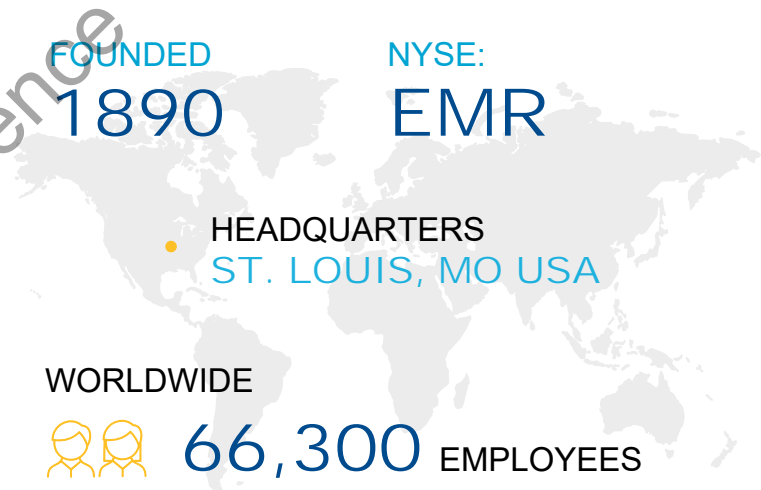


\$13.8 BILLION

GLOBAL NET SALES FY 2022

FOUNDED
1890

NYSE:
EMR



WORLDWIDE

66,300 EMPLOYEES

130 MANUFACTURING LOCATIONS

2022 RECOGNITIONS

TOP 50 EMPLOYERS
Woman Engineer Magazine

WORLD'S BEST EMPLOYERS
Forbes Magazine

INDUSTRIAL IOT COMPANY OF THE YEAR
IoT Breakthrough



CONSECUTIVE YEARS OF INCREASED DIVIDENDS

SUSTAINABILITY MARKET PRESENCE

~70%
Sales tied to sustainability enabling technologies

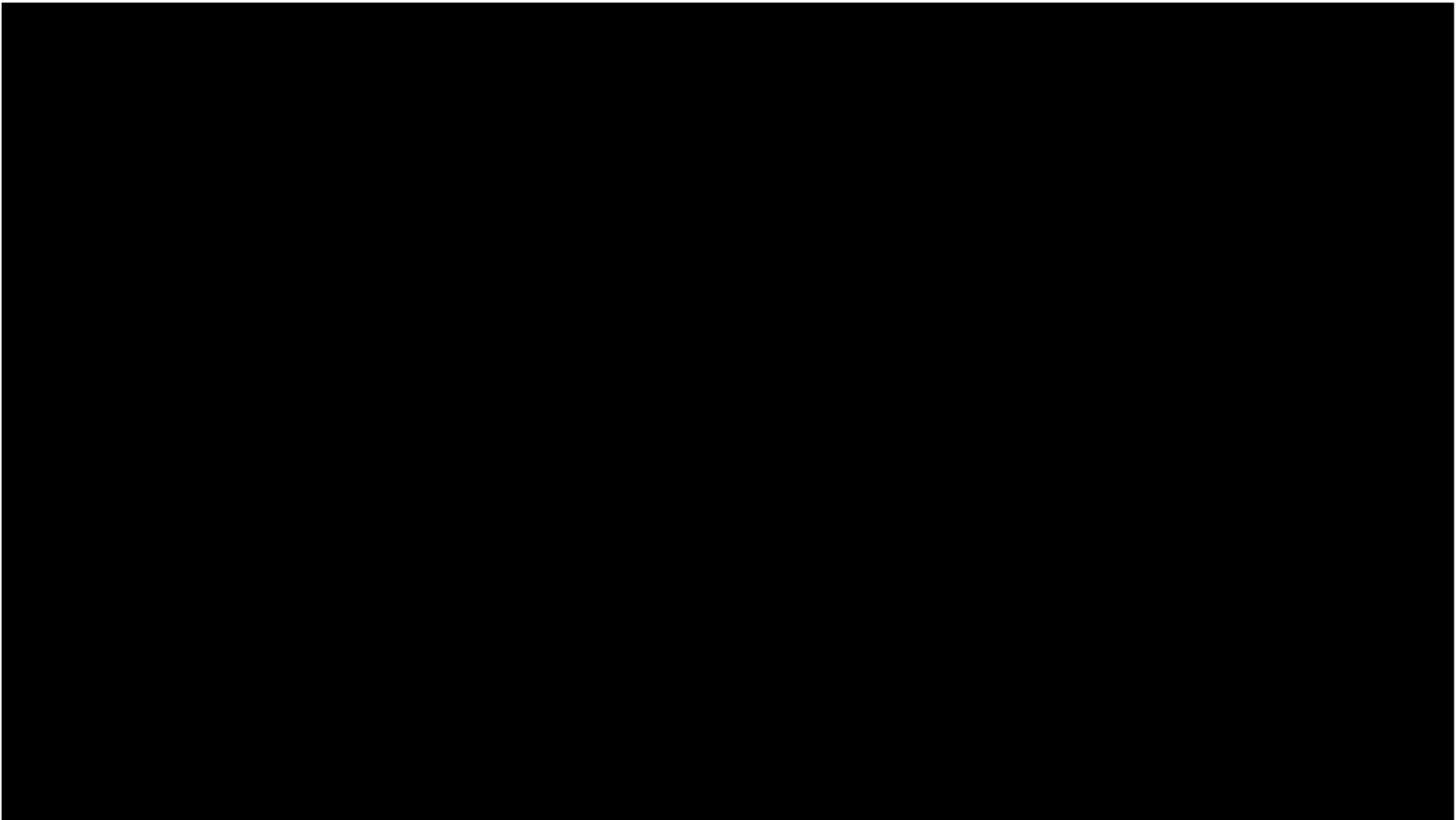
65%
Of 2022 electric vehicles produced using Emerson solutions

24 of Top 25
Life sciences companies use Emerson technology

60,000
Wind turbines controlled with Emerson systems

9 of Top 10
Semiconductor manufacturers use Emerson technology

CSB Video Of Philadelphia Refinery Explosion and Fire



Agenda

1 Introduction

2 What Does The Data Tell Us?

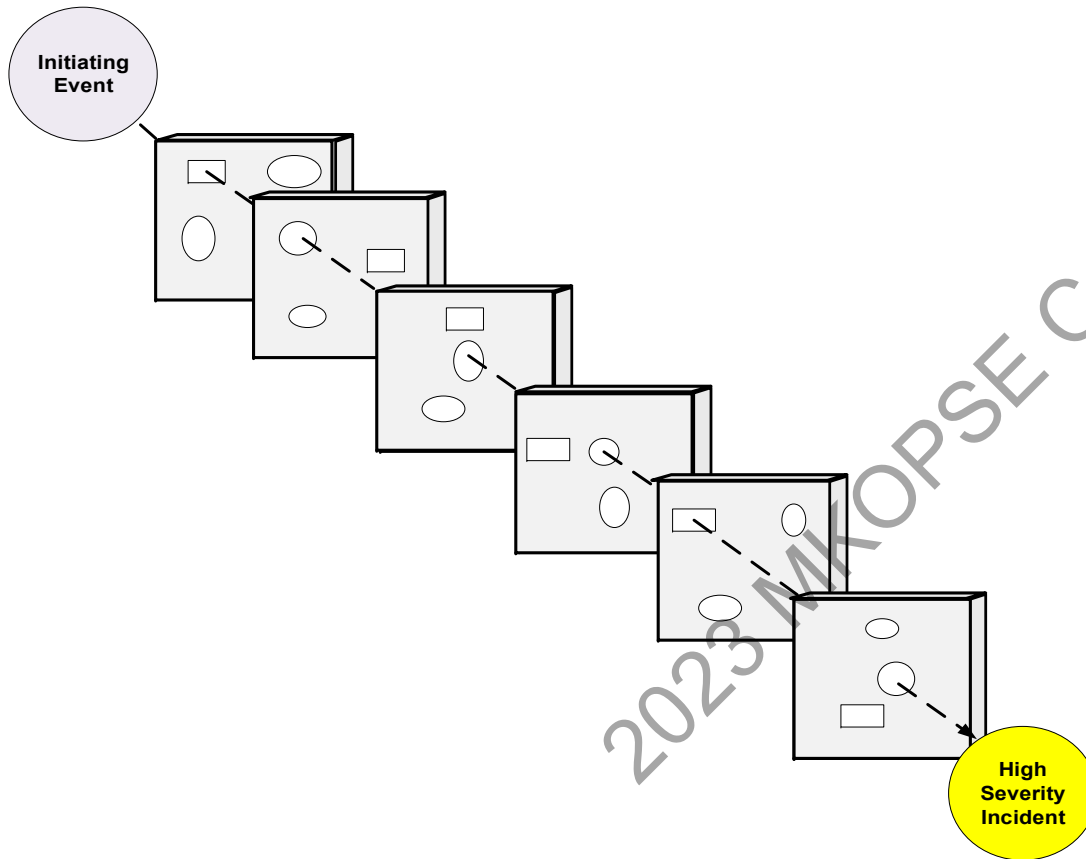
3 How Can Recent Technology Advances Improve Safety?

4 What To Do Next?

5 Summary And Questions

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Process Safety Risk Mitigation – Initial Layers of Protection

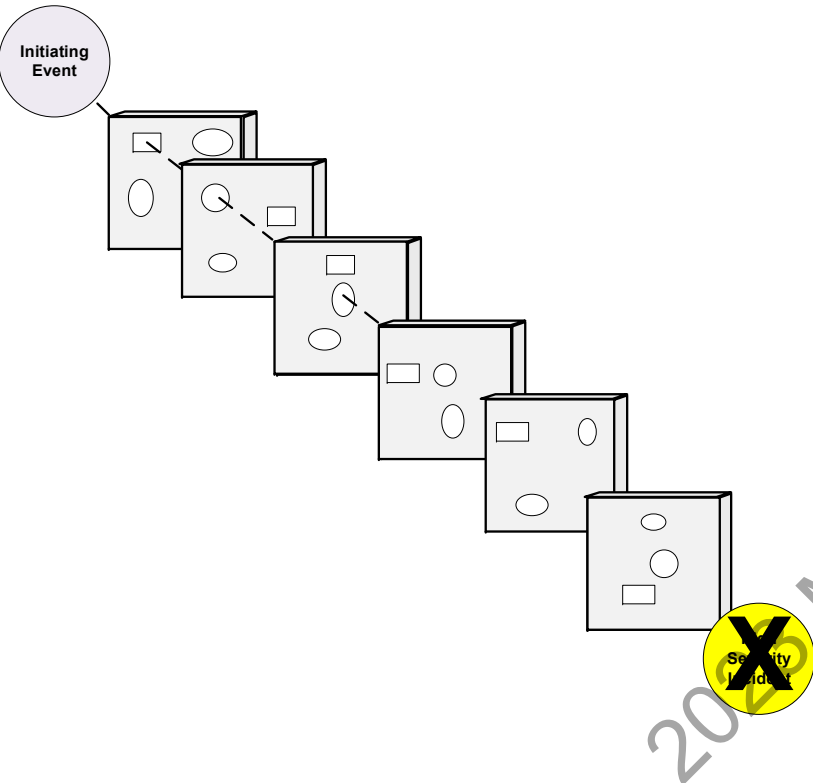


- Basic Process Chemistry and Components
- Process Design
- Staff Training and Procedures
- Equipment Maintenance and Monitoring Practices
- Basic Process Control Systems
 - Alarm Management
- Safety Shutdown Systems
- Relief Systems

How Can New Advanced Analytical and Automation Solutions Help?

- **Major Gulf Coast Refinery** - “Device diagnostic software (AMS) is key...we identified a problem with a boiler control transmitter that avoided an estimated production impact of \$5 million, as well as potential equipment damage.”
- **Major Onshore Oil & Gas Processor** – Implemented measurements and data analytics on key pumps. Analytics detected anomalous relationship between changes in pump intake pressure, motor amps and motor temperature and alerted maintenance – difficult to detect manually. Avoided a pump failure that could have created a safety incident and production losses.
- **A European refiner** operated four similar and parallel amine trains. They retrofitted real-time corrosion monitoring at key locations. It was determined that one of the four had *dramatically* higher corrosion rates which might have led to a safety incident and production losses prior to the next scheduled turnaround. Amine unit feed redistribution was implemented and the corrosion rate was brought under control.

Advanced Analytical and Automation Solutions - Process Safety Risk Mitigation – Components Impacted

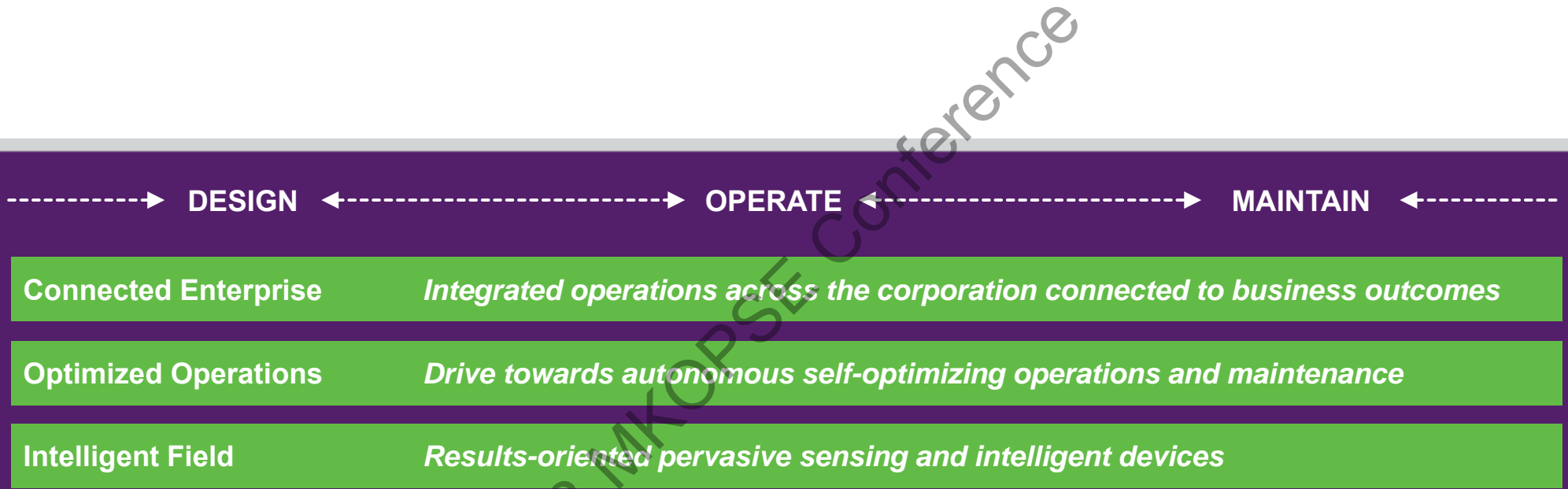


- **Basic Process Chemistry and Components**
- **Process Design**
- **Staff Training and Procedures**
- **Equipment Maintenance and Monitoring Practices**
- **Basic Process Control Systems**
 - **Alarm Systems**
- **Safety Shutdown Systems**
- **Relief Systems**



Advanced Analytical and Automation Solutions provide additional risk mitigation

What Is Meant By Advanced Analytical and Automation Solutions?



Safer Operation



More Sustainable

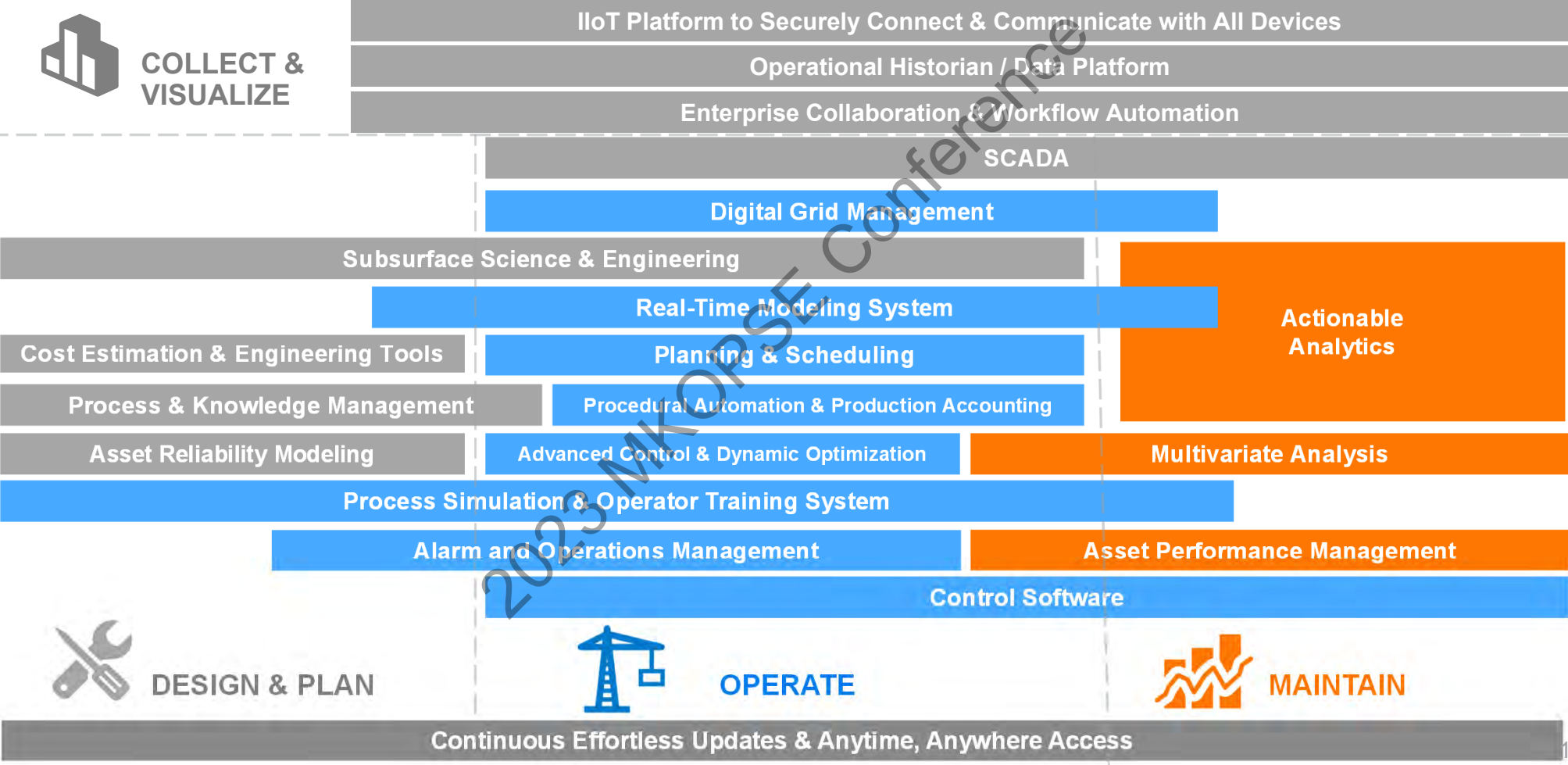


Increased Profitability



Improved Reliability

Advanced Automation/Industrial Software /Analytics Capabilities That Support Safety Across the Facility Lifecycle



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Refining And Chemical Plant Life Cycle: How Can Advanced Automation And Software Technology Help Improve Safety Through The Plant's Life Cycle?

Techno-economic Safety Design

Maintain Safe Operation

Meet Regulatory Requirements

Process Modification Evaluation

- Evaluate Potential Safety Issues Through Design Decisions Regarding New Processes Or Products
- Model Fire Environments

Production Planning For Safe Operation

- Operator Training Simulation
- Optimize Feedstock Selection
- Set Process Targets
- Optimize Predictive Maintenance

Enterprise Optimization

- Asset Safety Monitoring Available Throughout The Corporation
- Consolidate Disparate Data Into Actionable Desktop User Interface
- Automate Regulatory Report Generation

Process & Equipment Design

- Accelerate Effective But Safe Scale-up Of New Processes
- Sizing Overpressure Systems Including PRV's And Flare Systems
- Low Pressure Storage Tank Safety Modeling

Process Operation And Maintenance

- Accurate Warnings Of Potential Equipment Failures
- Reduce Personnel Exposure To Hazardous Conditions
- Procedural Automation Of Manual Operations
- Alarm System Management And Optimization
- Maintain "Integrity Operating Windows" Through Real Time Monitoring
- Digital Twin Modeling For Safety

Safety Incident – Possible Impact

Personnel Impact



- SIF (Serious Injuries/ Fatalities)
- OSHA Recordables
- OSHA Lost Time Injury

Safety Incident



Environmental Impact



- Tier 1, Tier 2 - LOPC Events
- EPA, State and Local Reportable Events
- NOV – Notice of Violations – Fines

Community Impact



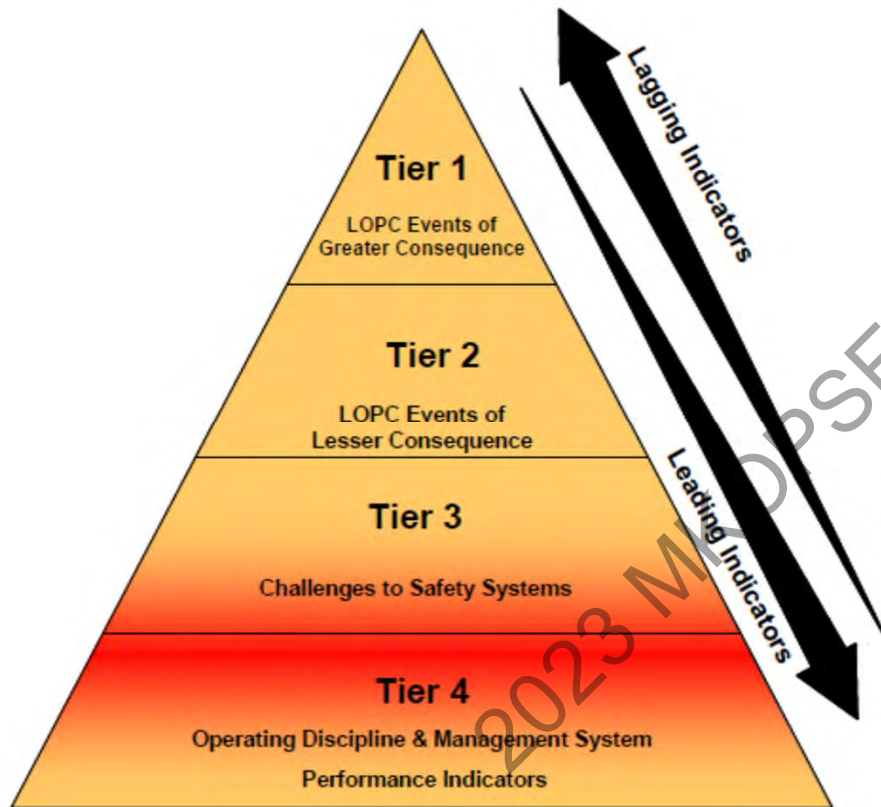
- Evacuation alert
- SIP – Shelter in Place alert
- Road Closures
- Media Headlines and Coverage

Financial Impact



- Direct Losses
- Production Losses
- Civil Suits
- High Loss Insurance Rates

Safety Event Classification - API RP 754

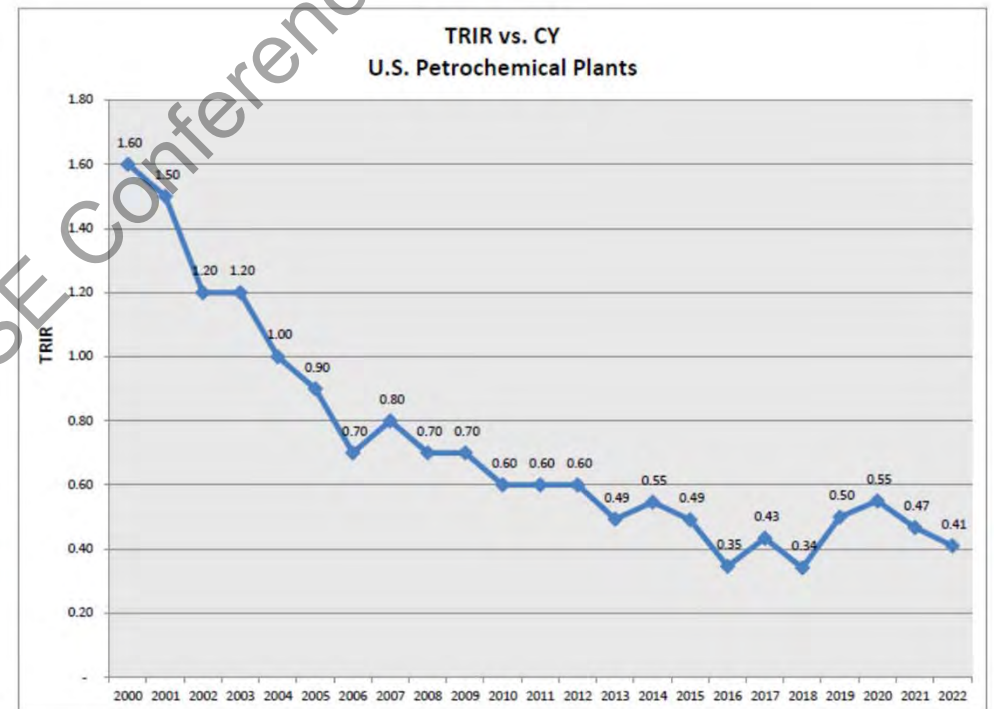
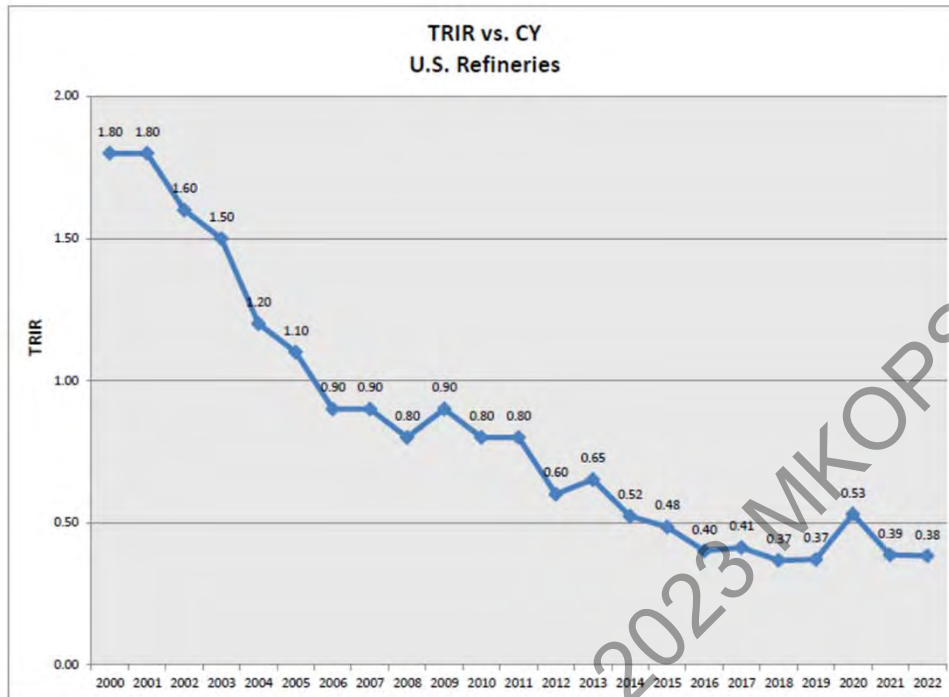


- In 2010, AFPM and API jointly created the Advanced Process Safety Program (APS)
- Consistent data collection (voluntary) on all safety events (big and small) from virtually all the US refining industry and the majority of the petrochemical industry
- Two sub-groups – Occupational Safety (Safety and Health Committee) and Process Safety (Process Safety Workgroup)

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What Does the Data Tell Us?

Occupational Safety



Source: 2022AFPM Occupational Injury and Illness Report

Process Safety - API 754 Tier 1 and Tier 2 Incidence



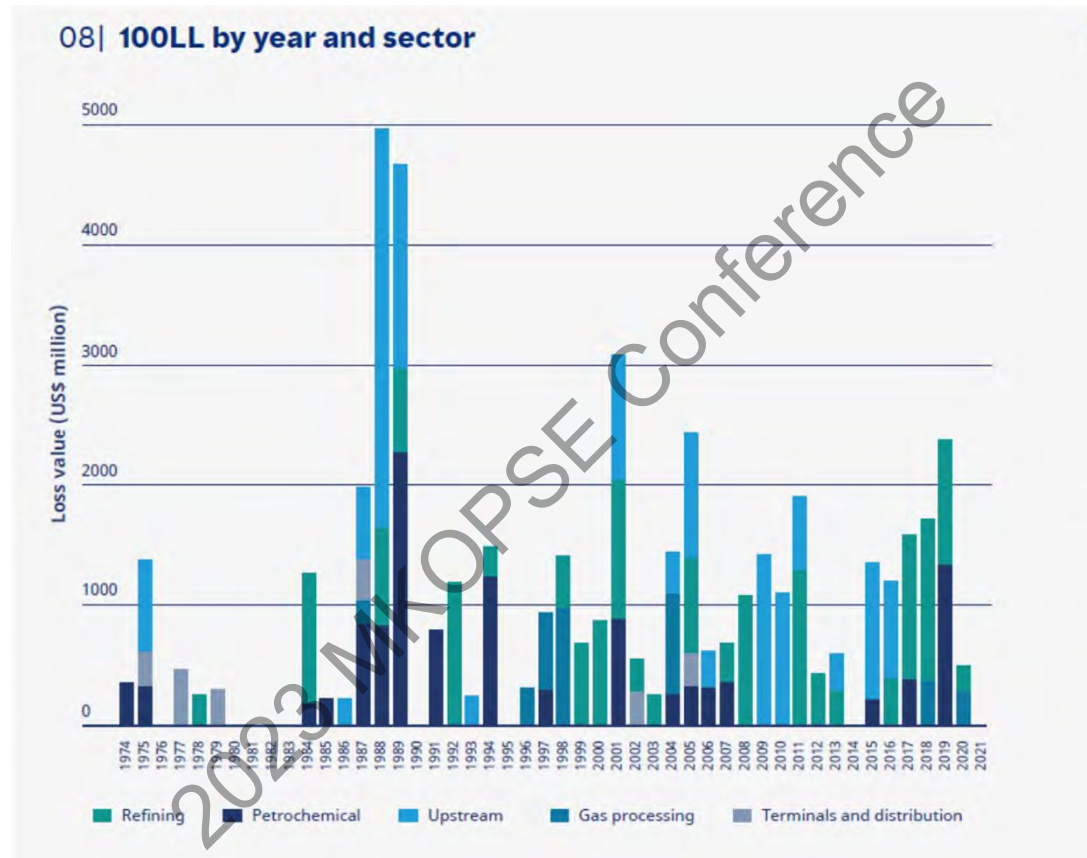
Source: AFPM Webinar; Advancing Process Safety; Nov 13, 2018

Most Common Locations For LOPC Incidents



Source: AFPM Focused Learning Report 2020

Hydrocarbon Industry Property Damage Loss History



Production
Losses Are
Additional!

Source: Marsh & McLennan; Large Property Damage Losses in the Hydrocarbon Industry 27th edition

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How Can Recent Technology Advances Improve Safety?

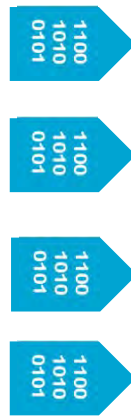
What Is Required For Advanced Analytics and Advanced Automation?

It starts with:

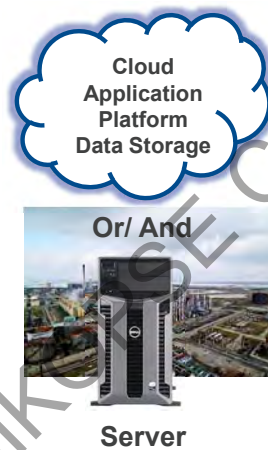
Data



Connectivity



Storage



Analytics



User Interface



You can measure and collect data from almost anything

You can send the data anywhere

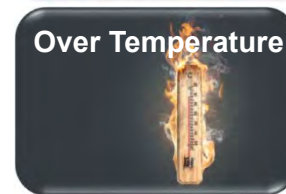
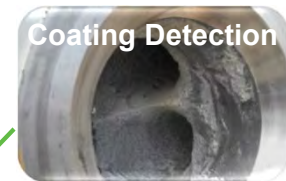
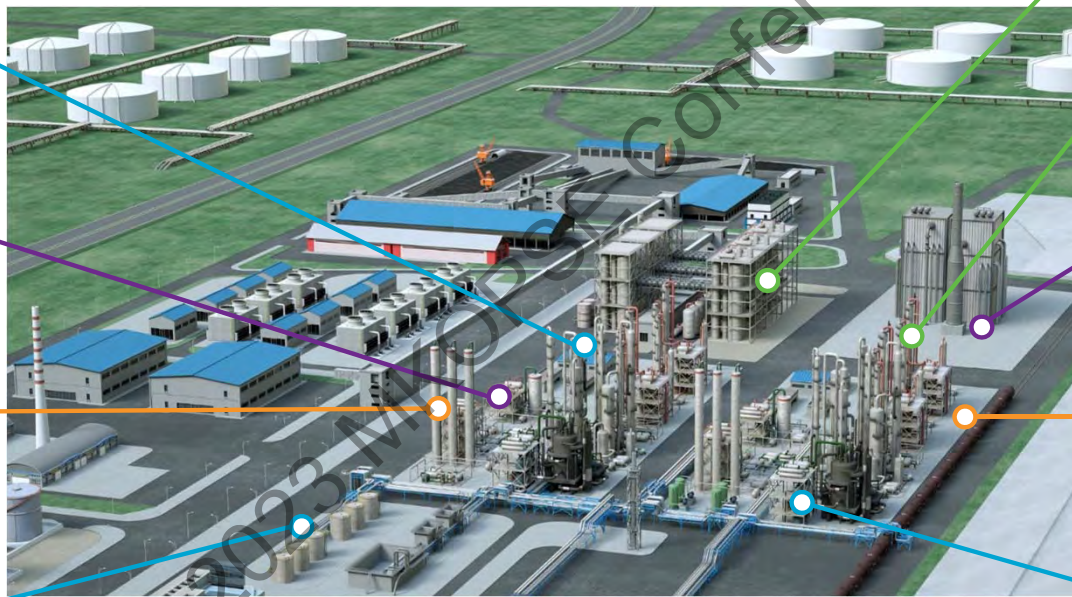
You can store all data with fast/ cheap access

Sophisticated analytics algorithms for model development easier to implement

Convenient User Interfaces

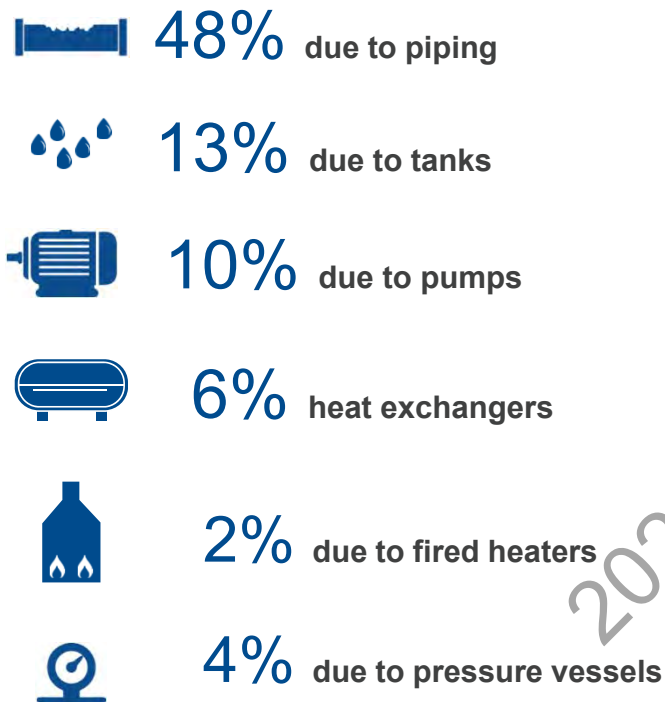
Improving Process Safety with Advanced Analytics

Process analytics can proactively monitor and detect abnormal conditions in processes, equipment, and connections that can affect operations and safety.



Tier 1 and Tier 2 Safety Events Frequency

Top Causes of Tier 1 and Tier 2 Safety Events



Solutions

Piping

Real time corrosion monitoring

Tanks

Complete tank safety systems including tank overfill protection

Pumps

Leak Detection and condition monitoring

Heat exchangers

Condition monitoring to detect problems

Fired heater

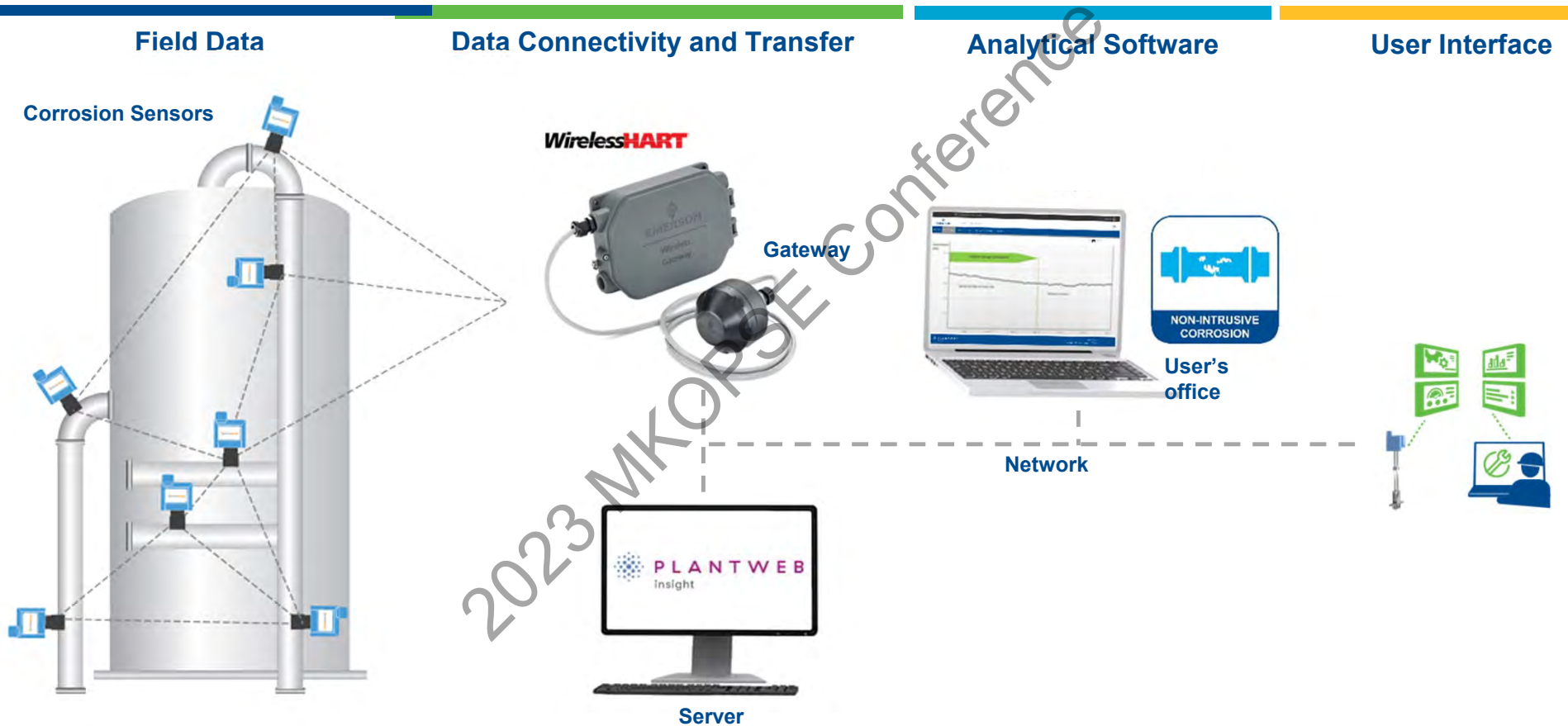
BMS compliant with new API standards.

Fire and leak monitoring

Ambient toxic gas detection and alarming

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Corrosion Example - Continuous Integrity Monitoring Delivers Real Time Asset Health Data Directly to Desk



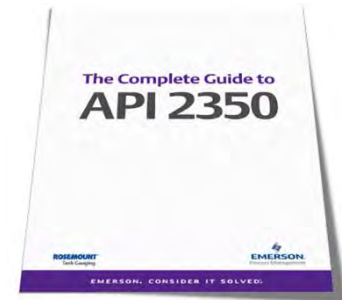
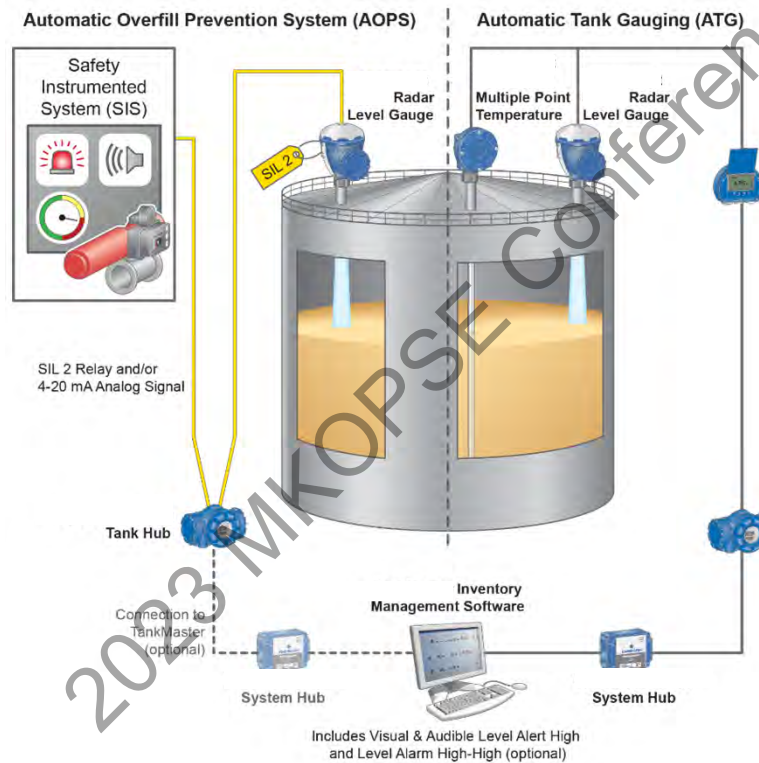
Tank Safety Solutions

One Overfill Statistically Occurs Every 3300 Filling Operations



One Overfill Every 10 Years for Group of 10 Tanks Filled 3x / Month

Source: Marsh and McLennan 2015



Independent Protection Layers

Serves as a Second Independent Layer of Defense Should the Basic Control System Fail



2-in-1 Functionality

Overfill Prevention and Level Measurement Using One Tank Nozzle



Comply with Regulations

API 2350 and IEC 61511 Compliant for Automatic and Manual Systems



Remote Proof-Testing

Safe and Fully Integrated Remote Partial Proof-Tests

Reduce Unplanned Shutdowns with Flame Instability Detection

Production Challenges

- Ultra low NOx burners were constantly on the verge of flame-out
- Variation in fuel BTU content causes flame instability
- Lack of insight to flame instability risked fired heater shutdowns and explosion risk in case of flame-out
- Traditional optical scanners are very expensive



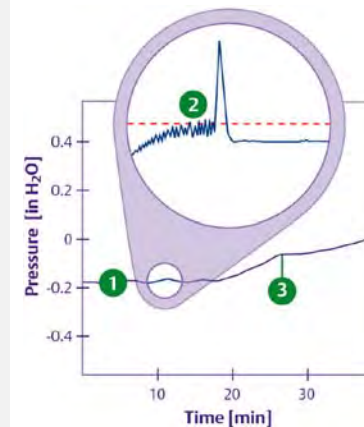
Value Enabler

Rosemount 3051S Pressure Transmitter with Process Intelligence Diagnostics

- Measure draft pressure in the firebox of the process heater at 22 times per second
- Statistical Process Monitoring (SPM) technology calculates standard deviation and mean of draft pressure
- Deviation from baseline is an indication of flame instability

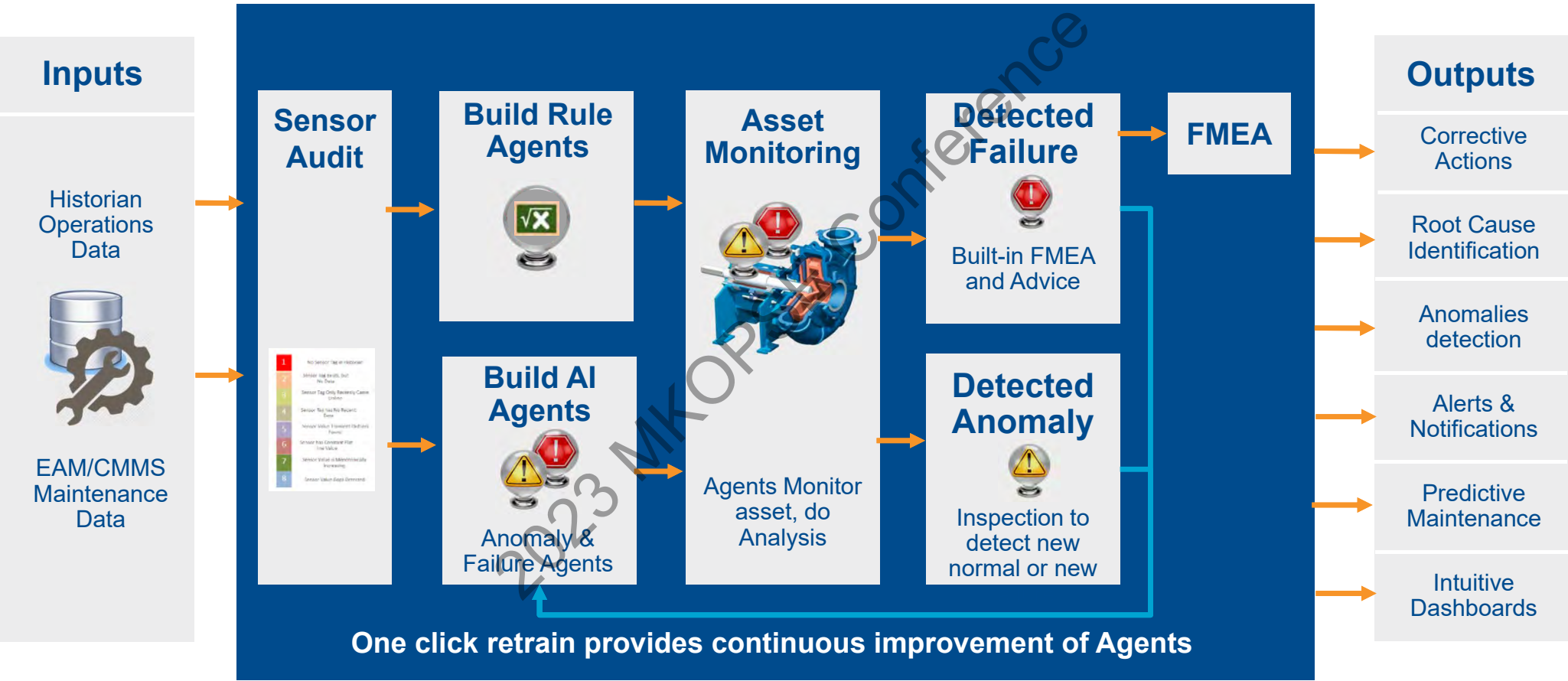
Impact on Operations

- Eliminating shutdowns saved \$1M per event
- 70% lower cost than optical system
- Reduced safety risk



1. Normal furnace operation
2. Early detection of flame instability
3. Flame-out occurs

AI Based Asset Fault Predictive Technology



Protective Autonomous Agent Fault Prediction - Lead Time Examples

Industry	Asset Type	Failure	Days Lead Time	Industry	Asset Type	Failure	Days Lead Time
Mining	De-Water/Thickener	High Torque	30	Transportation	Locomotive Engines	Hydro Loss-of-Engine	47
Transportation	Locomotive Engines	Crankcase Bearings	25	Midstream O&G	Pipeline Pump	Main Bearing Failure	21
Chemicals	Hyper-Compressors	Plunger Displacement	47	Downstream O&G	H2 Compressor	Valve Failure	30
Pharma	Freeze Driers	Pass-thur Leakage	21	Water/Wastewater	Generator (CH4)	Cracked Head	14
Refining	Charge Pumps	Bearings Seals	30	Midstream O&G	ESP's	Cavitation Fails Motor	30
Refining	Compressors	Impeller/Bearings/Seals	14	Transportation	Locomotive Engines	Crankshaft Fatigue	63
Mining	Slurry Pumps	Motor Burn-out	30	Chemicals	Quench Oil Tower	Fouling	26
LNG	Compressors	V-cone Flow Element	63	Chemicals	Compressors	Liquid Carry-over	5-60
Upstream	ESP's	Casing Leaks	26	Chemicals	Compressors	Cylinder Noise	4-34
Pharma	Chillers	Tube Leaks	5-60	Chemicals	Compressors	Valve Contamination	30
Upstream Drilling	Draw-works	Motor Fail	4-34	Chemicals	Furnace	Coil Plugging	48
Upstream	ESP's	Gas-lock	30	Downstream O&G	H2 Compressors	Liquid Carry-over Issues	45-80
Pulp & Paper	Kiln	Overheating/Fires	48	Downstream O&G	Compressor	3rd-stage Valve Fail	56
Forest Products	Drying System	Blower Thermal Flash	45-80	Downstream O&G	Charge Pumps	Feed Density Changes	120
Pulp & Paper	Pulp Refiner	Catastrophic Blade Fail	56	Downstream O&G	Incinerator	Flame-out Analysis	1000+
Pharma	Chiller	Motor Failure	30	Downstream O&G	Feed Pumps	Bearing Failures	40+
Upstream	Top-Drive	Lube Motor Failure	25	Downstream O&G	Feed Pumps	Alignment Issues	40+

Reducing Hazardous Exposure - Range of Wireless Measurement Products to Replace Manual Checks



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What To Do Next?

What Is The Next Step? – Safety Assessment Workshops

- Structured COLLABORATIVE process to build consensus on top priorities and safety impact
- Engagement from multiple disciplines at the plant and headquarters
- Experienced external consultants can facilitate session and provide outside expertise



Summary

- **Current Status in Refining and Petrochemical**
 - Occupational Safety – Significant decrease in incident rate previously but leveling off in recent years
 - Process Safety – Still a significant number of incidents of high significance
- **New Advanced Analytical and Automation technologies have the potential to provide early detection of potential safety incidents and to mitigate the consequences**

Catalog Client Safety Solutions

Customer	World Area	Application	Industry
BP Wytch Farm	EU	Safety -Eliminated operator rounds & used to improve wellhead monitoring	O&G Production
ADNOC	MEA	Safety -Eliminate hourly clipboard rounds to check fire safety system	Oil & Gas
Technochem	AP	Safety -Monitor tanks and are easily moved for multiple applications	Chemical
Croda	NA	Safety -Safely monitors temperatures in moving railcars	Chemical
Total Petrochemicals	EU	Safety -Monitors boiler condition of steam cracker to indicate. Increased safety due to reduction of movement of personnel into and around at-risk areas	Chemical

Customer	World Area	Application	Industry
Boise	NA	Severstal Wheeling	Metals - Steel
BP Port Allen	NA	Severstal Wheeling	Metals - Steel
We Energies	NA	Severstal Wheeling	Metals - Steel
Dow Chemical	NA	Dyno Nobel	Chemical

Customer	World Area	Application	Industry
San Diego Gas & Electric	NA	Lenzing Fibers	Pulp & Paper
Sun Chemical	NA	StatOil Hydro (Gulfaks)	Offshore
AOC	NA	CHS	Oil & Gas
Harcros Chemical	NA	Lion Oil	Oil & Gas
CalPortland	NA	Lion Oil	Oil & Gas
ADNOC	MEA	ADNOC	Oil & Gas
MET-MEX Pañoles	LA	MET-MEX Pañoles	Metals & Mining
Elkem	LA	Elkem	Metals & Mining
Temium	LA	Temium	Metals - Steel



EMERSON

Thank You!
Questions?

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A new index encompassing water-energy-food nexus and the risks associated with the production of protein

by

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²Institute for Energy Systems, University of Edinburgh, Edinburgh , UK

³Sustainability Cluster,

University of Petroleum and Energy Studies, Dehradun, India



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The food-water-energy-climate nexus impacted by the production of animal protein, and the associated risks

- Among the risks posed to the very existence of planet earth, one of the major ones is global warming and other forms of pollution caused in the course of producing animal protein from livestock

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The food system underpinning the world's current dietary patterns is responsible for around 21–37 % of total (GHG) emissions.

FAO report, 2020





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The livestock sector utilizes and impacts 30% of the non-polar terrestrial surface on the planet.

The meat and dairy industries create 7.1 gigatons of greenhouse gases annually—that's 14.5% of total man-made emissions.



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Raising, maintaining and utilizing livestock contribute about 18% of total anthropogenic greenhouse gas emission, second only to the top global warming sector: energy.

2023 WJK PSE Conference



Image courtesy <https://beef.unl.edu>

The water used by the livestock sector is more than 8% of the global human water use.

The global share of water used for industry, drinking and servicing is just 0.1%.

- 500-2000 litres to produce a 1 Kg of potato, wheat, rice, or soybeans
- 43000 litres to produce one 1 Kg of beef.



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Large quantities of energy and grain is required to produce meat as compared to other forms of food.

Livestock in USA consume more than 7 times as much grain as is consumed directly by the entire American population.



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- The impact of livestock production on degradation of land and soil erosion is equally severe.

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The prognosis



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- The demand for livestock—and consequently livestock production—is going to increase sharply and is expected to reach 465 million tonnes, or double the 2000 figure, by 2050 .

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Protein shortage

- The world is getting more and more short on plant protein
- But it is facing an even greater shortage of animal protein

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- There have been concerted attempts to reduce the footprints of the conventional livestock production processes but the limit of that goal seems to have reached within both technological as well as socio-economic constraints.
- This has left us with only one option: finding alternative sources of animal protein.

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The sustainability weighed protein production index (SWePPI)

- SWePPI aims to provide a tool with which risks of global warming and pollution are incorporated into the gains in terms of per unit mass of protein obtainable from a source.
- With the resulting index one can compare different options of protein production and learn how much risk each carries.
- The index also brings out the energy-water-food nexus as the driver of global warming and other forms of eco-degradation caused by different sources of animal protein.



Methodology

Parameter selection

Global warming potential (GWP)
Land use(LU)
Water use(WU)
Protein content(P)
Vitamin content (I and B)

Fuzzy inference system development

To develop the index, 729 rules were used

Optimization using evolutionary algorithms

To determine the optimal weights of a simplified weighted index

The food protein production index

The best algorithm was selected based on minimum error between the simplified index and fuzzy index. The optimized weights from the algorithm was deployed in the simplified weighted index

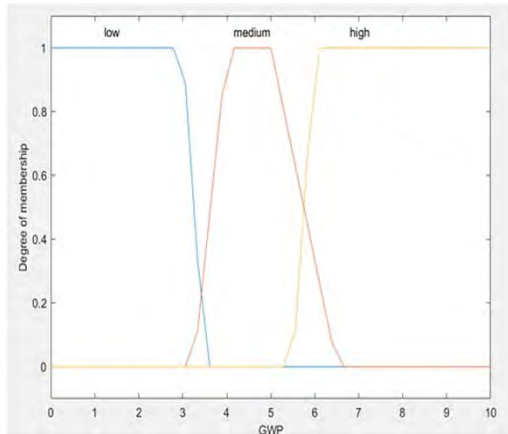
The fuzzy membership functions



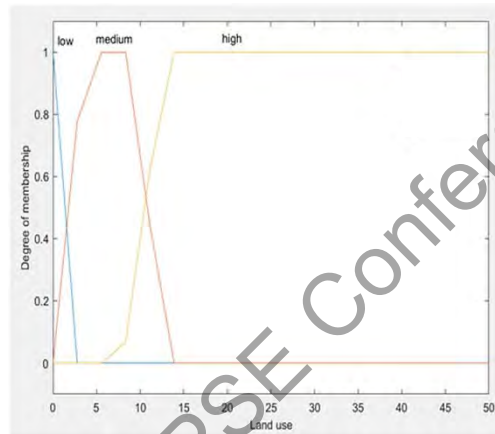
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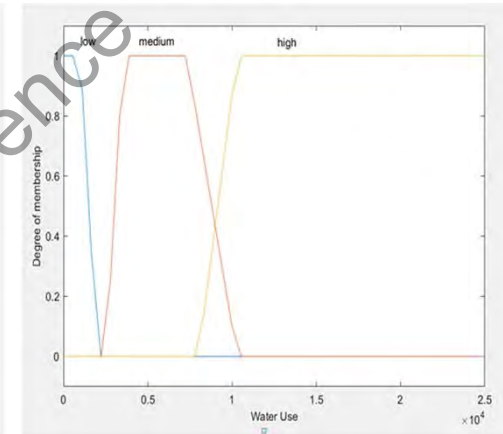
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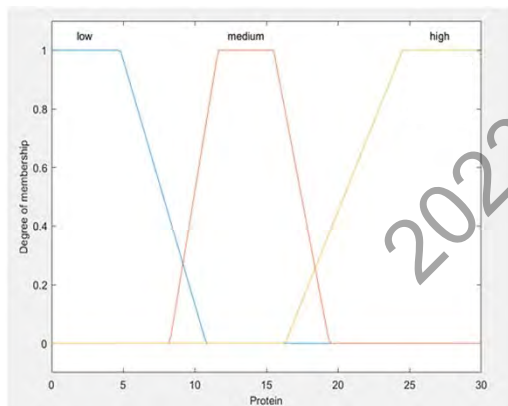
GWP



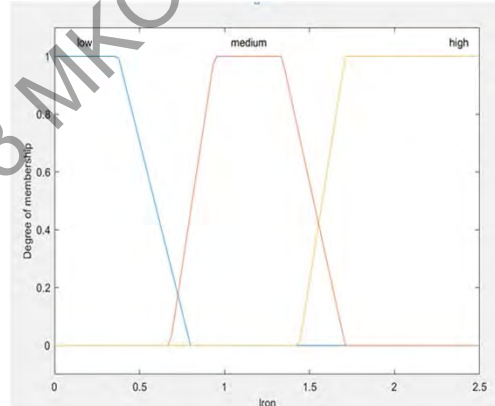
Land use



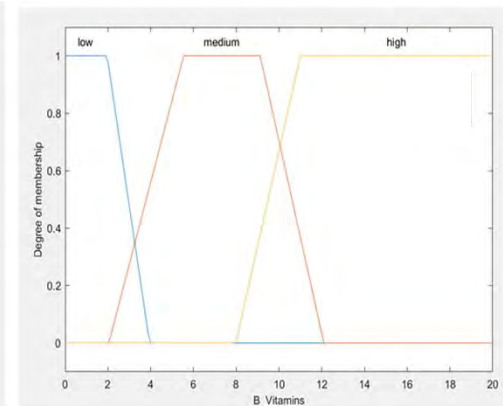
Water use



Protein content



Iron content



B-vitamins content

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Results



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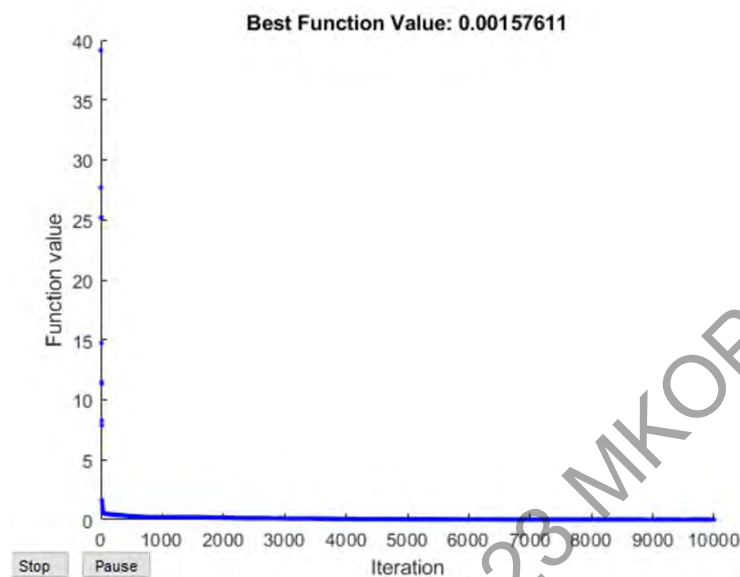


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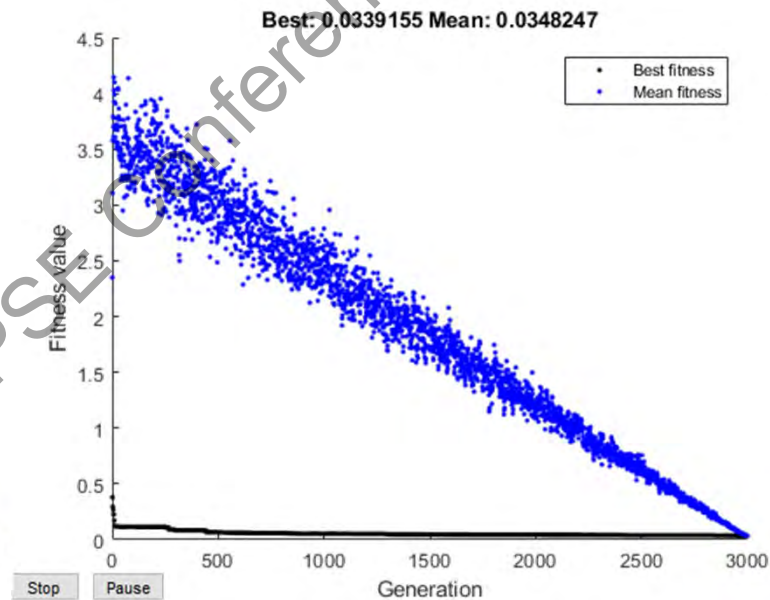


Animal Protein Source	GWP from farm to regional distribution centre (kg CO ₂ eq/kg produce or bone free meat)	Land use (m ² *year/kg food eaten)	Water (m ³ /ton)	Protein content per 100 g edible portion (g)	Iron content per 100 g edible portion (mg)	B Vitamins per 100 g edible portion (mg)	Fuzzy food sustainability index
Milk	1.39	1.7	1020	3.66	0.2	1.47	11.85
Eggs	3.39	4.5	3265	19	2.16	2.18	46.79
Beef	28.73	53	15415	21.45	2.96	13.86	12.34
Pork	5.85	24	5988	22	0.49	6.63	12.14
Chicken	4.12	8.7	4325	10.64	0.7	10.38	21.95
Mealworm	2.7	3.6	2.5	19.24	2.18	8.88	86.20

Performance of the PSO and GA algorithms in optimizing the weights of the PSI



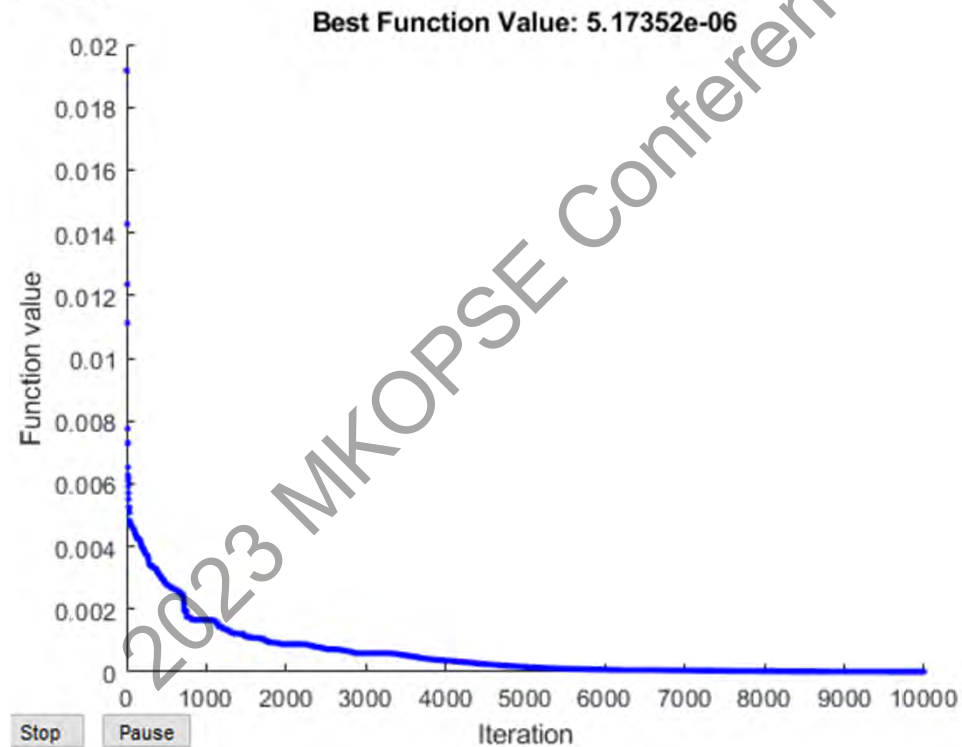
Performance of the Particle Swarm Optimization algorithm in optimizing weights of the PSI



Performance of the Genetic Algorithm in optimizing weights of the PSI



Performance of the particle swarm algorithm in optimizing weights of the PSI



Comparison of the linear indexes derived using GA and PSO

$$PSI_{PSO} = 7.66 * GWP - 3.00 * LU - 0.01 * WU + 3.81 * P - 5.95 * I + 1.81 * B$$

Animal Protein Source	Fuzzy food sustainability index	PSO derived linear food sustainability index (PSO-FSI)	GA derived linear food sustainability index (GA-FSI)
Milk	11.85	11.85	3.66
Eggs	46.79	46.79	47.71
Beef	12.34	12.34	12.25
Pork	12.14	12.14	12.51
Chicken	21.95	21.95	22.67
Mealworm	86.20	86.20	85.52

GWP: Global warming potential from farm to regional distribution center,
LU: Land use, WU: Water use, P: Protein content, I: Iron content, B: B-vitamins content

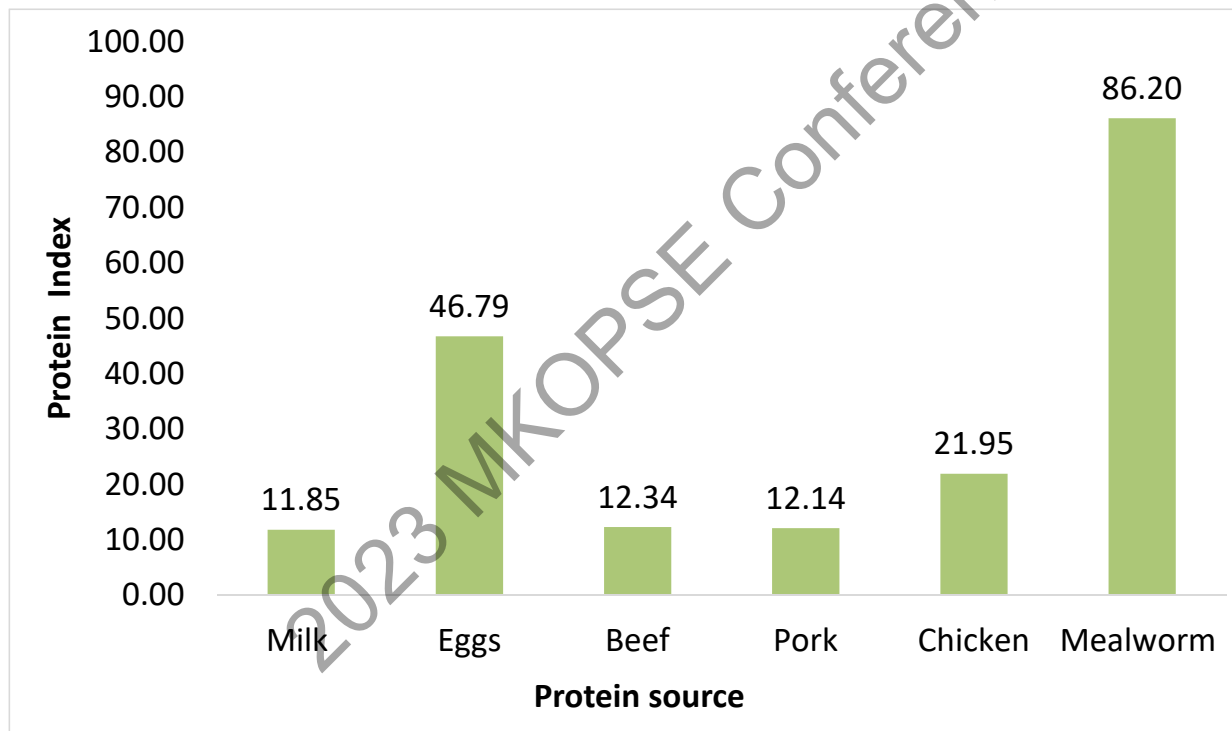


Index score	Interpretation
0 - 30	Low sustainability
30 - 60	Average sustainability
60 -80	Good sustainability
80 - 100	Excellent sustainability

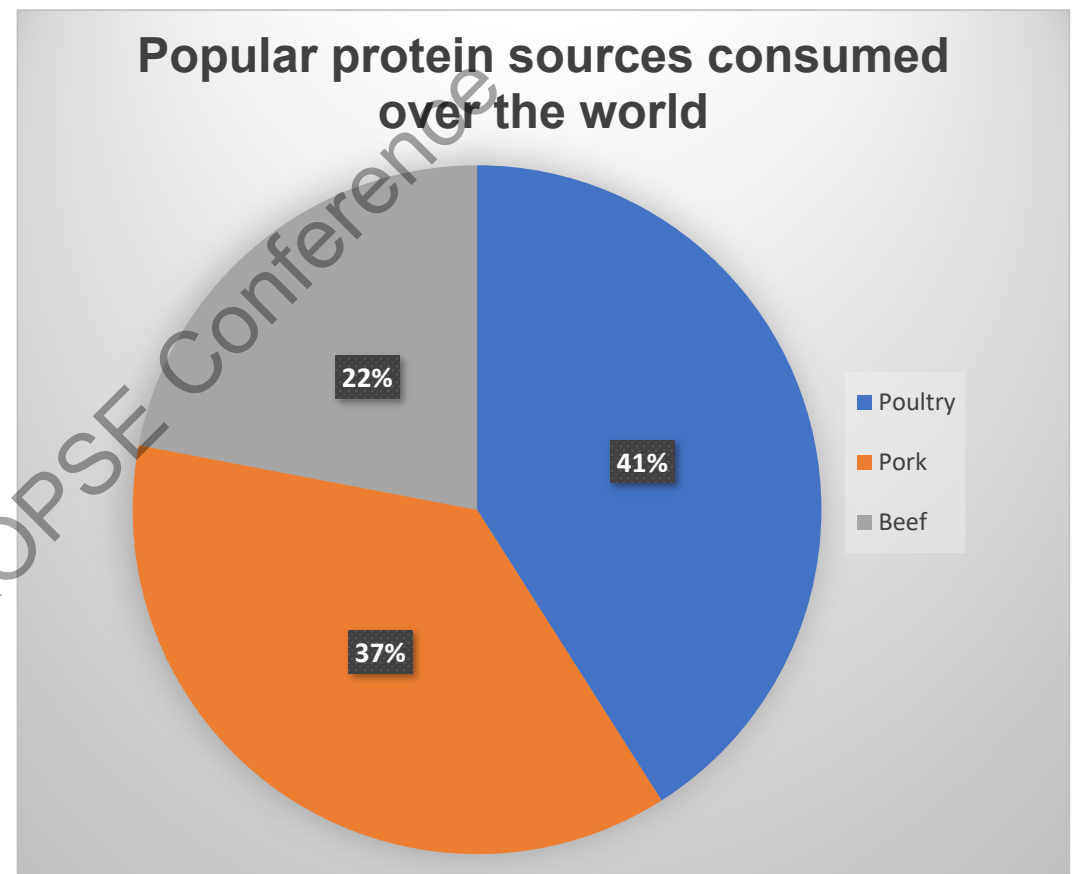
2023 MORSE Conference



Index scores for various sources of animal protein



- By a recent estimate (Shahbandeh, 2023) poultry is the most widely eaten animal meat in the world (41%), followed by pork (37%) and beef (22%).
- On the scale of animal protein in general, fish and other aquatic sources contribute the most (33%), followed by poultry (28%), pork (25%) and beef (15%).





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- Other sources of animal protein are also consumed in different regions such as bush meat, frogs, reptiles, and dogs but their proportion in global human diet is negligible.
- This shows that from among millions of genera of animals, humankind depends mostly on just 3 genera for its meat intake, and a few more for its overall animal protein intake.
- And production of all these sources of animal protein is imposing on the world great risk of global warming, pollution, and ecosystem collapse.



<https://www.mashed.com>



Minilivestock: a veritable treasure trove

- One of the potentially most diverse, nutritious, and eco-friendly sources of animal protein is small invertebrates, mainly insects.
- If this sounds incredulous, and possibly revolting, to hear, permit me to real off these facts:
- During all but a few hundred years of its 4 million year presence on earth, Homo sapiens has been an insect-eater, or entomophagous.
- It is even said that it was due to certain proteins present abundantly in insects, which are lean in higher animals, that human brain could evolve much faster and better than it otherwise have.





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Due to certain socio-religious factors entomophagy was gradually abandoned in most areas of the world.

Yet it not only survives but thrives in certain regions, mainly in South-East Asia, Latin America, and parts of Africa.



Insect lollipops, Germany

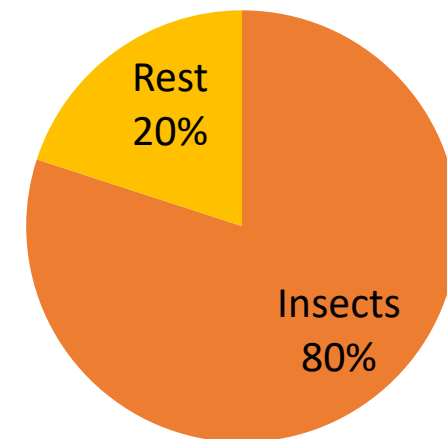


Chaprah – red ant Chutney , *Chattisgarh, India*



Key factors which make insects — or minilivestock — potentially better source of animal protein than conventional Livestock

- For every kilogram of vegetation consumed, more animal protein is generated by minilivestock than by conventional livestock.
- Meat production, in particular, consumes great energy as it takes 10 times more plant nutrients to produce meat than equivalent quantities of insect protein.



Animal Kingdom



- Minilivestock is able to transform phytomass into zoomass much more efficiently than conventional livestock .
- A substantial contribution to this energy efficiency comes from higher edible weight fraction of insects. For example 80% of a cricket is edible as compared to 58% of chicken and 40% of beef.
- Insects are poikilothermic—they can change their body temperatures to match that of the surroundings. Due to this, the insects have to spend much less part of their food energy and nutrients in maintaining their body temperature than the warm-blooded livestock have to. This further enhances the overall energy efficiency of insect-based protein production.





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- Unlike conventional livestock, insects can be reared on a myriad of biodegradable waste. For practically every substance of organic origin, there are one or more species of insects specialized in feeding upon it.
- If an organic waste happens to carry the risk of pathogens and contaminants—such as manure—the insects reared on it may not be directly utilizable for human consumption but can be made to contribute, with due quality control, indirectly to human diet by use as poultry or fish feed.
- In this manner insects can reduce the demand on foodgrain for livestock feed and free that much extra foodgrain for human consumption. In turn they may either reduce, or add value to the very substantial water use that is involved in grain production (especially rice).



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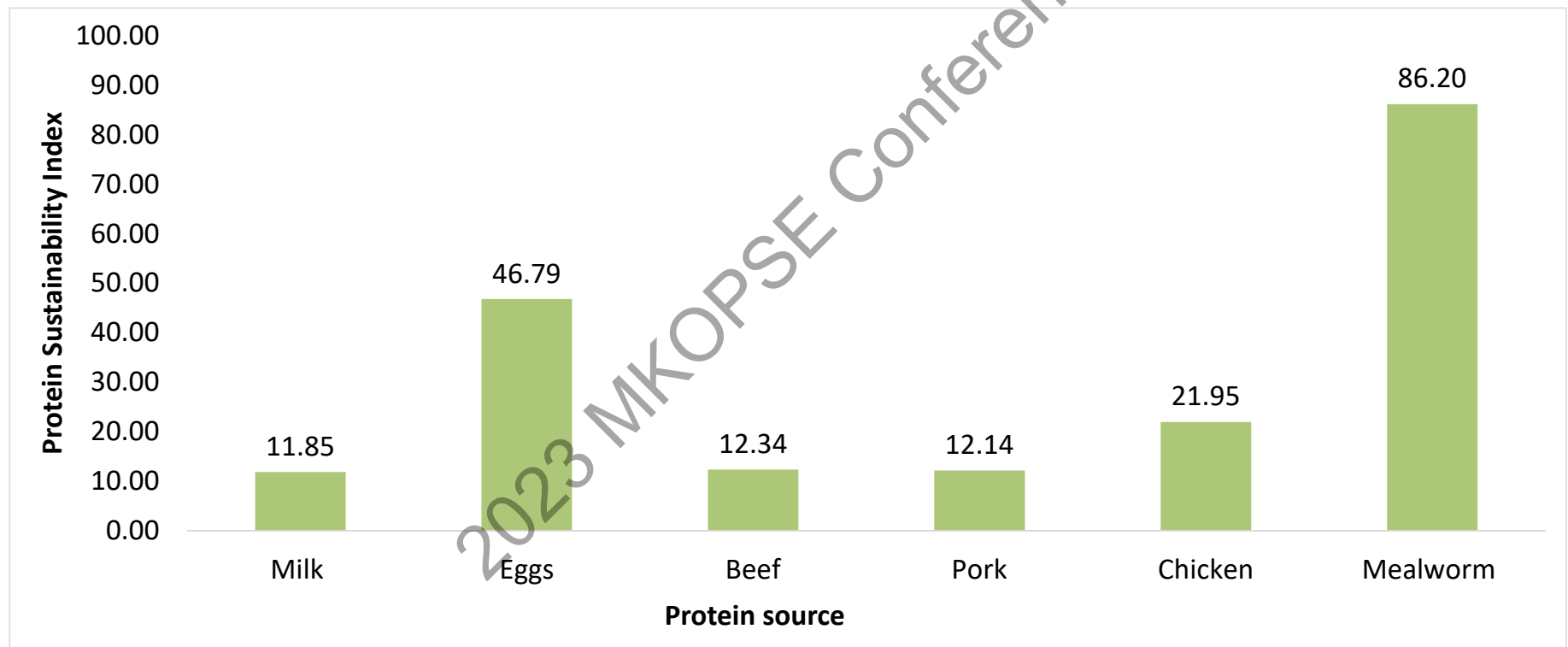
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- The significance of this aspect can be gauged from the fact that 60 percent of the total cost of raising farm animals is incurred on the feed of which a major portion comes from foodgrain.
- In the USA about 91% of the estimated 27.1 million tons of cereal, legume, and vegetable protein that is otherwise fit for human nutrition, is fed to livestock every year. In return only 5.3 million tons of animal protein is obtained.



Back to the sustainability score of various protein sources





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So would you like to try meal worms in your next meal?



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Thank you

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Greater reproductive thrust



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Insects have much higher fecundity and much faster growth rate

